

# **LS-DYNA EXAMPLES MANUAL**

**March 1998**

Copyright © 1989-1998

**LIVERMORE SOFTWARE  
TECHNOLOGY CORPORATION**

All Rights Reserved

**Written By**

**John D. Reid, Ph.D.  
Department of Mechanical Engineering  
University of Nebraska-Lincoln**

Mailing Address:

Livermore Software Technology Coporation  
2876 Waverley Way  
Livermore, California 94550-1740

Support Address:

Livermore Software Technology Corporation  
97 Rickenbacker Circle  
Livermore, California 94550-7612

FAX: 925-449-2507  
TEL: 925-449-2500  
EMAIL: sales@lstc.com

Copyright © 1989-1998 by Livermore Software Technology Corporation  
All Rights Reserved

**TABLE OF CONTENTS**

INTRODUCTION .....	1
*AIRBAG .....	3
Airbag Deploys into Cylinder .....	3
*BOUNDARY_PRESCRIBED_MOTION .....	11
Blow Molding .....	11
*CONSTRAINED .....	19
Two Plates Connected With Butt Welds .....	19
Sliding Blocks With Planar Joint .....	27
Hinged Shell With Stop Angle (Revolute Joint) .....	35
Linearly Constrained Plate .....	41
Impulsively Loaded Cap With Shells and Solids .....	47
Spot Weld Secures Two Plates .....	55
*CONTACT .....	61
Shell Rebounds From Plate Using Five Contact Types .....	61
Projectile Penetrates Plate .....	69
Rigid Sphere Impacts a Plate at High Speed .....	75
Corrugated Sheet Contacts Edges .....	83
Discrete Nodes Tied to a Surface .....	89
*CONTACT_ENTITY .....	95
Rigid Sphere Impacts Plate .....	95
*CONTROL .....	101
CONTACT: Hemispherical Punch .....	101
DAMPING: Cantilever Beam .....	109
ENERGY: Bar Impact .....	117
SHELL: Hemispherical Load .....	123
SHELL: Twisted Cantilever Beam .....	129
TIMESTEP: Billet Upset .....	135
*CONTROL_ADAPTIVE .....	141
Deep Drawing With Adaptivity .....	141
Square Crush Tube With Adaptivity .....	149
Cylinder Undergoing Deformation With Adaptivity .....	155

## TABLE OF CONTENTS

---

*DAMPING_GLOBAL.....	161
Tire Bounces on the Ground and Damps Out .....	161
*DEFORMABLE_TO_RIGID .....	167
Interaction of Pendulums .....	167
*INTEGRATION_SHELL .....	175
Cantilever Beam With Lobotto Integration.....	175
*INTERFACE_COMPONENT.....	181
An Interface File Controls the Response of a Cube .....	181
*LOAD_BODY .....	191
GENERALIZED: Rotating Elements .....	191
Z: Tire Under Gravity Loading Bounces on a Rigid Wall .....	197
*MAT .....	203
Frazer-Nash Single Element.....	203
Piecewise Linear Plasticity Fragmenting Plate .....	209
Rigid Sliding Block in Local Coordinate System .....	215
Soil and Foam Single Element.....	221
Belted Dummy With Springs .....	227
Rectangular Cup Drawing.....	239
*RIGIDWALL.....	247
Rigid Wall Sphere Impacts a Plate.....	247
Rotating Shell Strikes Rigid Wall .....	253
Cube Rebounding.....	259
Symmetric Crush Tube .....	265
*SECTION.....	271
SHELL: Fuse Plate in Tension Exhibits Hourglassing .....	271
SOLID: Breaking Post Exhibits Hourglassing.....	277
ACKNOWLEDGMENTS .....	285
REFERENCES .....	287
INDEX.....	289

## Introduction

This is an assembly of example problems provided by a number of resources. The resources and histories are documented in the acknowledgment and reference sections. Users are encouraged to submit examples which will facilitate the education of LS-DYNA users.

### October 1997 Modifications

- All examples were documented and re-organized for clarity.
- All examples ran successfully using LS-DYNA version 940 on a Sun SPARC 10 workstation.
- Many examples required changes to make them work. Descriptions of the examples were updated to reflect the examples as they are as of this date.
- All graphics in this edition have been replaced with newly created results using LS-TAURUS on the Sun SPARC 10 workstation.
- Many new examples were added to the manual.
- The examples are now strictly in keyword format. References to ingrid and structured format have been removed for they are no longer consistent with these examples.
- Naming Conventions for the examples have been changed as described below.

### Naming Convention

The naming convention for the input decks is: keyword.description.k Keyword defines the major keyword used within the example. Description defines either the action or the physical content of the problem. The “.k” on the end of the filename signifies that the file is a keyword format LS-DYNA input file.

## **INTRODUCTION**

---

**LS-DYNA Manual Section:** \*AIRBAG\_SIMPLE\_AIRBAG\_MODEL

**Additional Sections:**

\*CONTACT\_NODES\_TO\_SURFACE  
\*RIGIDWALL\_PLANAR

**Example:** Airbag Deploys into Cylinder

**Filename:** airbag.deploy.k

**Description:**

An airbag inflates below a rigid cylinder, causing the cylinder to fly into the air.

**Model:**

The volume pressure relationships is defined by the Simple Airbag Model for control volumes. The bag inflates through the flow of mass into the bag.

**Input:**

The control volume defines the thermodynamic relationship for the gas in terms of parameters such as heat capacity, gas temperature, incoming mass, and outgoing mass (\*AIRBAG\_SIMPLE\_AIRBAG\_MODEL). A rigidwall is used below the airbag to act as ground (\*RIGIDWALL\_PLANAR). A ground is displayed using rigid shell elements, but is used only for visualization purposes. The contact between the airbag and the cylinder is automatically generated by part id (\*CONTACT\_NODES\_TO\_SURFACE).

**Results:**

The plots show the bag expanding. The ASCII file abstat contains information on the computed pressure, volume, mass flow and internal energy of the control volume (\*DATABASE\_ABSTAT).





**\*AIRBAG\_SIMPLE\_AIRBAG\_MODEL**  
**Airbag Deploys into Cylinder**

---

```
$
*DATABASE_RCFORC
$   dt
  2.000E-04
$
*DATABASE_RBDOUT
$   dt
  2.000E-04
$
*DATABASE_RWFORC
$   dt
  2.000E-04
$
$$$$$
$$$$$ Airbag
$$$$$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*AIRBAG_SIMPLE_AIRBAG_MODEL
$   sid   sidtyp   rbid   vsca   psca   vini   mwd   spsf
$       1       1
$
$   cv     cp     t     lcld   mu     a     pe     ro
$ 1.736E+03 2.430E+03 1.200E+03   1 7.000E-01 0.000E+00 1.470E+01 3.821E-06
$
$   lou
$
$
*SET_PART_LIST
$   sid   da1   da2   da3   da4
$       1
$
$   pid1   pid2   pid3   pid4   pid5   pid6   pid7   pid8
$       3
$
*DEFINE_CURVE
$   lcld   sidr   scla   sclo   offa   offo
$       1
$
$   abscissa   ordinate
$   0.000E+00   0.000E+00
$   3.200E-02   2.600E+01
$   4.500E-02   6.000E-01
$   8.000E-02   1.000E-01
$
$$$$$
$$$$$ Rigid Walls
$$$$$
$$$$$ Ground
$
*RIGIDWALL_PLANAR
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$   nsid   nsidex   boxid
$       0       0       0
$   xt     yt     zt     xh     yh     zh     fric
$   0.0    0.0    0.0    0.0    1.0    0.0    0.5
$
```



**\*AIRBAG\_SIMPLE\_AIRBAG\_MODEL**  
Airbag Deploys into Cylinder

```

$
$  lco/a1      a2      a3      v1      v2      v3
$
$
$
$ *MAT_FABRIC
$      mid      ro      ea      eb      ec      prba      prca      prcb
$          3      1.00e-4      2.00e+6      2.00e+6      2.00e+6      0.35      0.35      0.35
$
$      gab      gbc      gca      gse      el      prl      lratio      damp
$      1.53e+6      1.53e+6      1.53e+6
$
$      aopt
$
$
$      xp      yp      zp      a1      a2      a3
$
$      v1      v2      v3      d1      d2      d3
$
$
$$$$$ Sections
$
$ *SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icomp
$          1          0
$
$      t1      t2      t3      t4      nloc
$      0.500      0.500      0.500      0.500
$
$
$ *SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icomp
$          2          9          4          1
$
$      t1      t2      t3      t4      nloc
$      0.015      0.015      0.015      0.015
$
$      b1      b2      b3      b4      b5      b6      b7      b8
$
$
$$$$$ Define Nodes and Elements
$
$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$      nid      x      y      z      tc      rc
$ *NODE
$      3722  2.250000000E+00  2.500000000E+00  -1.250000000E+01
$      3723  2.206770000E+00  2.938950000E+00  -1.250000000E+01
$      3724  2.078730000E+00  3.361040000E+00  -1.250000000E+01
$
$      ... in total, 3867 nodes defined
$
$      7586  1.200000000E+01  0.000000000E+00  -1.170000000E+01
$      7587  -1.200000000E+01  0.000000000E+00  -1.300000000E+01
$      7588  1.200000000E+01  0.000000000E+00  -1.300000000E+01
$
$
$$$$$ Elements
$
$
$ *ELEMENT_SHELL
$      eid      pid      n1      n2      n3      n4

```

# **\*AIRBAG\_SIMPLE\_AIRBAG\_MODEL**

## **Airbag Deploys into Cylinder**

---

6993	1	7547	7509	7148	7549
6994	1	7509	7510	7149	7148
6995	1	7510	7511	7150	7149

.  
... in total, 3792 shells defined

6990	3	7078	7048	7144	7145
6991	3	7108	7078	7145	7146
6992	3	5998	7108	7146	7147

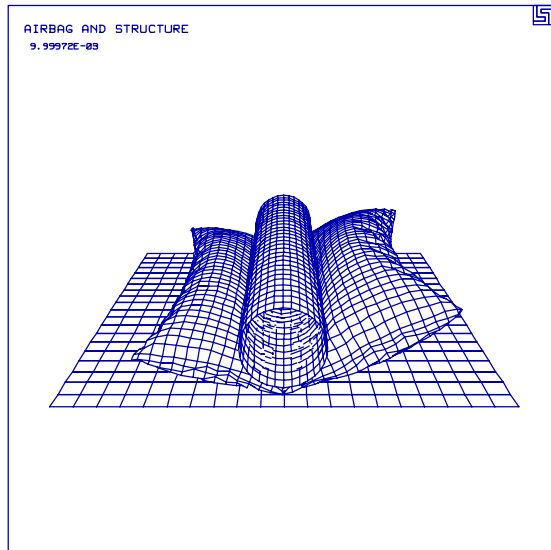
\$  
\*END

# \*AIRBAG\_SIMPLE\_AIRBAG\_MODEL

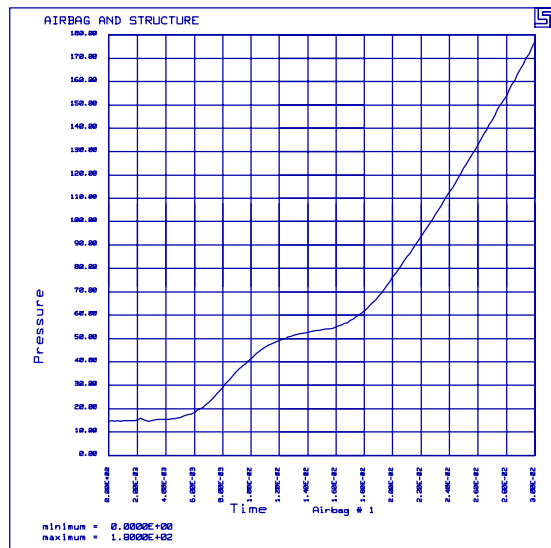
## Airbag Deploys into Cylinder

### Results:

taurus g=d3plot  
19  
state 15 rx 20 view



phs3  
abstat  
grid oset 0  
180 pressure



**\*AIRBAG\_SIMPLE\_AIRBAG\_MODEL**  
Airbag Deploys into Cylinder

---

**LS-DYNA Manual Section:** \*BOUNDARY\_PRESCRIBED\_MOTION

**Additional Sections:**

\*LOAD\_SEGMENT

**Example:** Blow Molding

**Filename:** boundary\_prescribed\_motion.blow-mold.k

**Description:**

This problem includes two tools, a punch nose and a die tube. A blank tube is formed by blow molding the nose through the tube.

**Model:**

The hollow tube blank is made with 600 shell elements AND has an outer radius of 12.06 mm, an initial thickness of 1.37 mm, and an initial length of 53.5 mm. The internal pressure of the hollow tube blank is  $40 \text{ N/mm}^2$  applied using the \*LOAD\_SEGMENT keyword. The tools are rigid shell elements. Only 1/4 of the system is modeled because of symmetry.

The motion of the punch nose and the end of the blank follow a linear motion with a total displacement of 15 mm (\*BOUNDARY\_PRESCRIBED\_MOTION).

**Reference:**

Wei, Lixin











# \*BOUNDARY\_PRESCRIBED\_MOTION

## Blow Molding

---

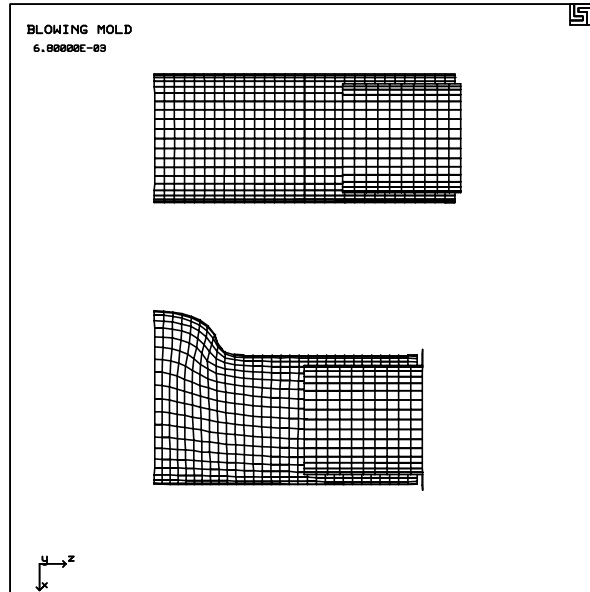
```
*NODE
$   nid          x          y          z          tc          rc
   1001  .130103000E+02  -.113825400E+01  .535000000E+02
   1002  .129937800E+02  .126376400E+01  .535000000E+02
   .
   ... in total, 1437 nodes defined
   .
   3650  -.113750000E+02  .442958800E-05  .517166600E+02
   3651  -.113750000E+02  .442958800E-05  .534999900E+02
$
$$$$$$$$$ Shell Elements
$
*ELEMENT_SHELL
$   eid      pid      n1      n2      n3      n4
   1001      1      1001      1002      1003      1004
   1002      1      1004      1003      1005      1006
   .
   ... in total, 1313 shells defined
   .
   2197      2      2226      2187      2198      2227
   2198      2      2227      2198      2209      2228
$
*END
```

# \*BOUNDARY\_PRESCRIBED\_MOTION

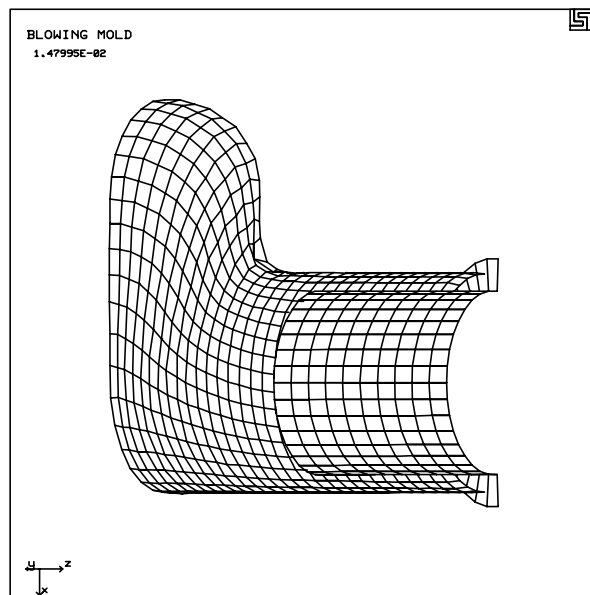
## Blow Molding

### Results:

taurus g=d3plot  
angle 1 rz -90 ry 90 -m 1 dist 6000  
ytrans 40 view ytrans -50 s 35 over view



s 75  
ry 30  
center view



**\*BOUNDARY\_PRESCRIBED\_MOTION**

Blow Molding

---

**\*CONSTRAINED\_GENERALIZED\_WELD**  
Two Plates Connected With Butt Welds

---

**LS-DYNA Manual Section:** \*CONSTRAINED\_GENERALIZED\_WELD

**Additional Sections:**

\*DATABASE\_CROSS\_SECTION\_PLANE

**Example:** Two Plates Connected with Butt Welds

**Filename:** constrained.butt-weld.k

**Description:**

Two plates are connected by four butt welds. The plates are pulled apart and the center two welds fail.

**Model:**

Each plate is constructed with 12 shell elements. One end of one plate is fixed with SPC's. One end of the other plate has a prescribed motion condition defined. The other ends of the plates are butt welded together with failure criteria. Cross sections are defined through each plate to monitor the forces through the plates as they are pulled apart.

**Results:**

```
butt weld constraint failed between nodes      35 & 23
: Time          = 1.26913E+00 : xl-force   = 5.56053E+00
: yl-force      = 2.28915E-03 : zl-force   = -1.93680E-07
: xl-moment     = -3.16675E-07 : yl-moment  = 9.09511E-07
: plastic ep=   0.00000E+00
```

Stresses in weld:

```
: signn        = 2.78026E-01 : tautn      = 0.00000E+00
: signm        = 9.09511E-08 : tautm      = 0.00000E+00
: signs        = 0.00000E+00 : tauts      = 1.14458E-04
: tautw        = -9.68398E-09
```

```
butt weld constraint failed between nodes      37 & 25
: Time          = 1.26913E+00 : xl-force   = 5.56054E+00
: yl-force      = -2.29328E-03 : zl-force   = -2.41027E-07
: xl-moment     = 2.97763E-07 : yl-moment  = 3.22515E-07
: plastic ep=   0.00000E+00
```

Stresses in weld:

```
: signn        = 2.78027E-01 : tautn      = 0.00000E+00
: signm        = 3.22515E-08 : tautm      = 0.00000E+00
: signs        = 0.00000E+00 : tauts      = -1.14664E-04
: tautw        = -1.20514E-08
```

# \*CONSTRAINED\_GENERALIZED\_WELD

## Two Plates Connected With Butt Welds

---

### List of LS-DYNA input deck:

```

*KEYWORD
*TITLE
Two plates connected with a Butt Weld
$
$ LSTC Example
$
$ Last Modified: October 16, 1997
$
$ Units: mm, kg, ms, kN, GPa, kN-mm
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Control Output
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*CONTROL_TERMINATION
$ endtim endcyc dtmin endneg endmas
 3.01
$
*CONTROL_ENERGY
$ hgen rwen slnten rylene
 2 2
$
*CONTROL_OUTPUT
$ npopt neecho nrefup iaccop opifs ipnint ikedit
 1 3
$
*CONTROL_SHELL
$ wrpang itrist irnxx istupd theory bwc miter
 1 6
$
$
*DATABASE_BINARY_D3PLOT
$ dt lcdt
 0.2
$
*DATABASE_EXTENT_BINARY
$ neiph neips maxint strflg sigflg epsflg rltflg engflg
$
$ cmpflg ieverp beamip
 1
$
*DATABASE_BINARY_D3THDT
$ dt lcdt
 999999
$
*DATABASE_GLSTAT
$ dt
 0.1
$
*DATABASE_MATSUM
$ dt
 0.1
$
*DATABASE_NODOUT
$ dt

```







**\*CONSTRAINED\_GENERALIZED\_WELD**  
**Two Plates Connected With Butt Welds**

---

```

$
*DEFINE_CURVE
$
$      lcid      sidr      scla      sclo      offa      offo
$            1

$
$      abscissa      ordinate
$            0.0000      0.0
$            5.0000      2.0000
$            20.0000      2.0000
$
*SET_NODE_LIST
$      sid
$      1
$      nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
$            34       36       38       40
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$      pid      sid      mid      eosid      hgid      grav      adpopt
$      platel      2      2      1
$      plate2      3      2      1
$
$
$$$$$ Materials
$
*MAT_PLASTIC_KINEMATIC
$      mid      ro      e      pr      sigy      etan      beta
$            1      2.70e-6      68.9      0.330      0.286      0.00689
$
$      src      srp      fs
$            0.1
$
$
$$$$$ Sections
$
*SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icomp
$            2      6
$
$      t1      t2      t3      t4      nloc
$            2.0      2.0      2.0      2.0
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$
*NODE
$      nid      x      y      z      tc      rc

```

# \*CONSTRAINED\_GENERALIZED\_WELD

## Two Plates Connected With Butt Welds

---

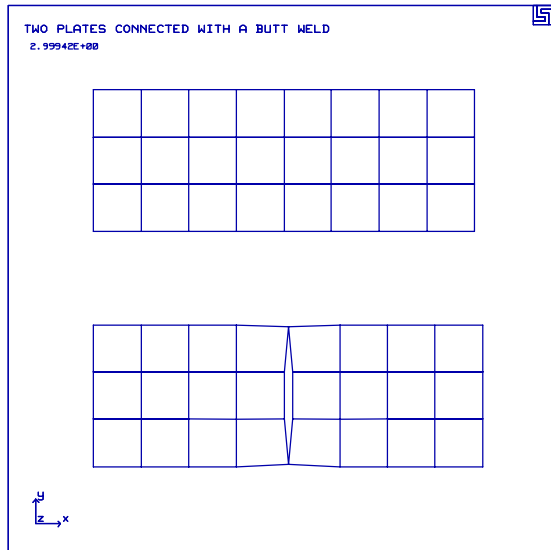
```
1 5.000000000E+01 2.000000000E+01 0.000000000E+00
2 6.000000000E+01 2.000000000E+01 0.000000000E+00
.
... in total, 40 nodes defined
.
39 4.000000000E+01 0.000000000E+00 0.000000000E+00
40 8.000000000E+01 0.000000000E+00 0.000000000E+00
$
$$$$$$$$ Shell Elements
$
*ELEMENT_SHELL
$   eid      pid      n1      n2      n3      n4
   1         2       20       14       8       22
   2         2       14       15       9       8
.
... in total, 24 shells defined
.
23         3         5         6       32       31
24         3         6        38       40       32
$
*END
```

# \*CONSTRAINED\_GENERALIZED\_WELD

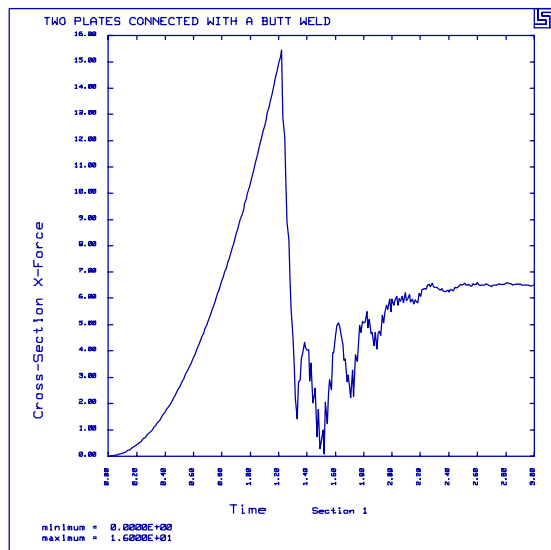
## Two Plates Connected With Butt Welds

### Results:

taurus g=d3plot  
ytran 25 view  
ytran -50 state 16 over view



phs3  
secforc  
smooth 5  
oset 0 16 x-for 1



**\*CONSTRAINED\_GENERALIZED\_WELD**

Two Plates Connected With Butt Welds

---

**LS-DYNA Manual Section:** \*CONSTRAINED\_JOINT\_PLANAR

**Additional Sections:**

\*LOAD\_NODE\_POINT  
\*LOAD\_SEGMENT  
\*INITIAL\_VELOCITY\_NODE  
\*CONSTRAINED\_EXTRA\_NODES\_SET

**Example:** Sliding Blocks with Planar Joint

**Filename:** constrained.joint\_planar.k

**Description:**

This problem illustrates a planar joint connecting two rigid bodies.

**Model:**

The first block measuring  $2 \times 2 \times 2$  slides along a second block measuring  $2 \times 2 \times 8$ . A third flexible body controls the time step size. The first block has a ramped pressure of 100 psi applied to the top surface and ramped concentrated forces applied to a lower edge of 40 lbs. The initial velocity of the first block is 400 inches/second.

**Input:**

One joint definition consist of nodes 128, 126, 129 and 127 (\*CONSTRAINED\_JOINT\_PLANAR). The nodes are extra nodes attached to the rigid bodies and are coincident (\*CONSTRAINED\_EXTRA\_NODES\_SET, \*SET\_NODE\_LIST).

**Results:**

The plots show that the first block correctly slides across the second block.





# \*CONSTRAINED\_JOINT\_PLANAR

## Sliding Blocks with Planar Joint

---

```

$
$. . . > . . . 1 . . . > . . . 2 . . . > . . . 3 . . . > . . . 4 . . . > . . . 5 . . . > . . . 6 . . . > . . . 7 . . . > . . . 8
$
*CONSTRAINED_JOINT_PLANAR
$
$          n1          n2          n3          n4          n5          n6          rps
$          128          126          129          127          127          128          0.000E+00
$
*CONSTRAINED_EXTRA_NODES_SET
$
$          pid          nsid
$           1           1
$
*SET_NODE_LIST
$
$          sid
$           1
$
$          nid1          nid2          nid3          nid4          nid5          nid6          nid7          nid8
$          126          127
$
*CONSTRAINED_EXTRA_NODES_SET
$
$          pid          nsid
$           2           2
$
*SET_NODE_LIST
$
$          sid
$           2
$
$          nid1          nid2          nid3          nid4          nid5          nid6          nid7          nid8
$          128          129
$
$$$$ Parts and Materials
$
$$$$
$
$. . . > . . . 1 . . . > . . . 2 . . . > . . . 3 . . . > . . . 4 . . . > . . . 5 . . . > . . . 6 . . . > . . . 7 . . . > . . . 8
$
*PART
fixed rigid body
$
$          pid          sid          mid          eosid          hgid          igrav          adpopt
$           1           1           1          1.000E+01          1           1           0
$
*PART
sliding rigid body
$
$          pid          sid          mid
$           2           2           2
$
*PART
elastic body for time step control
$
$          pid          sid          mid
$           3           3           3
$
$$$$ Materials
$
*MAT_RIGID
$
$          mid          ro          e          pr          n          couple          m          alias
$           1  7.850E-04  3.000E+07  3.000E-01

```

# \*CONSTRAINED\_JOINT\_PLANAR

## Sliding Blocks with Planar Joint

---

```
$
$   cmo      con1      con2
$ 1.000E+00 7.000E+00 7.000E+00
$
$   lco/a1      a2      a3      v1      v2      v3
$
$
$*MAT_RIGID
$
$   mid      ro      e      pr      n      couple      m      alias
$       2 7.850E-04 3.000E+07 3.000E-01
$
$   cmo      con1      con2
$
$   lco/a1      a2      a3      v1      v2      v3
$
$
$*MAT_ELASTIC
$
$   mid      ro      e      pr
$       3 7.850E-04 3.000E+07 3.000E-01
$
$
$$$$ Sections
$
$*SECTION_SOLID
$   sid      elform
$     1      0
$     2      0
$     3      0
$
$$$$
$$$$
$$$$ Loading
$$$$
$$$$ Pressure load on top of block
$
$*LOAD_SEGMENT
$
$   lcid      sf      at      n1      n2      n3      n4
$     1 1.000E+00 0.000E+00      97      106      107      98
$     1 1.000E+00 0.000E+00     106      115      116      107
$     1 1.000E+00 0.000E+00      98      107      108      99
$     1 1.000E+00 0.000E+00     107      116      117      108
$
$*DEFINE_CURVE
$
$   lcid      sidr      scla      sclo      offa      offo
$     1      0 0.000E+00 0.000E+00 0.000E+00 0.000E+00
$
$   abscissa      ordinate
$ 0.000000000E+00      0.000000000E+00
$ 9.99999978E-03      1.000000000E+02
$ 1.99999996E-02      1.000000000E+02
$
$
$$$$ Force load on lower edge of block
$
$*LOAD_NODE_POINT
$
```

---





# \*CONSTRAINED\_JOINT\_PLANAR

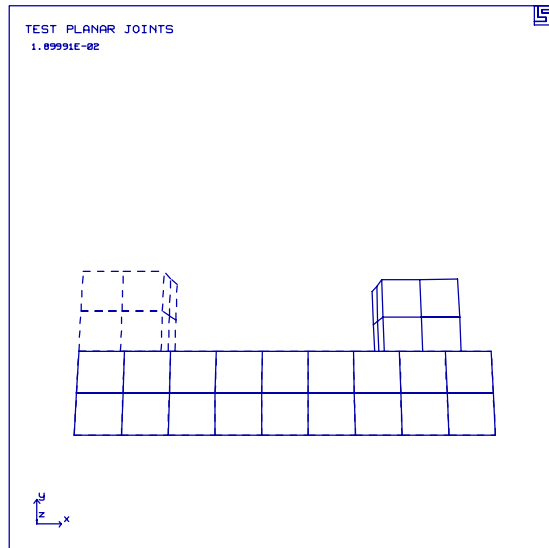
## Sliding Blocks with Planar Joint

### Results:

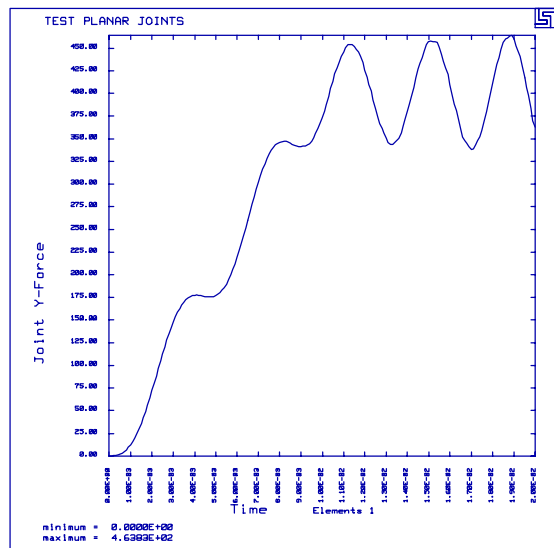
taurus g=d3plot

19

<m 3 rx -10 udg 1 state 20 over view



phs3  
jntforc  
oscl -1 y-force



**\*CONSTRAINED\_JOINT\_PLANAR**  
Sliding Blocks with Planar Joint

---

## \*CONSTRAINED\_JOINT\_REVOLUTE Hinged Shell with Stop Angle (Revolute Joint)

---

**LS-DYNA Manual Section:** \*CONSTRAINED\_JOINT\_REVOLUTE

**Additional Sections:**

\*CONSTRAINED\_JOINT\_STIFFNESS  
\*CONTROL\_TIMESTEP

**Example:** Hinged Shell with Stop Angle (Revolute Joint)

**Filename:** constrained\_joint\_revolute.k

**Description:**

Two rigid shell elements are joined together using a revolute joint. A stop angle is defined so that the rotating plate can only rotate 30 degrees relative to the other plate.

**Model:**

A pair of concentrated loads are applied to the end nodes of a hinge-jointed shell system using \*LOAD\_NODE\_POINT. One of the rigid plates is fixed by using the capability within the \*MAT\_RIGID keyword. The rotating plate has a stop angle of 30 degrees relative to the fixed plate defined using the \*CONSTRAINED\_JOINT\_STIFFNESS\_GENERALIZED keyword.

Because all components in the model are rigid, the time step needs to be controlled by limiting the maximum time step to 4.15E-06 s. (In deformable structures, the minimum time step is usually the one of concern.)

**Results:**

The rotating plate at several states are shown imposed on each other. The maximum rotated angle is closer to 38 degrees rather than the specified 30 degrees. This is because the joint stiffness actual defines the angle at which the resistance force is to begin. The forces associated with stopping the rotating plate can be determined by examining the jntforc ascii file.

# \*CONSTRAINED\_JOINT\_REVOLUTE

## Hinged Shell with Stop Angle (Revolute Joint)

---

### List of LS-DYNA input deck:

```

*KEYWORD
*TITLE
hinged shell w/ stop angle
$
$ LSTC Example
$
$ Last Modified: October 16, 1997
$
$ - This problem has a pair of concentrated loads applied to
$ the end nodes of a hinge-jointed shell system.
$
$ - 30 degree stop angle (must add joint stiffness, local coord system)
$
$ - control timestep with maximum 4.15E-06
$
$ Units: lbf-s2/in, in, s, lbf, psi, lbf-in
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTROL_TERMINATION
$  endtim   endcyc     dtmin    endeng    endmas
  2.000E-02
$
*CONTROL_TIMESTEP
$  dtinit    scft      isdo     tslimt     dtms      lctm      erode     mslst
                       5
$
*DEFINE_CURVE
$   lcid     sidr      scla     sclo      offa      offo
     5
$           abscissa           ordinate
             0.0               4.15E-06
             1.0               4.15E-06
$
*DATABASE_BINARY_D3PLOT
$   dt      lcdt
 5.000E-04
$
*DATABASE_GLSTAT
$   dt
 0.0001
$
*DATABASE_JNTFORC
$   dt
 1.000E-04
$
*DATABASE_NODOUT
$   dt
 0.0001
$
*DATABASE_HISTORY_NODE
$   nid1     nid2
     3       4
$

```



**\*CONSTRAINED\_JOINT\_REVOLUTE**  
**Hinged Shell with Stop Angle (Revolute Joint)**

---

```
*DATABASE_RBDOUT
$    dt
      0.0001
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Revolute Joint
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONSTRAINED_JOINT_REVOLUTE
$
$ Create a revolute joint between two rigid bodies.  The rigid bodies must
$ share a common edge to define the joint along.  This edge, however, must
$ not have the nodes merged together.  Rigid bodies A and B will rotate
$ relative to each other along the axis defined by the common edge.
$
$ Nodes 1 and 2 are on rigid body A and coincide with nodes 9 and 10
$ on rigid body B, respectively.  (This defines the axis of rotation.)
$
$ The relative penalty stiffness on the revolute joint is to be 1.0,
$ the joint is well lubricated, thus no damping at the joint is supplied.
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$    n1      n2      n3      n4      n5      n6      rps      damp
$      1      9      2      10      1.0
$
$
$
$$$$$$$$$$$$$$$$ Define a joint stiffness for the revolute joint described above.
$
$ Attributes of the joint stiffness:
$ - Used for defining a stop angle of 30 degrees rotation
$   (i.e., the joint allows a positive rotation of 30 degrees and
$   then imparts an elastic stiffness to prevent further rotation)
$ - Define between rigid body A (part 1) and rigid body B (part 2)
$ - Define a local coordinate system along the revolute axis
$   on rigid body A - nodes 1, 2 and 3 (cid = 5).  This is used to
$   define the revolute angles phi (PH), theta (T), and psi (PS).
$ - The elastic stiffness per unit radian for the stop angles
$   are 100, 10, 10 for PH, T, and PS, respectively.
$ - Values not specified are not used during the simulation.
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONSTRAINED_JOINT_STIFFNESS_GENERALIZED
$    jsid    pidA    pidB    cidA    cidB
$      1      1      2      5      5
$
$    lcidPH   lcidT   lcidPS   dlcidPH   dlcidT   dlcidPS
$
$
$    esPH     fmPS     esT      fmT      esPS     fmPS
$    100.0    10.0    10.0    10.0    10.0
$
$    nsAPH    psaPH     nsAT     psaT     nsAPS    psaPS
$             30.0
$
$
*DEFINE_COORDINATE_NODES
$    cid     n1      n2      n3
```

---





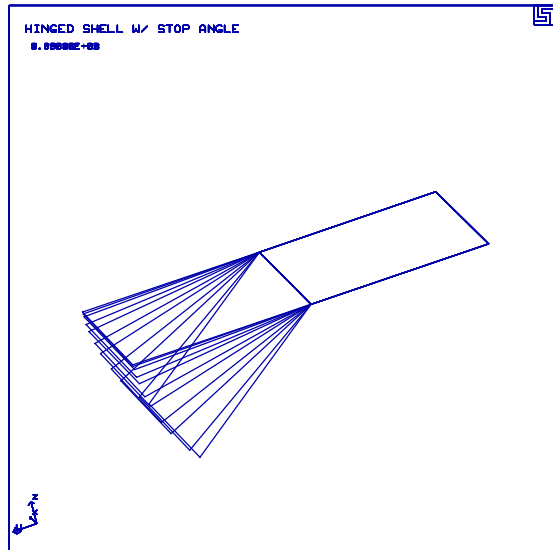
# \*CONSTRAINED\_JOINT\_REVOLUTE

## Hinged Shell with Stop Angle (Revolute Joint)

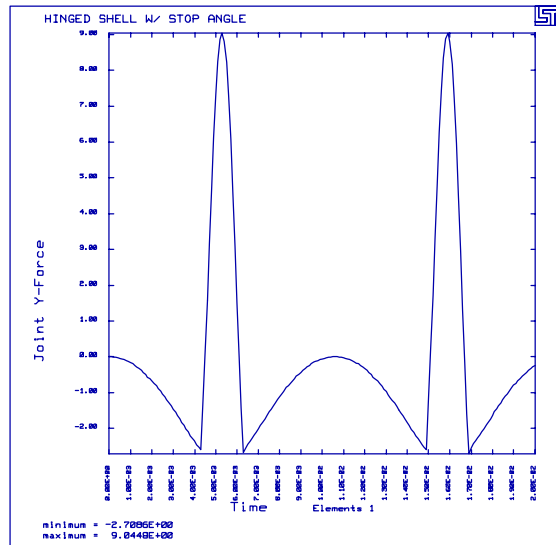
---

### Results:

taurus g=d3plot  
angle 1 rz 90 rx -45 ry 30 rx -15 rz 30 ry -20 s 1 v s 3 over v  
s 5 over v ...repeat for all odd states up to ... s 21 over v



phs3  
jntforc  
y-force



**LS-DYNA Manual Section:** \*CONSTRAINED\_LINEAR

**Additional Sections:**

BOUNDARY\_PRESCRIBED\_MOTION\_NODE  
DEFINE\_CURVE

**Example:** Linearly Constrained Plate

**Filename:** constrained.linear.plate.k

**Description:**

The center node of a plate moves in the normal direction. Two other nodes that are neighbors to the center node are constrained such that their displacement in the normal direction is identical.

**Model:**

The plate is made of an elastic material measuring  $40 \times 40 \times 2 \text{ mm}^3$  and contains 64 Hughes-Liu shell elements. The center node displacement increases linearly. At the termination time, 0.0005 seconds, the displacement is 15 mm. The degree of freedom in the z-direction for the two nodes is identical.

**Input:**

A load curve defines the magnitude of the prescribed displacement of the center node (\*BOUNDARY\_PRESCRIBED\_MOTION\_NODE, \*DEFINE\_CURVE). A linear constraint card defines the coupling of the displacement in the z-direction between the two nodes (\*CONSTRAINED\_LINEAR). Two equal coefficients with opposite signs control the displacement.

**Reference:**

Schweizerhof, K. and Weimer, K.



**\*CONSTRAINED\_LINEAR**  
 Linearly Constrained Plate

```

$          dt
      0.00001
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Constraints and Boundary Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1.>....2.>....3.>....4.>....5.>....6.>....7.>....8
$
$$$$$  nodes 40 and 42 are constrained to have identical z-direction motion
$
*CONSTRAINED_LINEAR
$      num
      2
$
$      nid      dofx      dofz      dofrx      dofry      dofz      coef
      40              1              1              1              1.00
      42              1              1              1              -1.00
$
$
$$$$$  node 41 is displaced in the z-direction according to load curve 1
$
*BOUNDARY_PRESCRIBED_MOTION_NODE
$      nid      dof      vad      lcid      sf      vid
      41          3          2          1          1.0
$
*DEFINE_CURVE
$      lcid      sidr      scla      sclo      offa      offo
      1
$
$          abscissa          ordinate
              0.0              0.0
              0.0005          -15.0
              0.0015          -15.1
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
*PART
Impacted Material
$      pid      sid      mid      eosid      hgid      adpopt
      1          1          1          0          0          0
$
$
$$$$$$$  Materials
$
*MAT_ELASTIC
$      mid      ro      e      pr      da      db      k
      1          2.00e-8  100000.0  0.300
$
$
$$$$$$$  Sections
$
*SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icomp
      1          6          0.83333      2.0      3.0
$
$      t1      t2      t3      t4      nloc
  
```



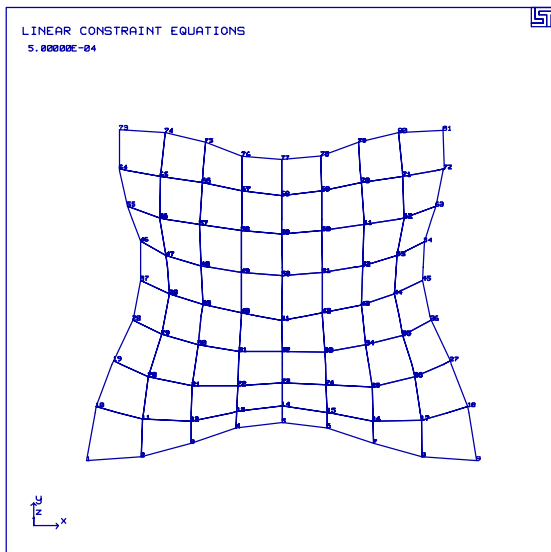


# \*CONSTRAINED\_LINEAR

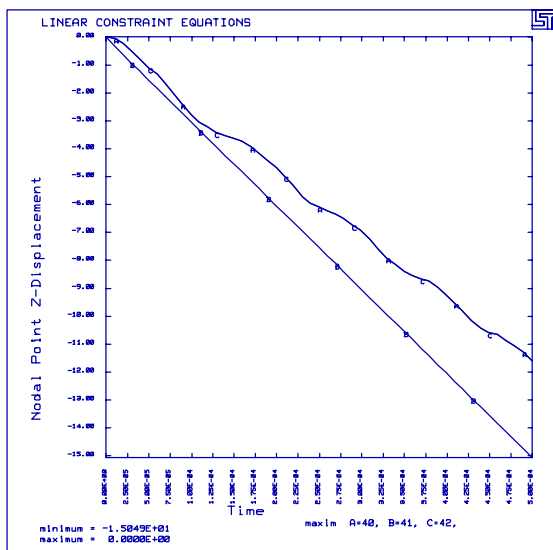
## Linearly Constrained Plate

### Results:

taurus g=d3plot  
19  
time 5e-4 rx -20 ndplt



phs3  
nodout  
z-disp



**\*CONSTRAINED\_LINEAR**  
Linearly Constrained Plate

---

## **\*CONSTRAINED\_SHELL\_TO\_SOLID** Impulsively Loaded Cap with Shells and Solids

---

**LS-DYNA Manual Section:** \*CONSTRAINED\_SHELL\_TO\_SOLID

**Additional Sections:**

\*LOAD\_SEGMENT

**Example:** Impulsively Loaded Cap with Shells and Solids

**Filename:** constrained.shell\_solid.dome.k

**Description:**

A dome has an impulsive pressure load. The dome contains shell and brick element joined with shell-brick interfaces.

**Model:**

Only 1/4 of the dome is modeled due to symmetry. The dome shells are Hughes-Liu shell elements with three integration point through the thickness. Four shell elements have a pressure load of 5,308 psi over 0.0017246 square inches. The termination time is 0.0004 seconds.

**Input:**

The model contains one shell-brick group that has 7 shell nodes tied to 5 brick node (\*CONSTRAINED\_SHELL\_TO\_SOLID). The model contains four pressure surfaces (\*LOAD\_SEGMENT). Five nodes are written to the time history ASCII database file nodout (\*DATABASE\_HISTORY\_NODE, \*DATABASE\_NODOUT).

**Results:**

The plots show the response of the dome.

**Reference:**

T. Littlewood





**\*CONSTRAINED\_SHELL\_TO\_SOLID**  
**Impulsively Loaded Cap with Shells and Solids**

---

```

$
*SET_NODE_LIST
$   sid      da1      da2      da3      da4
$       5
$   nid1     nid2     nid3     nid4     nid5     nid6     nid7     nid8
$   120     162     204     246     288
$
$
$
*CONSTRAINED_SHELL_TO_SOLID
$   nid      nsid
$   331      6
$
*SET_NODE_LIST
$   sid      da1      da2      da3      da4
$       6
$   nid1     nid2     nid3     nid4     nid5     nid6     nid7     nid8
$   121     163     205     247     289
$
$
$
*CONSTRAINED_SHELL_TO_SOLID
$   nid      nsid
$   332      7
$
*SET_NODE_LIST
$   sid      da1      da2      da3      da4
$       7
$   nid1     nid2     nid3     nid4     nid5     nid6     nid7     nid8
$   122     164     206     248     290
$
$
$
$$$$$ Define Loads
$
$$$$$ Load 4 segments with pressure at 5,308 psi for 2.0E-04 seconds
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*LOAD_SEGMENT
$   lcid      sf        at         n1         n2         n3         n4
$       1 1.000E+00 0.000E+00         1         2         4         3
$       1 1.000E+00 0.000E+00         2         5         7         4
$       1 1.000E+00 0.000E+00         3         4         8         6
$       1 1.000E+00 0.000E+00         4         7         9         8
$
$
*DEFINE_CURVE
$   lcid      sidr      scla      sclo      offa      offo
$       1
$
$
$       a           o
$       0.000E+00         5.308E+04
$       2.000E-04         5.308E+04
$       2.010E-04         0.000E+00
$       1.000E+00         0.000E+00
$
$$$$$ Define Parts and Materials
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8

```

---



**\*CONSTRAINED\_SHELL\_TO\_SOLID**  
**Impulsively Loaded Cap with Shells and Solids**

---

```

.
202      2      280      281      44      43      322      323      21      20
203      2      281      282      45      44      323      324      22      21
204      2      282      283      46      45      324      325      23      22
$
$$$$$ Elements - Shells
$
*ELEMENT_SHELL
$  eid      pid      n1      n2      n3      n4
   1         3      326      333      334      327
   2         3      327      334      335      328
   3         3      328      335      336      329
.
... in total, 60 shells defined
.
58         3      392      399      400      393
59         3      393      400      401      394
60         3      394      401      402      395
$
*END

```

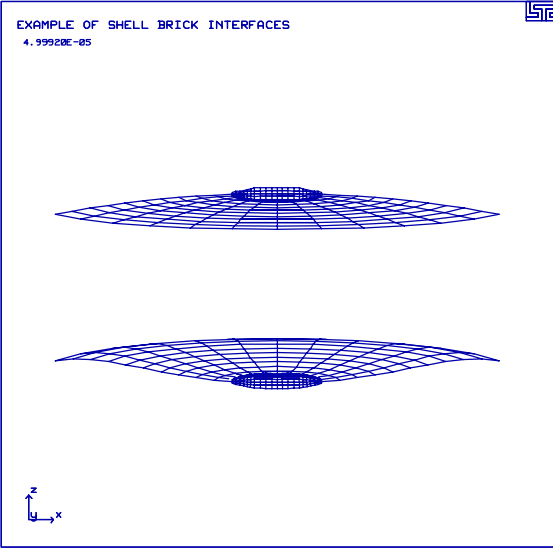


# \*CONSTRAINED\_SHELL\_TO\_SOLID

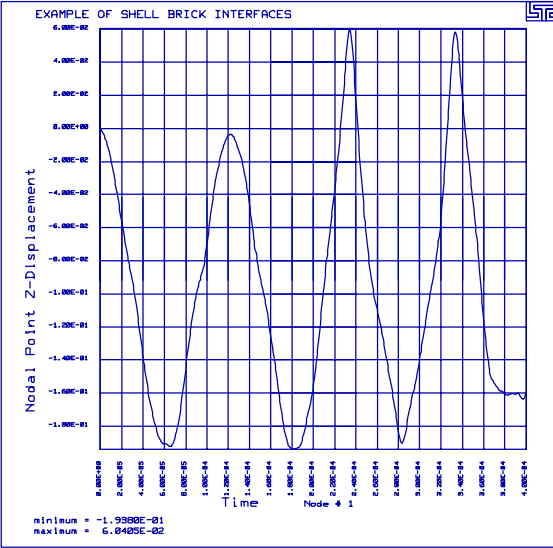
## Impulsively Loaded Cap with Shells and Solids

**Results:**

```
taurus g=d3plot  
19  
rayz rx -90 center ytran .3 v ytran -.6 s 6 over v
```



```
phs3  
nodout  
grid z-disp  
1
```



**\*CONSTRAINED\_SHELL\_TO\_SOLID**  
Impulsively Loaded Cap with Shells and Solids

---

**LS-DYNA Manual Section:** \*CONSTRAINED\_SPOTWELD

**Additional Sections:**

\*BOUNDARY\_PRESCRIBED\_MOTION\_SET  
\*DATABASE\_CROSS\_SECTION\_PLANE  
\*DATABASE\_CROSS\_SECTION\_SET

**Example:** Spot Weld Secures Two Plates

**Filename:** constrained.spotweld.plates.k

**Description:**

Two overlapping plates are connected using three spotwelds. The plates are pulled apart until the spot welds reach the defined failure condition.

**Model:**

The two plates measure  $80 \times 40 \times 1 \text{ mm}^3$  and are defined with S/R Hughes-Liu shell elements to control hourglassing. The location of the spotwelds connecting the two plates is in the center of the overlapping section. One end of the plate has fixed constraints and the other end of the other plate has linearly increasing displacement.

**Input:**

The nodal point cards contain the boundary conditions at one end of the plate (\*NODES). \*BOUNDARY\_PRESCRIBED\_MOTION\_SET defines the nodal motion of the end of the other plate. Massless beams simulate the connection between the plates at three locations (\*CONSTRAINED\_SPOTWELD). The definitions include failure as a function of the axial and shear force.

The ASCII file swforc contains the axial and shear forces on the spotweld (\*DATABASE\_SWFORC). A cross section is defined through each of the plates using two different techniques (\*DATABASE\_CROSS\_SECTION\_PLANE, \*DATABASE\_CROSS\_SECTION\_SET). Forces and moments through the cross sections are stored in the ASCII file secforc (\*DATABASE\_SECFORC).



**\*CONSTRAINED\_SPOTWELD**  
Spot Weld Secures Two Plates

```

201
$
*SET_NODE_LIST
$   sid
    201
$   nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
    213      123
$
*DATABASE_NODOUT
$   dt
    0.010
$
*DATABASE_HISTORY_NODE
$   id1      id2      id3      id4      id5      id6      id7      id8
    123      233
$
*DATABASE_SECFORC
$   dt
    0.010
$
*DATABASE_SWFORC
$   dt
    0.010
$
$
$$$$ Constrain the Plates Together
$
$$$$ Three spotwelds across the plate, with failure defined.
$
*CONSTRAINED_SPOTWELD
$   n1      n2      sn      sf      n      m
    212      122      7.854    4.534    2.0    2.0
    213      123      7.854    4.534    2.0    2.0
    214      124      7.854    4.534    2.0    2.0
$
$
$$$$ Boundary Motion Conditions
$
$$$$ Prescribe the velocity of the nodes on one end of the plate.
$
*BOUNDARY_PRESCRIBED_MOTION_SET
$   nid      dof      vad      lcid      sf      vid
    1         1         0         1         1.0     0
$
*DEFINE_CURVE
$   lcid      sidr      scla      sclo      offa      offo
    1
$   abscissa      ordinate
        0.0000      0.0
        10.0000     0.3048
        20.0000     0.3048
$
*SET_NODE_LIST
$   sid
    1

```



**\*CONSTRAINED\_SPOTWELD**  
**Spot Weld Secures Two Plates**

```

*DATABASE_CROSS_SECTION_PLANE
$      psid      xct      yct      zct      xch      ych      zch
        0        30.0      0.0      0.0      31.0      0.0      0.0
$      xhev      yhev      xhev      len1      lenm
        30.0      1.0        0.0
$
$$$  cross section through plate 2
$
*DATABASE_CROSS_SECTION_SET
$      nsid      hsid      bsid      ssid      tsid      dsid
        4
$
*SET_NODE_LIST
$      sid      da1      da2      da3      da4
        4
$      nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
        226      227      228      229      230
$
*SET_SHELL_LIST
$      sid      da1      da2      da3      da4
        2
$      eid1      eid2      eid3      eid4      eid5      eid6      eid7      eid8
        221      222      223      224
$
$
$$$$$ Define Nodes and Elements
$
$$$$$
$
*NODE
$      node      x      y      z      tc      rc
        101      0.000000E+00  0.000000E+00  0.000000E+00  7      0
        102      0.000000E+00  1.000000E+01  0.000000E+00  7      0
        103      0.000000E+00  2.000000E+01  0.000000E+00  7      0
        .
        ... in total, 70 nodes defined
        .
        233      1.200000E+02  2.000000E+01  2.000000E+00  5      0
        234      1.200000E+02  3.000000E+01  2.000000E+00  5      0
        235      1.200000E+02  4.000000E+01  2.000000E+00  5      0
$
$$$$$ SHELL ELEMENTS
$
*ELEMENT_SHELL
$      eid      pid      n1      n2      n3      n4
        101      1      107      102      101      106
        102      1      108      103      102      107
        103      1      109      104      103      108
        .
        ... in total, 48 shells defined
        222      2      233      228      227      232
        223      2      234      229      228      233
        224      2      235      230      229      234
$
*END

```

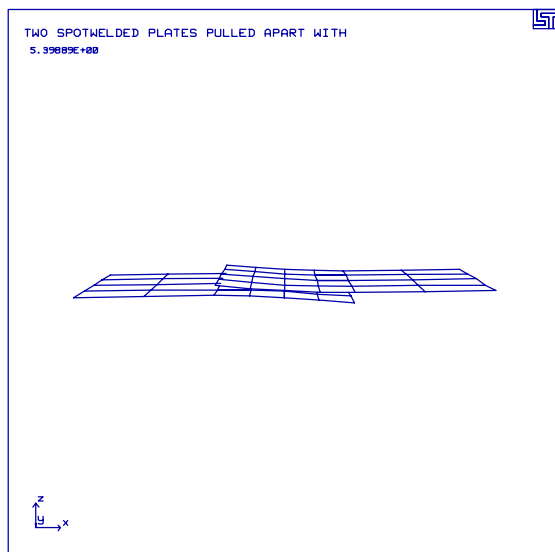
# \*CONSTRAINED\_SPOTWELD

## Spot Weld Secures Two Plates

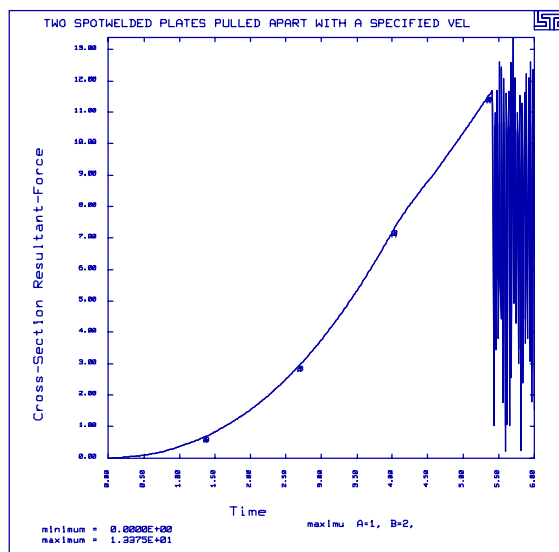
---

### Results:

taurus g=d3plot  
19  
rx -80 state 28 view



phs3  
secforc  
aset 0 6 r-forc





**LS-DYNA Manual Section: \*CONTACT****Additional Sections:**

\*INITIAL\_VELOCITY

**Example:** Shell Rebounds from Plate Using Five Contact Types

**Filename:** contact.plates.k

**Description:**

A shell element drops and rebounds on an elastic plate.

**Model:**

The plate measures  $40 \times 40 \times 1 \text{ mm}^3$  and contains 16 shell elements. The dropped shell element has a side length of 10 mm, a thickness of 2 mm and drop height of 10 mm. All shell elements are elastic with Belytschko-Tsay formulation. The dropped shell element has an initial velocity of 100,000 mm/second vertically towards the plate. The calculations terminate at 0.0002 seconds.

**Input:**

All four nodes of the dropped shell element have an initial velocity specified by \*INITIAL\_VELOCITY. Contact types 3, 5 and 10 use the dropped shell element as slave side and the four shell elements in the center of the plate as master side. The example file has type 3 contact activated, while the other contact types are commented out. To change contact types, simply comment out type 3 and un-comment the desired contact.

Type 3 contact is a two way surface to surface algorithm. The segments on the slave side are checked for penetration of the master segment then the opposite search takes place.

Type 4 is a single surface algorithm. The nodes of all segments are checked for penetration of all segments.

Type 5 is a node to surface one way algorithm. The program checks that no slave node penetrates any master segment.

Type 10 converts surface to surface definition into a node to surface definition.

Type 13 is a more robust version of the single surface algorithm.

**Reference:**

Schweizerhof, K. and Weimer, K.

---





# \*CONTACT

## Shell Rebounds from Plate Using Five Contact Types

---

```
$$      1
$      n1      n2      n3      n4
$$     101     103     104     102
$$      7      8      13     12
$$      8      9      14     13
$$     12     13     18     17
$$     13     14     19     18
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$$$$$$$$ Type 5, node to surface
$      to make active, remove the $$ from the lines below
$
$$*CONTACT_NODES_TO_SURFACE
$      ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
$$      1      2      4      1      1
$      fs      fd      dc      vc      vdc      penchk      bt      dt
$$
$      sfs      sfm      sst      mst      sfst      sfmt      fsf      vsf
$$
$
$$*SET_NODE_LIST
$      sid
$$      1
$      nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
$$      101      103      104      102
$
$$*SET_SEGMENT
$      sid
$$      2
$      n1      n2      n3      n4
$$      7      8      13     12
$$      8      9      14     13
$$     12     13     18     17
$$     13     14     19     18
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$$$$$$$$ Type 10, surface to surface
$      to make active, remove the $$ from the lines below
$
$$*CONTACT_ONE_WAY_SURFACE_TO_SURFACE
$      ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
$$      1      2      1      1
$      fs      fd      dc      vc      vdc      penchk      bt      dt
$$
$      sfs      sfm      sst      mst      sfst      sfmt      fsf      vsf
$$
$
$$*SET_SEGMENT
$      sid
$$      1
$      n1      n2      n3      n4
$$     101     103     104     102
$
$$*SET_SEGMENT
$      sid      da1      da2      da3      da4
$$      2
$      n1      n2      n3      n4
$$      7      8      13     12
$$      8      9      14     13
$$     12     13     18     17
$$     13     14     19     18
```

**\*CONTACT**

**Shell Rebounds from Plate Using Five Contact Types**

```

$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$$$$$$$ Type 13, automatic single surface
$
                to make active, remove the $$ from the lines below
$
$$*CONTACT_AUTOMATIC_SINGLE_SURFACE
$
  ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
$$
  0         0
$
  fs        fd        dc         vc         vdc        penchk      bt        dt
$$
  sfs       sfm       sst        mst        sfst       sfmt        fsf       vsf
$$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Initial Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Nodes of the Impactor Material are given an initial velocity.
$
*INITIAL_VELOCITY
$
  nsid      nsidex      boxid
$
  1
$
  vx        vy          vz
$
  0.0       0.0     -100000.0
$
*SET_NODE_LIST
$
  sid
$
  1
$
  nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
$
  101       102       103       104
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*PART
$
  pid      sid      mid      eosid      hgid      adpopt
Impacted Material
$
  1        1        1
Impactor Material
$
  2        2        1
$
$
$
*MAT_ELASTIC
$
  mid      ro      e      pr      da      db      k
$
  1        1.00e-8  100000.0  0.300
$
$
*SECTION_SHELL
$
  sid      elform      shrf      nip      propt      qr/irid      icomp
$
  1                0.83333      2.0      3.0
$
  t1       t2       t3       t4       nloc
$
  1.0      1.0      1.0      1.0
$
$
*SECTION_SHELL
$
  sid      elform      shrf      nip      propt      qr/irid      icomp

```



**\*CONTACT**

**Shell Rebounds from Plate Using Five Contact Types**

---

16	1	19	20	25	24
101	2	101	102	104	103

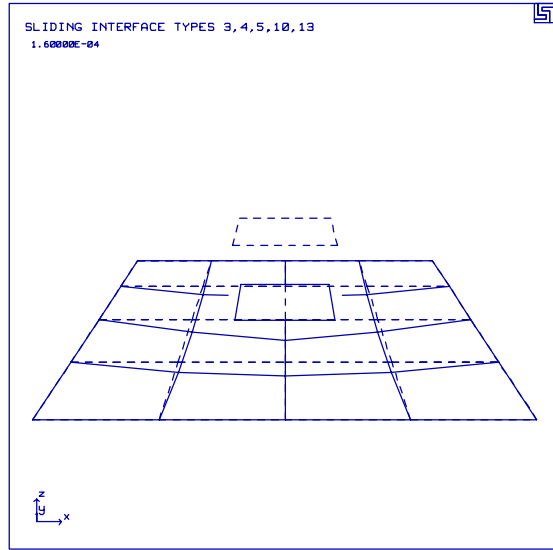
\$  
\*END

# \*CONTACT

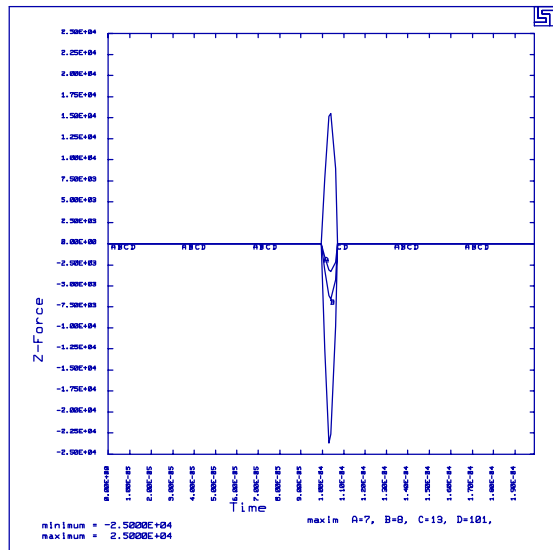
## Shell Rebounds from Plate Using Five Contact Types

### Results:

taurus g=d3plot  
19  
udg 1 time 1.6e-4 rx -70 view



phs3  
ncforc  
oset -2.5e4 2.5e4 z-forc 7 8 13 101





## **\*CONTACT\_ERODING\_SURFACE\_TO\_SURFACE** Projectile Penetrates Plate

---

**LS-DYNA Manual Section:** \*CONTACT\_ERODING\_SURFACE\_TO\_SURFACE

**Additional Sections:**

\*INITIAL\_VELOCITY\_GENERATION

**Example:** Projectile Penetrates Plate

**Filename:** contact.projectile.k

**Description:**

A projectile strikes a plate at a critical angle.

**Model:**

The hemispherical projectile has a length of 7.67 cm and a diameter of 0.767 cm. The plate measures 23.01 cm × 23 cm × 0.64 cm. The projectile and the plate are elastic perfectly plastic with failure strain. The initial velocity of the projectile is 0.129 cm/μsec at an angle of 75 degrees. The calculation terminates at 110.0 μsec.

**Input:**

The initial velocity (magnitude and direction) of the projectile is set using \*INITIAL\_VELOCITY\_GENERATION. Eroding contact between the projectile surface and plate surface is defined so that the contact erodes as the element erodes (\*CONTACT\_ERODING\_SURFACE\_TO\_SURFACE). This allows the contact to work correctly as layers of the parts erode during penetration.

**Results:**

The projectile fractures into a tip and trailing portion. The trailing portion punches a hole through the plate while the tip deflects off the plate.





# \*CONTACT\_ERODING\_SURFACE\_TO\_SURFACE

## Projectile Penetrates Plate

---

```

      1      1      1
Plate  2      1      2

```

```

$
$
$$$$$ Materials
$
$$$$ failure strain for erosion of the projectile and plate elements are
$$$$ set as: fs = 0.8

```

```

$
*MAT_PLASTIC_KINEMATIC
$  mid      ro      e      pr      sigy      etan      beta
   1  1.862E+01  1.170E+00  0.22  1.790E-02           1.0
$  src      srp      fs
              0.8

```

```

$
*MAT_PLASTIC_KINEMATIC
$  mid      ro      e      pr      sigy      etan      beta
   2  7.896E+00  2.100E+00  0.284  1.000E-02           1.0
$  src      srp      fs
              0.8

```

```

$$$$$ Sections

```

```

$
*SECTION_SOLID
$  sid      elform
   1      0

```

```

$$$$$

```

```

$$$$$ Define Nodes and Elements

```

```

$$$$$

```

```

$
*NODE
$  node      x      y      z      tc      rc
   1  9.241751E+00  -1.534000E-05  5.137928E-02  2      6
   2  9.193813E+00  0.000000E+00  1.344095E-01  2      6
   3  9.145876E+00  0.000000E+00  2.174397E-01  2      6
   .
   ... in total, 7668 nodes defined
   .
  7666  1.918446E+01  4.800000E+00  0.000000E+00  7      7
  7667  2.071067E+01  4.800000E+00  0.000000E+00  7      7
  7668  2.300000E+01  4.800000E+00  0.000000E+00  7      7

```

```

$$$$$ Elements

```

```

$
*ELEMENT_SOLID
$  eid      pid      n1      n2      n3      n4      n5      n6      n7      n8
   1      1      1      2      5      4      10     11     14     13
   2      1      2      3      6      5      11     12     15     14
   3      1      4      5      8      7      13     14     17     16
   .
   ... in total, 5664 solids defined
   .
  5662      2      7617     7618     7626     7625     7657     7658     7666     7665
  5663      2      7618     7619     7627     7626     7658     7659     7667     7666

```

---

**\*CONTACT\_ERODING\_SURFACE\_TO\_SURFACE**  
Projectile Penetrates Plate

---

5664            2        7619        7620        7628        7627        7659        7660        7668        7667  
\$  
\*END

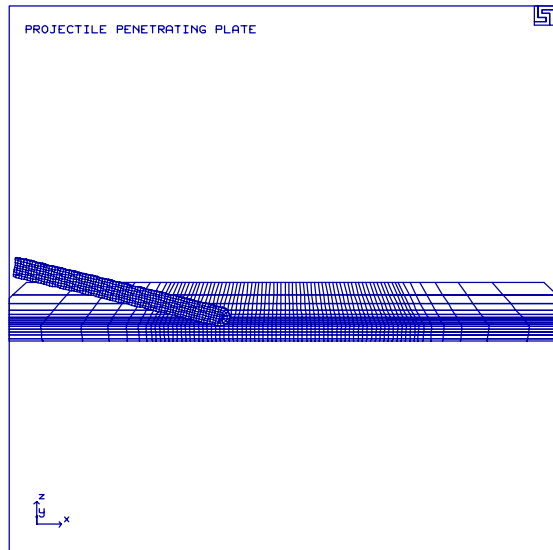
# \*CONTACT\_ERODING\_SURFACE\_TO\_SURFACE

## Projectile Penetrates Plate

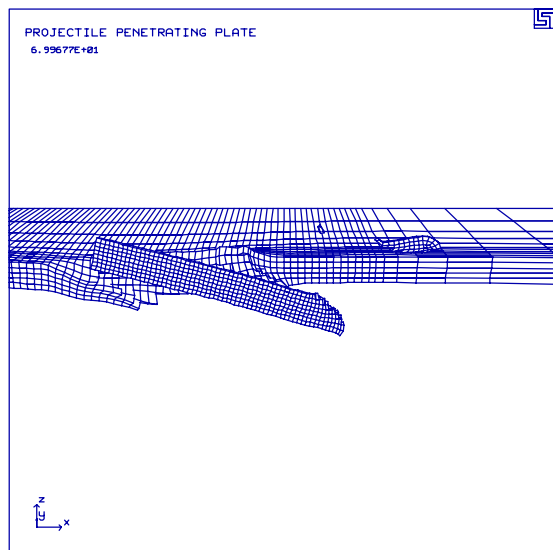
---

### Results:

taurus g=d3plot  
19  
rx -70 dist 27 view



state 8  
m 1 center  
dam view



## \*CONTACT\_NODES\_TO\_SURFACE

### Rigid Sphere Impacts a Plate at High Speed

---

**LS-DYNA Manual Section:** \*CONTACT\_NODES\_TO\_SURFACE

**Additional Sections:**

\*CONSTRAINED\_TIED\_NODES\_FAILURE

**Example:** Rigid Sphere Impacts a Plate at High Speed

**Filename:** contact.n2s-sphere.k

**Description:**

A sphere impacts a plate at high speed causing failure of the plate. This model can be used to show how different contacts can behave differently in a rather simple model. Instructions of this are explained in the header of the input deck.

**Model:**

A rigid sphere is made out of solid elements and given an initial velocity of 89 mm/ms towards a plate using the \*DEFINE\_BOX keyword. The plate is constructed out of shell elements. The shells of the plates do NOT have their nodes merged at common locations. Instead, tied nodes with failure constraints are used to connect the common nodes. This allows the plate to rupture and rip along seam lines instead of having elements fail (and being deleted) by using the more common failure criteria within the material definition.

**Results:**

The plate is definitely not made out of a bullet proof material.





**\*CONTACT\_NODES\_TO\_SURFACE**  
Rigid Sphere Impacts a Plate at High Speed

---

```
*DATABASE_BINARY_D3THDT
$   dt       lcdt
     999999
$
$
*DATABASE_GLSTAT
$   dt
     0.005
$
$
*DATABASE_MATSUM
$   dt
     0.005
$
$
*DATABASE_NODOUT
$   dt
     0.005
$
$
*DATABASE_HISTORY_NODE
$   id1      id2      id3      id4      id5      id6      id7      id8
     2633    362     489
$
$
*DATABASE_RBDOUT
$   dt
     0.005
$
$
*DATABASE_RCFORC
$   dt
     0.005
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Initial Velocity
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
*INITIAL_VELOCITY
$
$   nsid     nsidex   boxid
$               5
$
$   vx       vy       vz       wx       wy       wz
$   0.0     0.0    -89.0
$
*DEFINE_BOX
$
$   boxid     xmm     xmx     ymn     ymx     zmn     zmx
$         5   -39.0   39.0   -39.0   39.0   -25.41  51.0
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Define Contacts - sliding interface definitions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
*CONTACT_NODES_TO_SURFACE
$
$   ssid     msid     sstyp   mstyp   sboxid   mboxid   spr     mpr
$         2       3       3       3
$
$   fs       fd       dc       vc       vdc     penchk   bt     dt
$
$
```





# \*CONTACT\_NODES\_TO\_SURFACE

## Rigid Sphere Impacts a Plate at High Speed

---

```

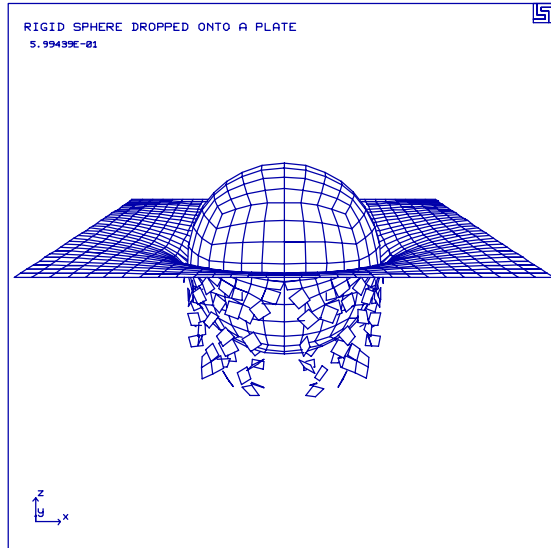
$
$$$$ Define Tied Nodes with Failure Constraints
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$ Tie all the adjacent corners of the shells together. Essentially, do
$$$$ a merge by way of tied nodes with failure.
$
*CONSTRAINED_TIED_NODES_FAILURE
$   nsid      eppf
    101      0.0850
$
*SET_NODE_LIST
$   sid
    101
    775      778      896      897
$
.
... in total, 841 CONSTRAINED_TIED_NODES_FAILURE/SET_NODE_LIST pairs defined
.
$
*CONSTRAINED_TIED_NODES_FAILURE
$   nsid      eppf
    941      0.0850
*SET_NODE_LIST
$   sid
    941
    4247      4250      4368      4369
*END

```

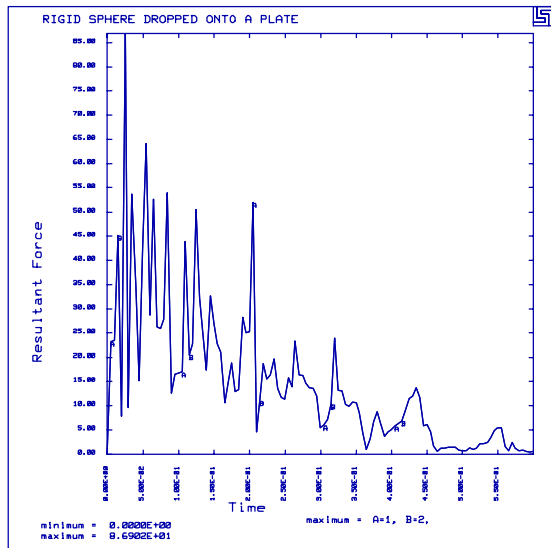
# \*CONTACT\_NODES\_TO\_SURFACE Rigid Sphere Impacts a Plate at High Speed

## Results:

taurus g=d3plot  
state 7 center  
rx -75 view



phs3  
rforc  
result



**\*CONTACT\_NODES\_TO\_SURFACE**  
Rigid Sphere Impacts a Plate at High Speed

---

**LS-DYNA Manual Section:** \*CONTACT\_SINGLE\_EDGE

**Additional Sections:**

\*CONTACT\_FORCE\_TRANSDUCER\_PENALTY

**Example:** Corrugated Sheet Contacts Edges

**Filename:** contact.edge.k

**Description:**

A corrugated plate strikes a flat plate from opposite directions.

**Input:**

The model consists of 135 elastic plastic Belytschko-Tsay shell elements. The interaction of the two structures is to edge contact (\*CONTACT\_SINGLE\_EDGE). A contact force transducer is defined to monitor the forces of the contact in the ascii file rforc. The nodes on the upper corrugated plate have an initial velocity of 10 meters/second.

**Results:**

A contour plot of the effective-stress and a plot of the forces from the ascii file rforc illustrate that the plates are in contact.

**Reference:**

Stillman, D. W.





**\*CONTACT\_SINGLE\_EDGE**  
Corrugated Sheet Contacts Edges

---

\$	sfs	sfm	sst	mst	sfst	sfmt	fsf	vsf
\$	*SET_SEGMENT							
\$	sid							
	1							
\$	n1	n2	n3	n4				
	1	2	0	0				
	2	3	0	0				
	3	13	0	0				
	13	14	0	0				
	14	21	0	0				
	21	22	0	0				
	22	29	0	0				
	29	30	0	0				
	30	37	0	0				
	37	38	0	0				
	38	45	0	0				
	45	46	0	0				
	46	53	0	0				
	53	54	0	0				
	54	61	0	0				
	61	62	0	0				
	69	70	0	0				
	70	71	0	0				
	71	72	0	0				
	72	73	0	0				
	73	74	0	0				
	74	75	0	0				
	75	76	0	0				
	76	77	0	0				
	77	78	0	0				
	78	79	0	0				
	79	80	0	0				
	80	81	0	0				
	81	82	0	0				
	111	112	0	0				
	112	113	0	0				
	113	114	0	0				
	114	115	0	0				
	115	116	0	0				
	116	117	0	0				
	117	118	0	0				
	118	119	0	0				
	119	120	0	0				
	120	121	0	0				
	121	122	0	0				
	122	123	0	0				
	123	124	0	0				
	125	126	0	0				
	126	127	0	0				
	127	137	0	0				
	137	138	0	0				
	138	145	0	0				
	145	146	0	0				
	146	153	0	0				
	153	154	0	0				
	154	161	0	0				
	161	162	0	0				
	162	169	0	0				
	169	170	0	0				
	170	177	0	0				
	177	178	0	0				

---

**\*CONTACT\_SINGLE\_EDGE**

**Corrugated Sheet Contacts Edges**

---

```

178      185      0      0
185      186      0      0

```

```

$
$$$ Force transducer defined to calculate contact forces on part 1.
$
*CONTACT_FORCE_TRANSDUCER_PENALTY
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$  ssid      msid      sstyp      mstyp
   5          2

```

```

$
*SET_PART_LIST
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
   5
   1

```

```

$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$ Initial Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$ Nodes of the part 1 (node set id = 2) are given an initial velocity
$$$ in the y-direction of 10 m/s.

```

```

$
*INITIAL_VELOCITY
$  nsid      nsidex      boxid
   2
$  vx        vy        vz        vxr        vyr        vzy
   0.0       10.0       0.0       0.0       0.0       0.0

```

```

$
*SET_NODE_LIST
$  sid
   2
$  nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
   1         2         3         4         5         6         7         8
   9        10        11        12        13        14        15        16
  17        18        19        20        21        22        23        24
  25        26        27        28        29        30        31        32
  33        34        35        36        37        38        39        40
  41        42        43        44        45        46        47        48
  49        50        51        52        53        54        55        56
  57        58        59        60        61        62        63        64
  65        66        67        68

```

```

$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8

```

```

$
*PART
$  pid      sid      mid      eosid      hgid      adpopt
plate-1
   1         1         1
plate-2
   2         1         1
plate-3

```

---

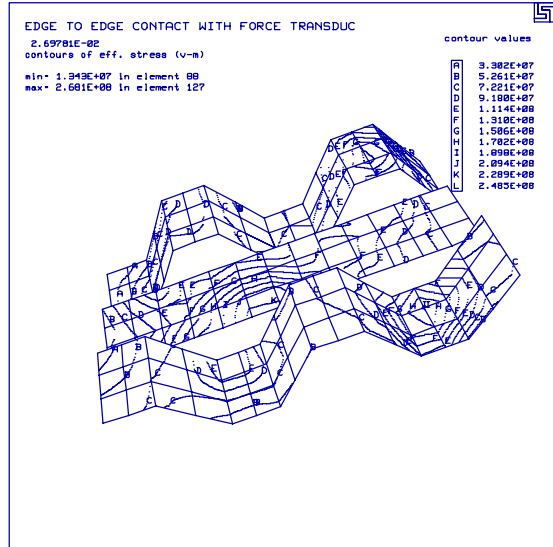


# \*CONTACT\_SINGLE\_EDGE

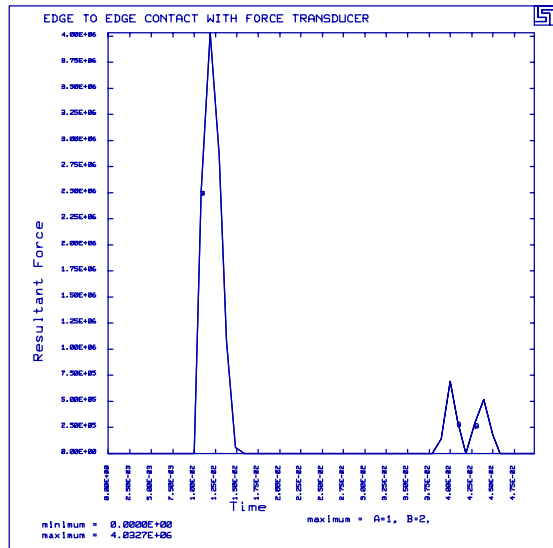
## Corrugated Sheet Contacts Edges

**Results:**

taurus g=d3plot  
 19  
 rx -40 rz 20 s 28 mono numc 12 contour 9



phs3  
 rforc  
 resultant



## \*CONTACT\_TIED\_NODES\_TO\_SURFACE

### Discrete Nodes Tied to a Surface

---

#### **LS-DYNA Manual Section:** \*CONTACT\_TIED\_NODES\_TO\_SURFACE

**Example:** Discrete Nodes Tied to a Surface

**Filename:** contact.tied\_nodes.box.k

#### **Description:**

A shell element drops onto and then rebounds from, a hollow box that is tied to an elastic plate.

#### **Model:**

The plate measures  $40 \times 40 \times 1 \text{ mm}^3$  and contains 16 Belytschko-Tsay shell elements. The dropped shell element has a side length of 10 mm, a thickness of 2 mm and a drop height of 10 mm. The box contains 12 Belytschko-Tsay shell elements. All shell element materials are elastic. The initial velocity of the shell elements is 100,000 mm/second. The calculation terminates at 0.002 seconds.

#### **Input:**

The nodes of the dropped shell are given an initial velocity (\*INITIAL\_VELOCITY). The nodes on the bottom of the box, those facing the plate, are tied to the plate (\*CONTACT\_TIED\_NODES\_TO\_SURFACE). Automatic single surface contact is used to define the contact between the dropped shell and the box.

#### **Reference:**

Schweizerhof, K. and Weimer, K.

# \*CONTACT\_TIED\_NODES\_TO\_SURFACE

## Discrete Nodes Tied to a Surface

---

### List of LS-DYNA input deck:

```
*KEYWORD
*TITLE
Sliding Interface Type 6
$
$  LSTC Example
$
$  Last Modified: September 5, 1997
$
$  A box is tied to a bottom plate with tied nodes to surface contact.
$  This box is impacted by a shell element, which has an initial velocity.
$
$  Units: mm, s
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
*CONTROL_TERMINATION
$  endtim  endcyc    dtmin  endneg  endmas
   0.200E-03
$
*CONTROL_HOURLASS
$    ihq      qh
     4
$
$
$
*DATABASE_BINARY_D3PLOT
$  dt      lcdt
   0.010E-03
$
*DATABASE_BINARY_D3THDT
$  dt      lcdt
   .0005E-03
$
$
$
*DATABASE_NODOUT
$  dt
   .0010E-03
$
*DATABASE_HISTORY_NODE
$  id1      id2      id3      id4      id5      id6      id7      id8
    101      13      213
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Define Contacts
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$. . . > . . . 1 . . . > . . . 2 . . . > . . . 3 . . . > . . . 4 . . . > . . . 5 . . . > . . . 6 . . . > . . . 7 . . . > . . . 8
$
$
*CONTACT_AUTOMATIC_SINGLE_SURFACE
$  ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
     0
$  fs      fd      dc      vc      vdc      penchk      bt      dt
$  sfs      sfm      sst      mst      sfst      sfmt      fsf      vsf
```

## \*CONTACT\_TIED\_NODES\_TO\_SURFACE

### Discrete Nodes Tied to a Surface

```

$
$
$$$$$$$$ The nodes on the bottom of the box (part 2) are tied to
$$$$$$$$ the bottom plate (part 1).
$
*CONTACT_TIED_NODES_TO_SURFACE
$      ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
$         2         1         4         3         1         1
$
$      fs      fd      dc      vc      vdc      penchk      bt      dt
$
$      sfs      sfm      sst      mst      sfst      sfmt      fsf      vsf
$
$
*SET_NODE_LIST
$      sid      da1      da2      da3      da4
$         2
$      nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
$      201      202      203      204      206      207      208      209
$
$$$$$$$$
$
$$$$ Initial Conditions
$
$$$$$$$$
$
$$$$ Nodes of the dropped shell are given an initial velocity.
$
*INITIAL_VELOCITY
$      nsid      nsidex      boxid
$         3
$      vx      vy      vz
$      0.0      0.0 -100000.0      0.0      0.0      0.0
$
*SET_NODE_LIST
$      sid
$         3
$      nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
$      101      102      103      104
$
$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$      pid      sid      mid      eosid      hgid      adpopt
bottom plate
$         1         1         1
dropped shell
$         2         2         1
box
$         3         1         1
$
$
*MAT_ELASTIC
$      mid      ro      e      pr      da      db      k
$         1 1.00e-08 100000. 0.300
$

```

# \*CONTACT\_TIED\_NODES\_TO\_SURFACE

## Discrete Nodes Tied to a Surface

---

```
$
*SECTION_SHELL
$   sid   elform   shrf   nip   propt   qr/irid   icomp
$     1     1       0.83333   2     propt   qr/irid   icomp
$   t1     t2     t3     t4     nloc
$     1.0     1.0     1.0     1.0
$
*SECTION_SHELL
$   sid   elform   shrf   nip   propt   qr/irid   icomp
$     2     1       0.83333   2     propt   qr/irid   icomp
$   t1     t2     t3     t4     nloc
$     2.0     2.0     2.0     2.0
$
$$$$$ Define Nodes and Elements
$
$$$$$ Outer edge nodes of the bottom plate (part 1)
$$$$$ are fixed in translation (tc = 7)
$
*NODE
$   node      x      y      z      tc      rc
$     1  0.000000E+00  0.000000E+00  0.000000E+00  7  0
$     2  1.000000E+01  0.000000E+00  0.000000E+00  7  0
$     3  2.000000E+01  0.000000E+00  0.000000E+00  7  0
$     .
$     ... in total, 48 nodes defined
$     .
$    217  5.867900E+00  2.000000E+01  4.000000E+00  0  0
$    218  1.292890E+01  2.707110E+01  4.000000E+00  0  0
$    219  2.000000E+01  3.414210E+01  4.000000E+00  0  0
$
$$$$$ SHELL ELEMENTS
$
*ELEMENT_SHELL
$   eid   pid   n1   n2   n3   n4
$     1     1     1     2     7     6
$     2     1     2     3     8     7
$     3     1     3     4     9     8
$     .
$     ... in total, 29 shells defined
$     .
$    210     3    212    213    216    215
$    211     3    214    215    218    217
$    212     3    215    216    219    218
$
*END
```

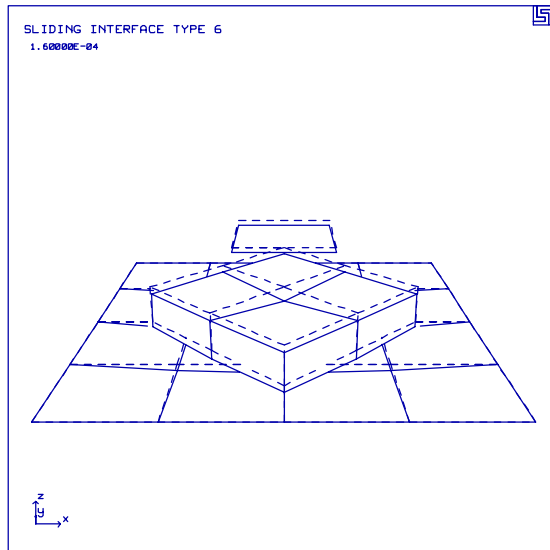


# \*CONTACT\_TIED\_NODES\_TO\_SURFACE

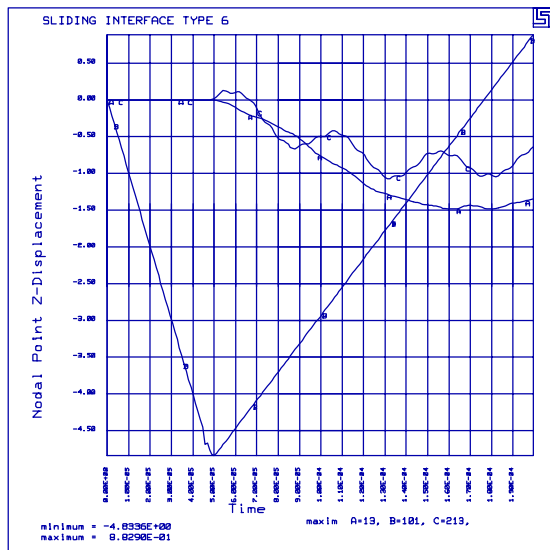
## Discrete Nodes Tied to a Surface

### Results:

taurus g=d3plot  
19  
udg 1 time 1.6e-4 rx -70 view



phs3  
nodout  
grid z-disp



## **\*CONTACT\_TIED\_NODES\_TO\_SURFACE**

Discrete Nodes Tied to a Surface

---

**LS-DYNA Manual Section:** \*CONTACT\_ENTITY

**Additional Sections:**

\*BOUNDARY\_PRESCRIBED\_MOTION\_RIGID

**Example:** Rigid Sphere Impacts Plate

**Filename:** contact\_entity.sphere.k

**Description:**

A rigid sphere drops onto an elastic plate. The sphere contains shell elements automatically generated with a “Geometric Contact Entity” spherical surface.

**Model:**

The plate of elastic material measures  $40 \times 40 \times 2 \text{ mm}^3$  and contains 64 Belytschko-Tsay shell elements. The sphere has a radius of 6.0 mm and the distance from the center of the cube to the plate is 8.5 mm. The inertia properties of the sphere are defined by the properties of the rigid brick element. A geometric contact entity defines the spherical contact surface. The sphere moves toward the plate with a uniform motion. The termination time is 0.0005 seconds.

**Input:**

The Geometric Contact Entity defines the outer master surface on the rigid sphere (\*CONTACT\_ENTITY). The nodes on the plate are slave nodes (\*SET\_NODE\_LIST), and are in the “Geometric Entity”. A load curve definition defines the movement of the sphere (\*BOUNDARY\_PRESCRIBED\_MOTION\_RIGID, \*DEFINE\_CURVE). The displacement condition for rigid bodies is input by part number, not by listing the nodes included in the definition.

**Reference:**

Schweizerhof, K. and Weimer, K.







**\*CONTACT\_ENTITY**  
**Rigid Sphere Impacts Plate**

---

```

      3    1.000000E+01    0.000000E+00    0.000000E+00    3    0
      .
      ... in total, 81 nodes defined
      .
      79    3.000000E+01    4.000000E+01    0.000000E+00    3    0
      80    3.500000E+01    4.000000E+01    0.000000E+00    3    0
      81    4.000000E+01    4.000000E+01    0.000000E+00    3    0
$
$$$$$ Elements
$
*ELEMENT_SHELL
$  eid      pid      n1      n2      n3      n4
   1         1         1         2         11        10
   2         1         2         3         12        11
   3         1         3         4         13        12
   .
   ... in total, 64 shells defined
   .
   62         1         69         70         79        78
   63         1         70         71         80        79
   64         1         71         72         81        80
$
*END

```

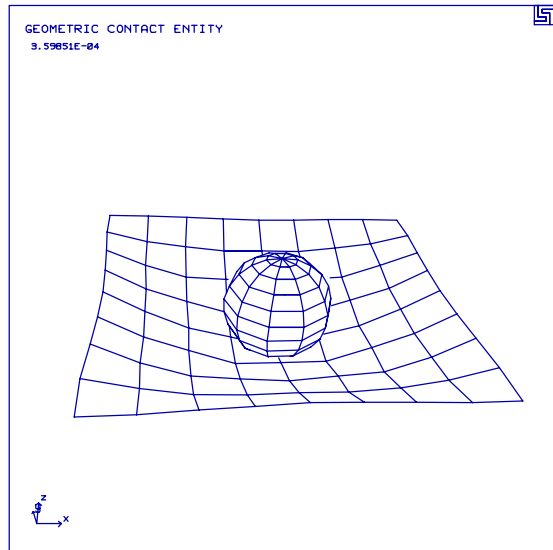
# \*CONTACT\_ENTITY

## Rigid Sphere Impacts Plate

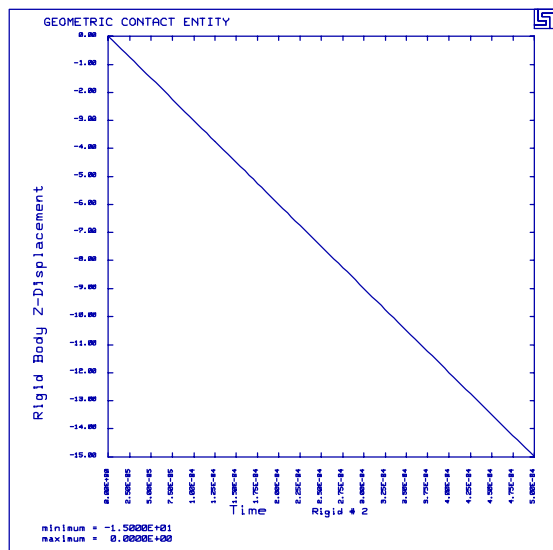
---

### Results:

taurus g=d3plot  
19  
rx -60 ry 10 ytrans 5 s 19 view



phs3  
rbdout  
oset -15 0 z-disp





**LS-DYNA Manual Section:** \*CONTROL\_CONTACT

**Additional Sections:**

\*LOAD\_SEGMENT  
\*MAT\_POWER\_LAW\_PLASTICITY  
\*RIGIDWALL\_PLANAR

**Example:** Hemispherical Punch

**Filename:** control\_contact.hemi-draw.k

**Description:**

This problem includes three tools a punch, a pressure pad, a die and a workpiece. A workpiece is deep drawn by the hemispherical punch while the pressure pad and die prevents wrinkling. The load on the pressure pad is ramped, then the punch displaces in the y direction.

**Model:**

The workpiece measures 80 mm in radius and 1 mm in thickness. The punch radius is 50.0 mm and the die torus radius is 6.35 mm. The workpiece contains 528 Belytschko Tsay shell elements with 5 integration points through the thickness. The tools are rigid members. Only 1/4 of the system is modeled because of symmetry.

**Input:**

The number of integration points is 5 for the workpiece. (\*SECTION\_SHELL) This model contains two options to consider shell thickness. The first option is the contact surfaces are projected to the true surface of shell (\*CONTROL\_CONTACT). The second option is membrane straining results in thickness changes (\*CONTROL\_CONTACT). The motion of the punch follows a sine function represented by load curve number 2 (Section 22).

**Reference:**

Honecker, A. and Mattiason, K.











**\*CONTROL\_CONTACT**  
**Hemispherical Punch**

---

```

1597    0.000000E+00   -5.000533E-01   -7.462286E+01    7    7
1598    0.000000E+00   -5.000534E-01   -7.771143E+01    7    7
1599    0.000000E+00   -5.000535E-01   -8.080000E+01    7    7
$
$$$$$$$ SHELL ELEMENTS
$
*ELEMENT_SHELL
$   eid      pid      n1      n2      n3      n4
   1         1         1         8         9         2
   2         1         2         9        10         3
   3         1         3        10        11         4
   .
   ... in total, 1452 shells defined
   .
1450         4    1589    1596    1597    1590
1451         4    1590    1597    1598    1591
1452         4    1591    1598    1599    1592
*END

```

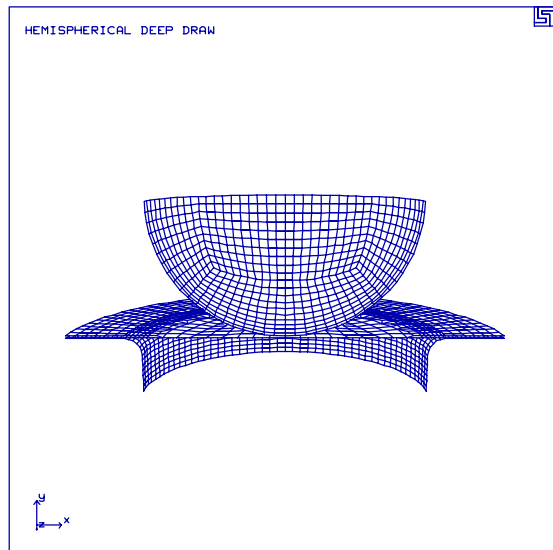
# \*CONTROL\_CONTACT

## Hemispherical Punch

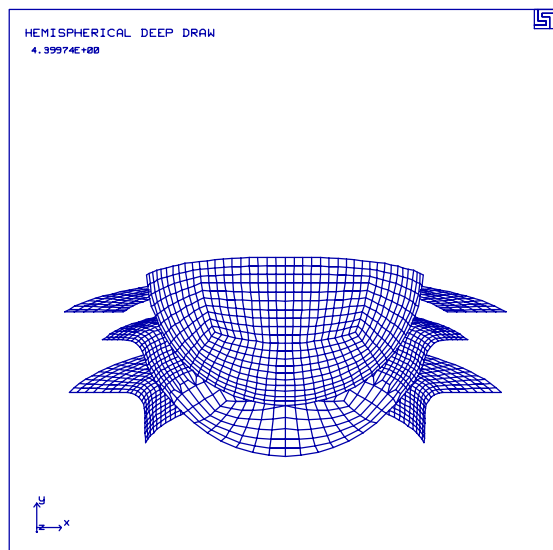
---

**Results:**

taurus g=d3plot  
19  
rx 10 rayz view



restore rx 10 state 23 explode 1 0 -20 0 1  
explode 1 0 10 0 3  
explode 1 0 20 0 4 rayz view





**LS-DYNA Manual Section:** \*CONTROL\_DAMPING

**Additional Sections:**

\*DAMPING\_GLOBAL  
\*DATABASE\_CROSS\_SECTION\_SET  
\*LOAD\_NODE\_SET

**Example:** Cantilever Beam

**Filename:** control\_damping.beam.k

**Description:**

A cantilever beam is subjected to a load at the free end. The beam then vibrates relative to the equilibrium position without damping in case 1 and with damping in case 2.

**Model:**

The beam measures  $1000 \times 100 \times 10 \text{ mm}^3$  and is modeled by 10 Belytschko-Tsay shell elements. A force of 100 N is applied in the z-direction at the free end. The calculation ends at 0.5 seconds.

**Input for the undamped system:**

The force at the free end is applied as two point forces. The size of these forces is controlled by load curve definition number 1 (\*DEFINE\_CURVE, \*LOAD\_NODE\_SET). The ASCII-files contain information for section force data, nodal information, and shell element information. Data from ASCII-files can be processed in phase 3 of LS-TAURUS.

**Input for the damped system:**

The same input as in the undamped case except for a global damping constant (\*DAMPING\_GLOBAL, \*CONTROL\_DAMPING).

**Reference:**

Schweizerhof, K. and Weimer, K.



**\*CONTROL\_DAMPING**  
**Cantilever Beam**

---

```

    4
$
*CONTROL_OUTPUT
$  npopt   neecho   nrefup   iaccop   opifs    ipnint   ikedit
     0       0       0         0         0         2       1000
$
*DATABASE_EXTENT_BINARY
$  neiph   neips   maxint   strflg   sigflg   epsflg   rltflg   engflg
     1         1
$  cmpflg   ieverp   beamip
$
*DATABASE_BINARY_D3PLOT
$  dt      lcdt
     0.020
$
*DATABASE_BINARY_D3THDT
$  dt      lcdt
     999999
$
*DATABASE_ELOUT
$  dt
     0.001
$
*DATABASE_HISTORY_SHELL
$  id1     id2     id3     id4     id5     id6     id7     id8
     1
$
*DATABASE_GLSTAT
$  dt
     0.001
$
*DATABASE_NODOUT
$  dt
     0.001
$
*DATABASE_HISTORY_NODE
$  id1     id2     id3     id4     id5     id6     id7     id8
     21
$
*DATABASE_SECFORC
$  dt
     0.001
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Cross Sections
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$$ define a cross section through the beam to monitor force & moment
$
*DATABASE_CROSS_SECTION_SET
$  nsid     hsid     bsid     ssid     tsid     dsid
     1         1
$
*SET_NODE_LIST
$  sid      da1      da2      da3      da4
     1
$  nid1     nid2     nid3     nid4     nid5     nid6     nid7     nid8
     1         2
$

```

---

# \*CONTROL\_DAMPING

## Cantilever Beam

---

```
*SET_SHELL_LIST
$   sid      da1      da2      da3      da4
$     1
$   eid1
$     1
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Loading
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Load nodes 21 and 22 with a constant 50 N in the z-direction.
$
*LOAD_NODE_SET
$   nsid      dof      lcid      sf      cid      m1      m2      m3
$     2        3        1        0.5
$
*SET_NODE_LIST
$   sid      da1      da2      da3      da4
$     2
$   nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
$    21        22
$
*DEFINE_CURVE
$   lcid      sidr      scla      sclo      offa      offo
$     1
$           a           o
$         0.0         100.0
$        10.0         100.0
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*PART
$   pid      sid      mid      eosid      hgid      adpopt
Beam - Elastic Material
$     1        1        1
$
$
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
$     1  1.00e-08  210000.0  0.300
$
$
*SECTION_SHELL
$   sid      elform      shrf      nip      propt      qr/irid      icomp
$     1        2        1.0        2        1.0
$   t1      t2      t3      t4      nloc
$   10.0    10.0    10.0    10.0    0.0
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
```

**\*CONTROL\_DAMPING**  
**Cantilever Beam**

---

```
$
$$$$ Nodes 1 and 2 have fixed boundary conditions (translation and rotation).
$
*NODE
$  node          x          y          z          tc          rc
   1  0.000000E+00  0.000000E+00  0.000000E+00    7          7
   2  0.000000E+00  1.000000E+02  0.000000E+00    7          7
   3  1.000000E+02  0.000000E+00  0.000000E+00    0          0
   .
   ... in total, 22 nodes defined
   .
  20  9.000000E+02  1.000000E+02  0.000000E+00    0          0
  21  1.000000E+03  0.000000E+00  0.000000E+00    0          0
  22  1.000000E+03  1.000000E+02  0.000000E+00    0          0
$
$$$$$ Shell Elements
$
*ELEMENT_SHELL
$  eid          pid          n1          n2          n3          n4
   1           1           1           3           4           2
   2           1           3           5           6           4
   3           1           5           7           8           6
   4           1           7           9          10           8
   5           1           9          11          12          10
   6           1          11          13          14          12
   7           1          13          15          16          14
   8           1          15          17          18          16
   9           1          17          19          20          18
  10           1          19          21          22          20
$
*END
```

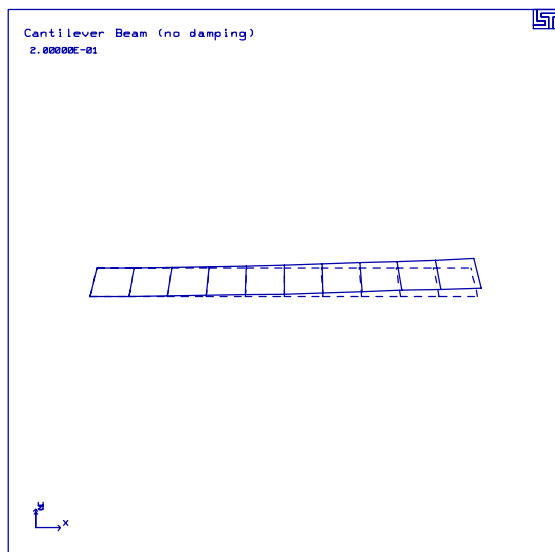
# \*CONTROL\_DAMPING

## Cantilever Beam

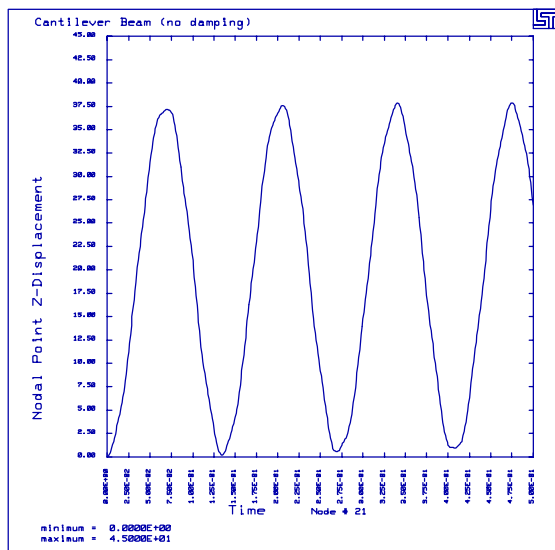
---

### Results:

taurus g=d3plot  
rx -40 head Cantilever Beam (no damping)  
time 0.2 udg 1 view

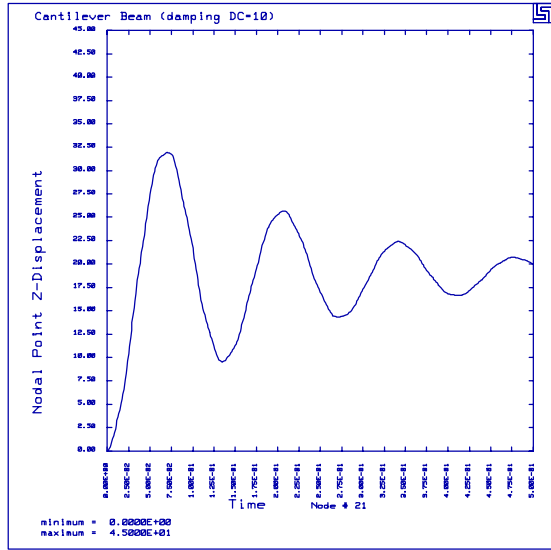


phs3 nodout  
head Cantilever Beam (no damping)  
oset 0 45 z-disp

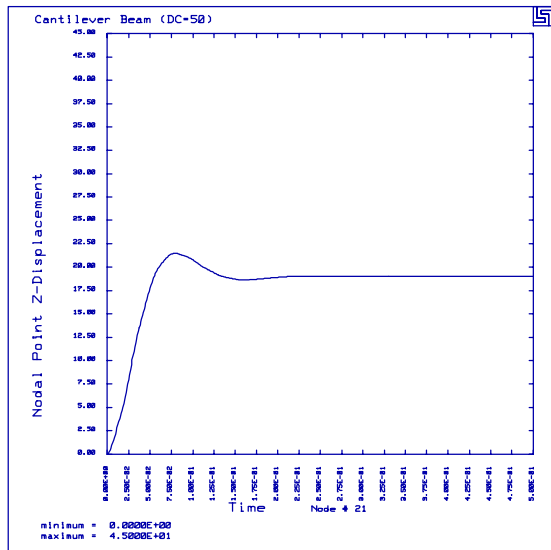


**Results:**

from phase 3, nodout - damping of DC = 10



from phase 3, nodout - damping of DC = 50



**\*CONTROL\_DAMPING**  
Cantilever Beam

---



**LS-DYNA Manual Section:** \*CONTROL\_ENERGY

**Example:** Bar Impact

**Filename:** control\_energy.bar-impact.k

**Description:**

A copper bar strikes a wall.

**Model:**

A 1/4 symmetry bar measures 0.32 cm in radius and 3.24 cm in length and contains 972 hexahedron element. The bar starts at 0.0227 cm/ $\mu$ sec and stops at 0 cm/ $\mu$ sec. The calculation illustrates the energy balance where  $E = KE + IE + HGE$ .

**Input:**

The hourglass energy is computed at a negligible cost. (\*CONTROL\_ENERGY) The initial velocity for every node is set to -0.0227 except the nodes at  $z = 0$ .

**Results:**

The undeformed and deformed shape of the bar are shown. The total, kinetic, internal and hourglass energies are also shown.

# \*CONTROL\_ENERGY

## Bar Impact

### List of LS-DYNA input deck:

```
*KEYWORD
*TITLE
bar impact
$
$ LSTC Example
$
$ Last Modified: September 12, 1997
$
$ Units: gm, cm, microsec, 1e+07 N, Mbar, 1e+07 N-cm
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1.>....2.>....3.>....4.>....5.>....6.>....7.>....8
$
*CONTROL_TERMINATION
$   endtim   endcyc   dtmin   endneg   endmas
     82.10
$
*CONTROL_ENERGY
$   hgen     rwen     slnten     rrlen
     2
$
*CONTROL_HOURLASS
$   ihq       qh
     4
$
*CONTROL_OUTPUT
$   npopt    neecho    nrefup    iaccop    opifs     ipnint    ikedit
     0        0         0         0         0         2         1000
$
$
*DATABASE_BINARY_D3PLOT
$   dt       lcdt
     5.0
$
*DATABASE_BINARY_D3THDT
$   dt       lcdt
     1.0
$
*DATABASE_GLSTAT
$   dt
     0.5
$
*DATABASE_NODOUT
$ dt/cycl   lcdt
     0.5
$
*DATABASE_HISTORY_NODE
$   id1      id2      id3      id4      id5      id6      id7      id8
     1333
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Initial Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
```



# \*CONTROL\_ENERGY

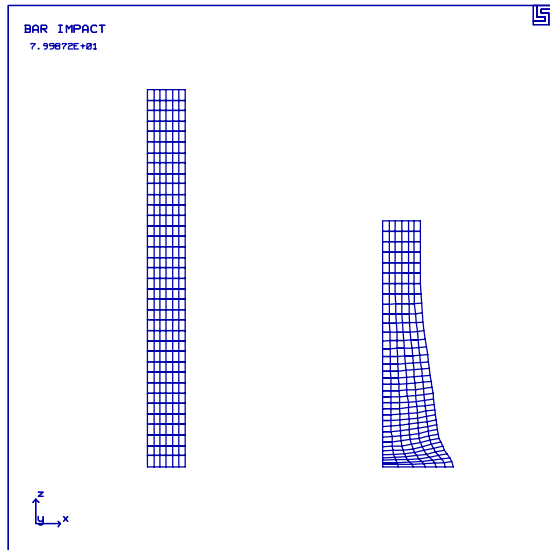
## Bar Impact

---

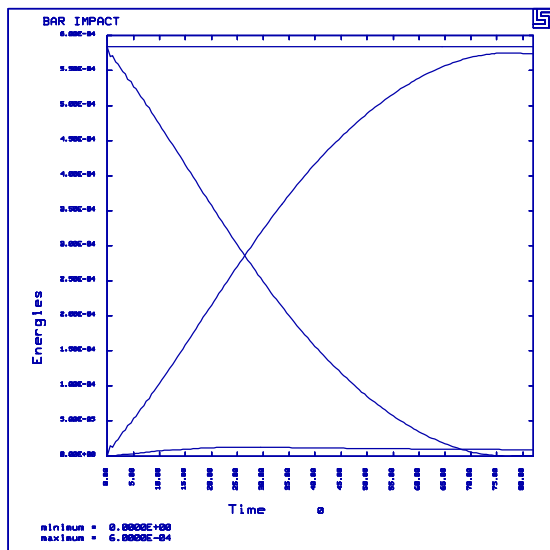
```
$
*ELEMENT_SOLID
$   eid      pid      n1      n2      n3      n4      n5      n6      n7      n8
    1         1         8         1         2         9         45        38        39        46
    2         1         9         2         3        10        46        39        40        47
    3         1        10         3         4        11        47        40        41        48
    .
    ... in total, 972 solids defined
    .
    970        1    1317    1318    1327    1330    1354    1355    1364    1367
    971        1    1330    1327    1328    1331    1367    1364    1365    1368
    972        1    1331    1328    1329    1332    1368    1365    1366    1369
$
*END
```

**Results:**

taurus g=d3plot  
19  
rx -90 angle 1 xtrans -1 view xtrans 2 state 17 over view



phs3 glstat  
oset 0 6e-4 otxt Energies  
total over kine over inter over hour



**\*CONTROL\_ENERGY**

Bar Impact

---

**LS-DYNA Manual Section:** \*CONTROL\_SHELL

**Example:** Hemispherical Load

**Filename:** control\_shell.hemi-load.k

**Description:**

A spherical shell is subjected to outward point loads on the x-axis and inward point loads on the z-axis.

**Model:**

The 1/8 symmetry model of a sphere measures 10 inches in radius with a thickness of 0.04 inches. The model contains 48 shell elements. A force of one pound is applied in the positive x-direction to the node on the x-axis. A force of one pound is applied in the negative z-direction to the node on the y-axis.

**Input:**

The element formulation is the Hughes-Liu shell with four integration points through the thickness. Note: If B-T element formulation is used the solution would be incorrect. To fix it, the Belytschko Tsay shell requires the Belytschko-Wang-Chiang warpage stiffness modification (\*CONTROL\_SHELL). The concentrated loads are applied to two nodes (\*DEFINE\_CURVE, \*LOAD\_NODE\_POINT).

**Results:**

The oscillation of the node on the z-axis shows a regular oscillatory behavior. Since there is no specified damping, oscillations would be expected.

**Reference:**

Belytschko, T., Wang and Chiang.

## \*CONTROL\_SHELL

### Hemispherical Load

---

#### List of LS-DYNA input deck:

```

*KEYWORD
*TITLE
Twisted Beam
$
$   LSTC Example
$
$   Last Modified: September 15, 1997
$
$   Units: lbf-s2/in, in, s, lbf, psi, lbf-in
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$   Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$. . . > . . . 1 . . . > . . . 2 . . . > . . . 3 . . . > . . . 4 . . . > . . . 5 . . . > . . . 6 . . . > . . . 7 . . . > . . . 8
$
*CONTROL_TERMINATION
$   endtim   endcyc       dtmin   endneg   endmas
      0.018
$
*CONTROL_OUTPUT
$   npopt    neecho      nrefup   iaccop    opifs     iprint    ikedit
           0          0          0          0          2         1000
$
*CONTROL_SHELL
$   wrpang   itrism      irnxx    istupd    theory    bwc       miter
           -2                 1
$
$
*DATABASE_EXTENT_BINARY
$   neiph     neips    maxint    strflg    sigflg    epsflg    rltflg    engflg
                   4
$   cmpflg   ieverp    beamip
$
$
*DATABASE_BINARY_D3PLOT
$   dt      lcdt
      0.001
$
*DATABASE_BINARY_D3THDT
$   dt      lcdt
      0.0001
$
*DATABASE_BNDOUT
$   dt
      0.0001
$
*DATABASE_GLSTAT
$   dt
      0.0001
$
*DATABASE_NODOUT
$   dt
      0.0001
$
*DATABASE_HISTORY_NODE
$   id1      id2      id3      id4      id5      id6      id7      id8
           37

```





# \*CONTROL\_SHELL

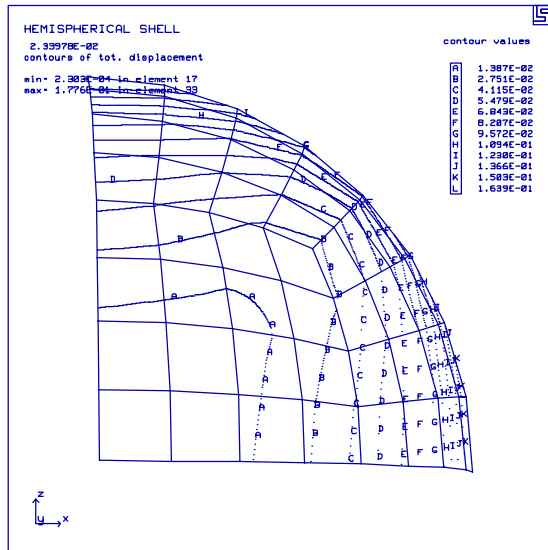
## Hemispherical Load

---

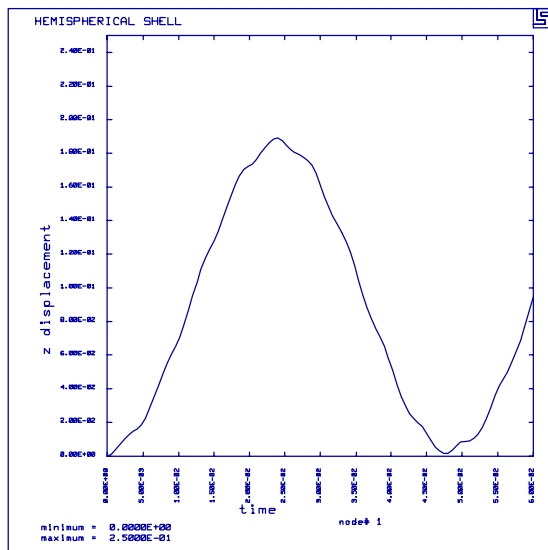
```
.
... in total, 39 nodes defined
.
37  0.000000E+00  -5.500000E-01  1.200000E+01  0  0
38  0.000000E+00   0.000000E+00  1.200000E+01  0  0
39  0.000000E+00   5.500000E-01  1.200000E+01  0  0
$
$$$$ Shell Elements
$
*ELEMENT_SHELL
$  eid      pid      n1      n2      n3      n4
   1         1         1         4         5         2
   2         1         2         5         6         3
.
... in total, 24 shells defined
.
23         1        34        37        38        35
24         1        35        38        39        36
$
*END
```

**Results:**

taurus g=d3plot  
19  
rx -90 angle 5 mono numc s 40 contour 20



phs2  
nodes 2 1 10 gather  
oset 0 0.25 black ntime 3 1 1



**\*CONTROL\_SHELL**  
Hemispherical Load

---

**LS-DYNA Manual Section:** \*CONTROL\_SHELL

**Example:** Twisted Cantilever Beam

**Filename:** control\_shell.beam-twist.k

**Description:**

A beam twisted 90 degrees about its length is constrained on one edge and has a point load prescribed normal to the opposite end of the beam.

**Model:**

The beam measures  $12.00 \times 1.10 \times 0.32$  cubic inches. A concentrated load is applied to one node on the end in the x-direction and the other node on the end in the z-direction.

**Input:**

This model uses the Hughes-Liu five through the thickness integration points (\*CONTROL\_SHELL, \*SECTION\_SHELL). The element has the shell normal update calculation performed at each nodal fiber every cycle (\*CONTROL\_SHELL). Note: This is another example that will not work correctly with the B-T shell formulation (unless warping stiffness is added).

**Results:**

The beam oscillates about a neutral amplitude.

**Reference:**

Belytschko, Wang and Chiang.



**\*CONTROL\_SHELL**  
**Twisted Cantilever Beam**

---

```

1
$      abscissa      ordinate
      0.000E+00      1.000E+00
      1.000E+00      1.000E+00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$      pid      sid      mid      eosid      hgid      adpopt
Hemisphere
      1      1      1
$
$
$
*MAT_PLASTIC_KINEMATIC
$      mid      ro      e      pr      sigy      etan      beta
      1 1.000E-03 6.825E+07      0.3 600000.00 0.000E+00 0.000E+00
$      src      srp      fs
      0.000E+00 0.000E+00 0.000E+00
$
$
$
*SECTION_SHELL
$      sid      elform      shrff      nip      propt      qr/irid      icomp
      1      t1      t2      t3      t4      nloc
      4.000E-02 4.000E-02 4.000E-02 4.000E-02
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Multiple nodes have boundary conditions to simulate symmetry.
$
*NODE
$      node      x      y      z      tc      rc
      1      0.000000E+00      0.000000E+00      1.000000E+01      1      5
      2      1.950897E+00      0.000000E+00      9.807854E+00      0      0
      3      3.826834E+00      0.000000E+00      9.238795E+00      0      0
      .
      ... in total, 61 nodes defined
      .
      59      8.180990E+00      1.705178E+00      5.492155E+00      0      0
      60      7.794079E+00      3.370117E+00      5.281538E+00      0      0
      61      7.167934E+00      4.930554E+00      4.930554E+00      0      0
$
$$$$$ Shell Elements
$
*ELEMENT_SHELL
$      eid      pid      n1      n2      n3      n4
      1      1      1      6      7      2
      2      1      2      7      8      3
      3      1      3      8      9      4
      .
      ... in total, 48 shells defined

```

**\*CONTROL\_SHELL**  
**Twisted Cantilever Beam**

---

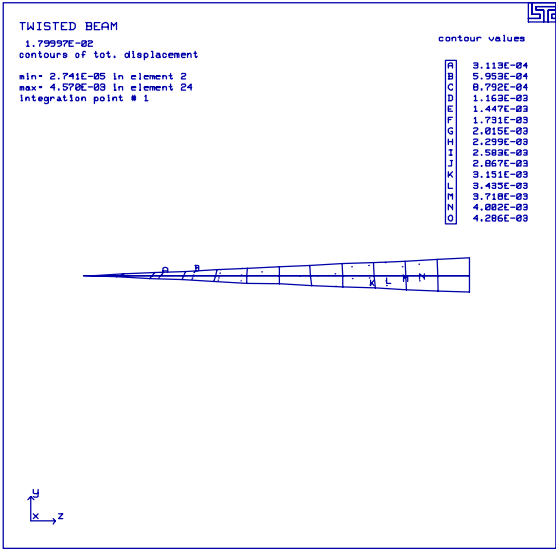
.					
46	1	59	10	15	60
47	1	60	15	20	61
48	1	61	20	25	45

\$  
\*END

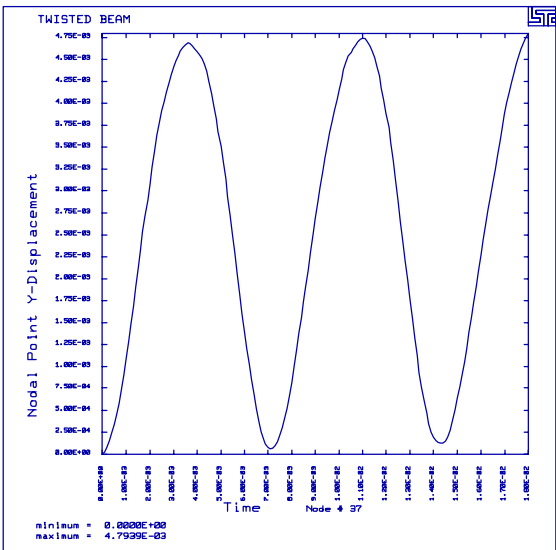


**Results:**

taurus g=d3plot  
19  
ry 90 state 19 mono numc 15 contour 20



phs3  
nodout  
black y-disp



**\*CONTROL\_SHELL**  
Twisted Cantilever Beam

---

**LS-DYNA Manual Section:** \*CONTROL\_TIMESTEP

**Example:** Billet Upset

**Filename:** control\_timestep.billet-forge.k

**Description:**

A rod of steel is forged between two dies. The billet upset problem is a measure of friction under forming conditions.

**Model:**

The billet material is isotropic elastic-plastic, and the model has  $1 \bullet 8$  symmetry. The billet measures 2.25 inches in height and 1.26 inches in radius. The die compresses the billet 1.60 inches. The relationship between the shear friction and the normal pressure is bilinear.

**Input:**

The mass scaling time step size is set to 12 microseconds (\*CONTROL\_TIMESTEP). The billet nodes contact the die surfaces (\*CONTACT\_NODES\_TO\_SURFACE). The Coulomb frictional constant is 0.10 and the constant shear is 2,055 psi . A half sine wave defines the velocity of the die (\*BOUNDARY\_PRESCRIBED\_MOTION).

**Results:**

The results show that effective plastic strains with and without timestep control are the same. CPU savings is approximately 33% on the cray J90 using 1 cpu..

**Reference:**

Avitzur, B., Lee, C. H. and Altan, T.





## \*CONTROL\_TIMESTEP

### Billet Upset

```

$
$$$$ Define Contacts
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
*CONTACT_NODES_TO_SURFACE
$      ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
$       1         2         3         3
$      fs        fd         dc         vc         vdc        penchk      bt        dt
$     0.1        0.1         2.055E+03
$      sfs        sfm         sst         mst         sfst        sfmt        fsf        vsf

$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$ Part    1    solid: Billet - Aluminum
$
$$$ Part    2    shell: Press - Aluminum - rigid
$
*PART
$      pid      sid      mid      eosid      hgid      adpopt
Billet - Aluminum
      1         1         1
Press - Aluminum
      2         2         2

$
$$$$ materials
$
*MAT_PIECEWISE_LINEAR_PLASTICITY
$      mid      ro      e      pr      sigy      etan      eppf      tdel
$       1    2.50e-4  10.00e+6  0.33
$       c      p      lcss     lcsr

$
$      eps1     eps2     eps3     eps4     eps5     eps6     eps7     eps8
$   0.000E+00  5.000E-03  1.000E-02  5.000E-02  1.000E-01  2.000E-01  7.000E-01  4.000E+00
$
$      es1     es2     es3     es4     es5     es6     es7     es8
$   4.785E+03  6.505E+03  7.423E+03  1.063E+04  1.254E+04  1.482E+04  2.010E+04  3.081E+04
$
$
$
*MAT_RIGID
$      mid      ro      e      pr      n      couple      m      alias
$       2    2.50e-4  10.00e+6  0.33
$      cmo      con1      con2
$    -1.0      0.0      110111
$   lco/a1     a2      a3      v1      v2      v3
$   0.0

$
$$$$ sections
$
*SECTION_SOLID
$      sid      elform
$       1         0
$

```

**\*CONTROL\_TIMESTEP**  
**Billet Upset**

```

*SECTION_SHELL
$   sid   elform   shrf   nip   propt   qr/irid   icomp
    2
$   t1     t2     t3     t4     nloc
 1.000E-02 1.000E-02 1.000E-02 1.000E-02
$
$
$$$$$ Define Nodes and Elements
$
$$$$$ Many nodes have boundary conditions in order to simulate symmetry.
$
*NODE
$   node          x          y          z          tc          rc
    1   0.000000E+00  0.000000E+00  0.000000E+00    7          7
    2   4.687500E-02  0.000000E+00  0.000000E+00    5          7
    3   9.375000E-02  0.000000E+00  0.000000E+00    5          7
    .
    ... in total, 5755 nodes defined
    .
 5753   9.731613E-01  8.317921E-01  1.126000E+00    0          0
    .
 5754   1.018930E+00  8.704337E-01  1.126000E+00    0          0
 5755   1.064698E+00  9.090752E-01  1.126000E+00    0          0
$
$$$$$ Solid Elements
$
*ELEMENT_SOLID
$   eid   pid   n1   n2   n3   n4   n5   n6   n7   n8
    1     1     1    2   11   10   82   83   92   91
    2     1     2    3   12   11   83   84   93   92
    3     1     3    4   13   12   84   85   94   93
    .
    ... in total, 4576 solids defined
    .
 4574     1   5307  5308  3627  3618  5379  5380  3708  3699
 4575     1   5308  5309  3636  3627  5380  5381  3717  3708
 4576     1   5309  5310  3645  3636  5381  5382  3726  3717
$
$$$$$ Shell Elements
$
*ELEMENT_SHELL
$   eid   pid   n1   n2   n3   n4
    1     2   5383  5394  5395  5384
    2     2   5384  5395  5396  5385
    3     2   5385  5396  5397  5386
    .
    ... in total, 340 shells defined
    .
 338     2   5752  5602  5613  5753
 339     2   5753  5613  5624  5754
 340     2   5754  5624  5635  5755
$
*END

```

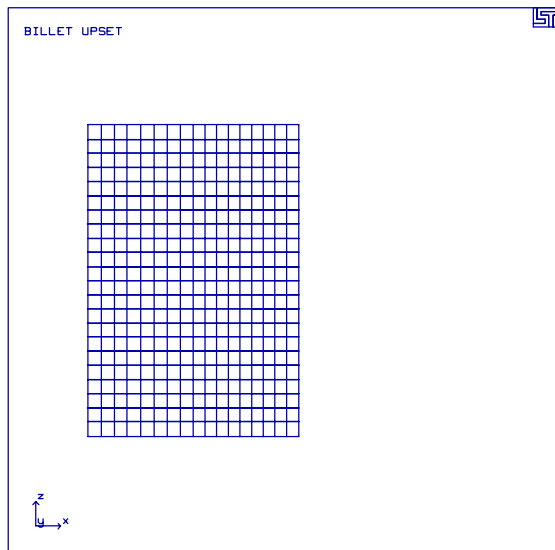
# \*CONTROL\_TIMESTEP

## Billet Upset

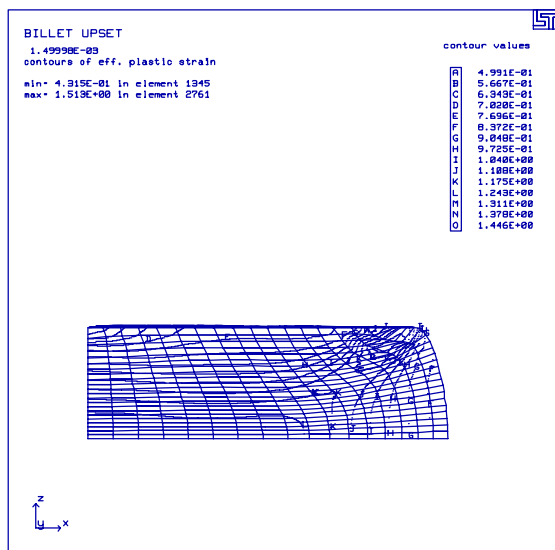
---

### Results:

taurus g=d3plot  
19  
rx -90 angle 5 m 1 view



state 16  
numc 15 mono  
contour 7





**LS-DYNA Manual Section:** \*CONTROL\_ADAPTIVE

**Additional Sections:**

\*DAMPING\_GLOBAL  
\*LOAD\_RIGID\_BODY

**Example:** Deep Drawing with Adaptivity

**Filename:** control\_adaptive.cup-draw.k

**Description:**

This problem includes three tools a punch, a binder and a die and also includes a blank to be formed. The blank is deep drawn by the punch while the binder and die hold the blank edges and help prevent wrinkling. During the process, adaptivity is employed to refine the mesh of the blank to improve accuracy.

**Model:**

Only 1/4 of the system is modeled because of symmetry. The binder pushes down on the blank against the die using a \*LOAD\_RIGID command to model the boundary edge condition. The punch is moved down onto the blank with a \*BOUNDARY\_PRESCRIBED\_MOTION\_RIGID command. Global damping and contact damping are defined to prevent local nodal vibrations. The time step size is controlled with mass scaling because inertial effects are insignificant in this problem. One way surface to surface contact is defined between the major parts. This allows the drawing (i.e., contact) forces to be monitored using the rforc ascii output file.

**Results:**

During the drawing operation, the mesh is refined considerably.





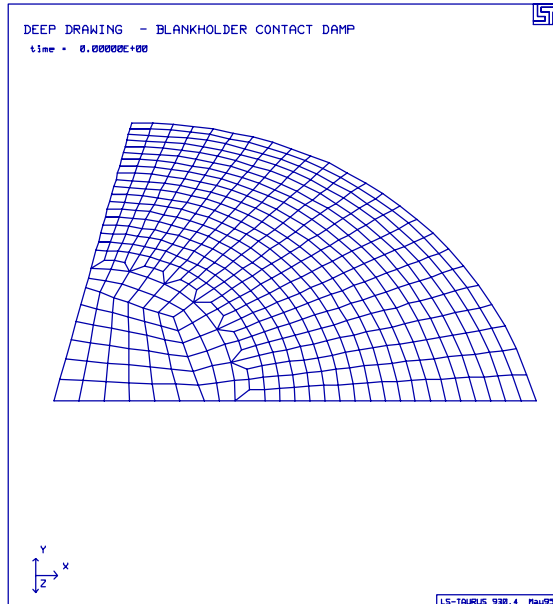




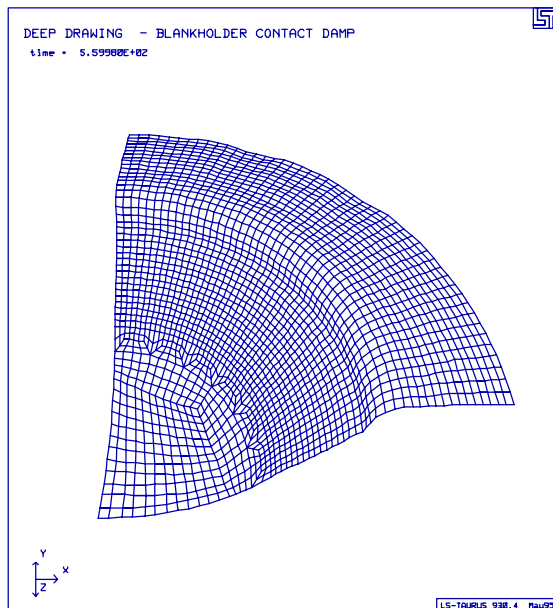


**Results:**

taurus g=d3plot  
rx 45 m 3 s 15 center  
state 1 view



state 15  
view







**LS-DYNA Manual Section:** \*CONTROL\_ADAPTIVE

**Additional Sections:**

\*CONTROL\_SUBCYCLE

**Example:** Square Crush Tube with Adaptivity

**Filename:** control\_adaptive.square-beam.k

**Description:**

A square cross section of a crush tube uses adaptivity to re-fine the mesh as needed to improve accuracy..

**Model:**

Only 1/4 of the tube is modeled because of symmetry. The nodes on top of the crush tube are assigned extra mass with \*ELEMENT\_MASS and given an initial velocity in the y-direction of -5,646 mm/s. The nodes on the bottom of the tube are fixed in y-translation. Automatic single surface contact is defined to prevent penetration when the folds of the crush tube start to form. The model has subcycling defined.

**Results:**

The mesh at the fold location in the crush tube is automatically re-fined as the crush progresses.

# \*CONTROL\_ADAPTIVE

## Square Crush Tube with Adaptivity

---

### List of LS-DYNA input deck:

```
*KEYWORD
*TITLE
square cross section for single surface contact and adaptivity test
$
$  LSTC Example
$
$  Last Modified: October 15, 1997
$
$  Units: ton, mm, s, N, MPa, N-mm
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$  Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTROL_TERMINATION
$  endtim  endcyc  dtmin  endneg  endmas
  3.000E-03
$
*CONTROL_ENERGY
$  hgen  rwen  slnten  rylen
   2      2        2
$
*CONTROL_OUTPUT
$  npopt  neecho  nrefup  iaccop  opifs  ipnint  ikedit
   1        3
$
$
*DATABASE_BINARY_D3PLOT
$  dt  lcdt
  0.999e-4
$
*DATABASE_GLSTAT
$  dt
  0.00002
$
*DATABASE_MATSUM
$  dt
  0.00002
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$  Adaptivity
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTROL_ADAPTIVE
$  adpfreq  adptol  adpopt  maxlvl  tbirth  tdeath  lcadp  ioflag
  1.0e-4    5.0      2        2        0.0      0.0      0
$
$
*CONTROL_SUBCYCLE
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
```



# \*CONTROL\_ADAPTIVE

## Square Crush Tube with Adaptivity

---

```

$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*PART
$  pid        sid        mid        eosid        hgid        grav        adpopt
square-tube
$        1            1            1            0            0            0            1
$
$
*MAT_PLASTIC_KINEMATIC
$  mid        ro            e            pr            sigy        etan        beta
$        1 7.850E-09 1.994E+05 3.000E-01 3.366E+02 1.000E+00 1.000E+00 0.000E+00
$  src        srp            fs
$
$
$
*SECTION_SHELL
$  sid        elform        shrf        nip        propt        qr/irid        icomp
$        1            2            1.            3.            0.            0.            0
$  t1            t2            t3            t4            nloc
$        1.2        1.2            1.2            1.2
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*NODE
$  nid        x            y            z            tc            rc
$        1-3.501449966E+01 0.000000000E+00 -3.501800156E+01 0 0
$        2-3.003639984E+01 0.000000000E+00 -3.496210098E+01 0 0
$        .
$        ... in total, 715 nodes defined
$        .
$        714-3.504100037E+01 -1.550000000E+02 -4.540000111E-02 3 4
$        715-3.497240067E+01 -1.600000000E+02 1.499999966E-02 7 7
$
$$$$ Elements - Shells
$
*ELEMENT_SHELL
$  eid        pid        n1        n2        n3        n4
$        1            1            1            2            4            3
$        2            1            3            4            6            5
$        .
$        ... in total, 640 shells defined
$        .
$        639            1            681            682            714            713
$        640            1            682            683            715            714
$
$.>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$ Elements - Discrete Masses

```

**\*CONTROL\_ADAPTIVE**  
**Square Crush Tube with Adaptivity**

---

```
$
*ELEMENT_MASS
$   eid      nid      mass
    65       65      1.000E-02
    66       66      1.000E-02
    99       99      1.000E-02
   132      132      1.000E-02
   165      165      1.000E-02
   198      198      5.000E-03
   423      423      1.000E-02
   456      456      1.000E-02
   489      489      1.000E-02
   522      522      1.000E-02
   555      555      5.000E-03
$
*END
```

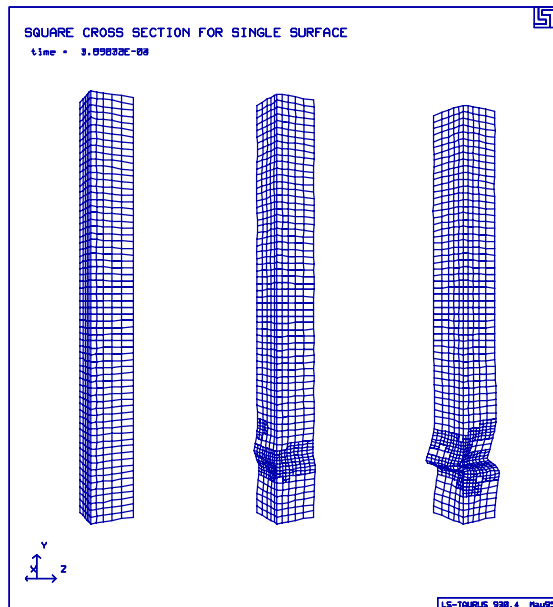
# \*CONTROL\_ADAPTIVE

## Square Crush Tube with Adaptivity

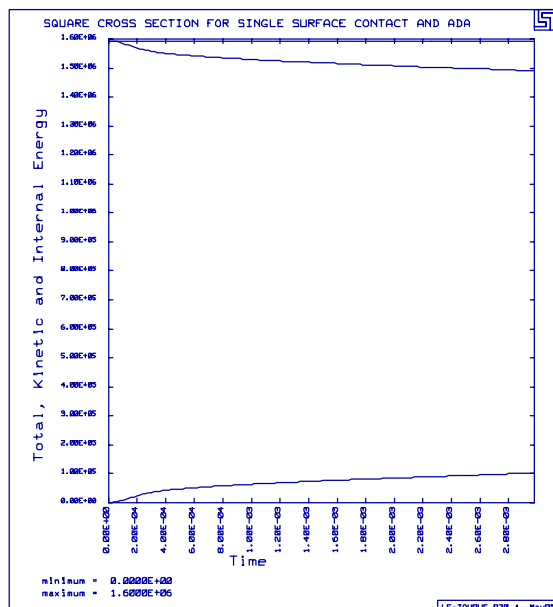
---

### Results:

taurus g=d3plot  
ry 120 xtran -150 v xtran 150 s 5 over v  
xtran 150 s 20 over v



phs3 glstat  
otxt Total, Kinetic and Internal Energy  
oset 0 1.6e6 total over kine over inte



**LS-DYNA Manual Section:** \*CONTROL\_ADAPTIVE

**Additional Sections:**

\*DEFINE\_COORDINATE\_VECTOR

**Example:** Cylinder Undergoing Deformation with Adaptivity

**Filename:** control\_adaptive.cylinder.k

**Description:**

Several nodes on a cylinder are given initial velocities towards the center of the cylinder causing the cylinder to indent. To improve accuracy, adaptivity is defined so that the mesh of the cylinder is re-fined during the deformation.

**Model:**

Only 1/4 of the system is modeled because of symmetry. The boundary conditions on the cylinder are defined with single point constraints (SPC's). Because of the geometry orientation, several of the SPC's require local coordinate system defined using the keyword \*DEFINE\_COORDINATE\_VECTOR.

**Results:**

Before and after mesh refinement are shown in the figures. Additionally, the total, kinetic and internal energy from the glstat ascii file are shown. The entire initial kinetic energy is absorbed by the cylinder due to material deformation (internal energy).







## \*CONTROL\_ADAPTIVE

### Cylinder Undergoing Deformation with Adaptivity

---

```

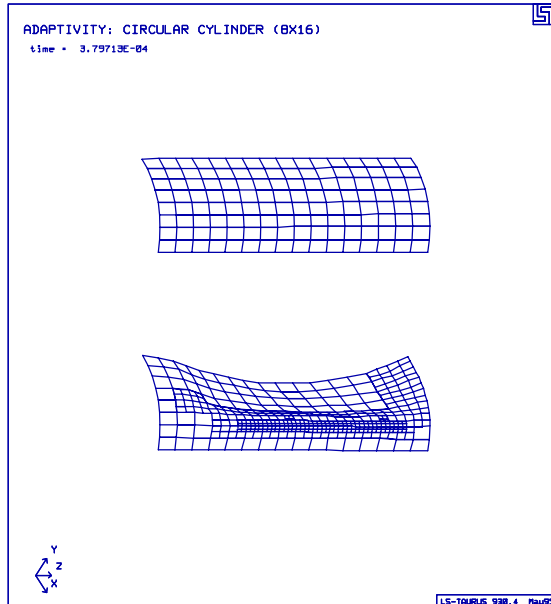
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Initial Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*INITIAL_VELOCITY_NODE
$   nid      vx      vy      vz      vxr      vyr      vzr
    2        0.00 -5650.00   0.00   0.00   0.00   0.00
   19     -737.47 -5601.66   0.00   0.00   0.00   0.00
.
... in total, 65 initial nodal velocities defined
.
   48    -1462.33 -5457.48   0.00   0.00   0.00   0.00
   53    -2162.16 -5219.92   0.00   0.00   0.00   0.00
   82    -2825.00 -4893.04   0.00   0.00   0.00   0.00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*NODE
$   nid      x      y      z      tc      rc
    1 0.000000000E+00 0.294000006E+01 0.000000000E+00   0   0
    2 0.000000000E+00 0.294000006E+01-0.785000026E+00   0   0
.
... in total, 153 nodes defined
.
  152 0.254611492E+01 0.147000003E+01-0.117749996E+02   0   0
  153 0.254611492E+01 0.147000003E+01-0.125600004E+02   0   0
$
$$$$$$$$$$$$ Shell Elements
$
*ELEMENT_SHELL
$   eid      pid      n1      n2      n3      n4
    1        1        1       18       19        2
    2        1        2       19       20        3
.
... in total, 128 shells defined
.
  127        1      134      151      152      135
  128        1      135      152      153      136
*END

```

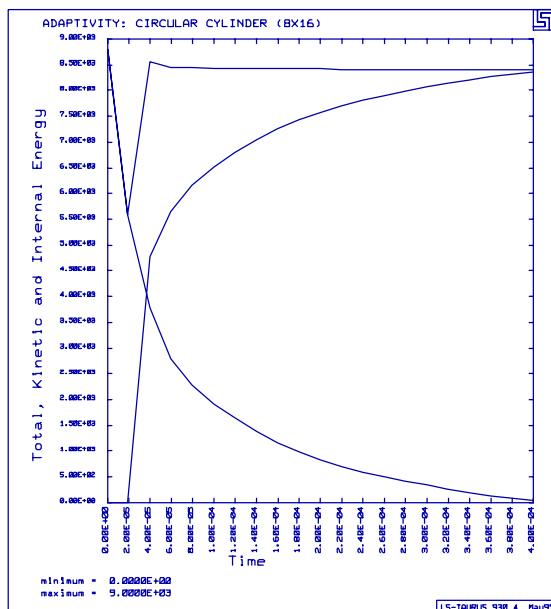
# \*CONTROL\_ADAPTIVE Cylinder Undergoing Deformation with Adaptivity

## Results:

taurus g=d3plot  
angle 1 ry 90 rx -45 ry -45 ytrans 3 view  
ytrans -6 s 20 over view



phs3 glstat  
otxt Total, Kinetic and Internal Energy  
oset 0 9e3 total over kine over inte



**\*CONTROL\_ADAPTIVE**

Cylinder Undergoing Deformation with Adaptivity

---

**LS-DYNA Manual Section:** \*DAMPING\_GLOBAL

**Additional Sections:**

\*CONTROL\_DAMPING  
\*LOAD\_BODY\_Z

**Example:** Tire Bounces on the Ground and Damps Out

**Filename:** damping.tire.k

**Description:**

A simple model of a tire is placed under gravity loading and drops onto rigid solid elements. Fully integrated shell elements are used for the tire to prevent hourglassing from damping out the model. Additionally, rigid solid elements are used for modeling the ground instead of a rigidwall because the rigidwall will also damp the system because of its' perfectly plastic contact definition. Thus, to damp out the bouncing, global damping is applied to the system.

**Model:**

Global damping of 0.5 is applied to the system using the \*DAMPING\_GLOBAL keyword. Contact between the tire and ground is defined using node to surface contact. Gravity is applied with the \*LOAD\_BODY\_Z command.

**Results:**

The total energy of the system comes from the external energy of gravity (potential energy of "mgh"). This energy is absorbed by the damping in the model.

# **\*DAMPING\_GLOBAL**

## Tire Bounces on the Ground and Damps Out

---

### List of LS-DYNA input deck:

```
*KEYWORD
*TITLE
A simple tire bouncing on the ground with damping.
$
$  LSTC Example
$
$  Last Modified: October 13, 1997
$
$  Units: mm, kg, ms, kN, GPa, kN-mm
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$. . . > . . . 1 . . . > . . . 2 . . . > . . . 3 . . . > . . . 4 . . . > . . . 5 . . . > . . . 6 . . . > . . . 7 . . . > . . . 8
$
*CONTROL_TERMINATION
$  endtim  encyc  dtmin  endeng  endmas
    40.01
$
*CONTROL_ENERGY
$  hgen  rwen  slnten  rrlen
    2    2    2        2
$
*CONTROL_OUTPUT
$  npopt  neecho  nrefup  iaccop  opifs  ipnint  ikedit
    1    3
$
*DATABASE_BINARY_D3PLOT
$  dt  lcdt
    10.0
$
*DATABASE_BINARY_D3THDT
$  dt  lcdt
    999999
$
*DATABASE_GLSTAT
$  dt
    0.1
$
*DATABASE_MATSUM
$  dt
    0.1
$
*DATABASE_NODOUT
$  dt
    0.1
$
*DATABASE_HISTORY_NODE
$  id1  id2  id3  id4  id5  id6  id7  id8
    8914  8746  8918
$
*DATABASE_RCFORC
$  dt
    0.1
$
*DATABASE_RWFORC
$  dt
```

# \*DAMPING\_GLOBAL

## Tire Bounces on the Ground and Damps Out

---

```
0.1
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Damping
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*DAMPING_GLOBAL
$    lcid    valdmp
      0       0.5
$
*CONTROL_DAMPING
$    nrcyck    drtol    drfctr    drterm    tssfdr    irelal    edttl    idrflg
      100     1.0e-3    0.995     0.9
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Gravity
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*LOAD_BODY_Z
$    lcid      df     lciddr      xc      yc      zc
      1  9.810E-03
$
$
$
*DEFINE_CURVE
$    lcid      sidr      scla      sclo      offa      offo
      1
$
$          abscissa          ordinate
              0.00              1.000
             1000.00             1.000
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Contacts - sliding interface definitions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$ Prevent the nodes of the tire from penetrating the ground.
$
*CONTACT_NODES_TO_SURFACE
$
$    ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
       36         76         3         3
$
$    fs        fd        dc        vc        vdc        penchk      bt        dt
$
$    sfs       sfm       sst       mst       sfst       sfmt       fsf       vsf
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
```

---

**\*DAMPING\_GLOBAL**

**Tire Bounces on the Ground and Damps Out**

```

$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$. . . > . . . 1 . . . > . . . 2 . . . > . . . 3 . . . > . . . 4 . . . > . . . 5 . . . > . . . 6 . . . > . . . 7 . . . > . . . 8
$

```

```

$PART
$ pid sid mid eosid hgid grav adpopt
wheel
  35 1 1
tire
  36 1 1
ground
  76 76 2
$

```

\$\$\$\$ Materials

```

$
*MAT_PIECEWISE_LINEAR_PLASTICITY
$ mid ro e pr sigy etan eppf tdel
  1 0.783E-05 200.0 0.3 0.207 0.750
$ Cowper/Symonds Strain Rate Parameters
$ C p lcss lcsr
  40 5
$ Plastic stress/strain curves
  0.000 0.080 0.160 0.400 1.000
  0.207 0.250 0.275 0.290 0.300
$

```

```

$
*MAT_RIGID
$ mid ro e pr n couple m alias
  2 0.783E-05 200.0 0.3
$
$ cmo con1 con2
  1.0 7 7
$
$ lco/a1 a2 a3 v1 v2 v3

```

\$\$\$\$ Sections

```

$
*SECTION_SHELL
$ sid elform shrf nip propt qr/irid icompl
  1 6 3.0000
$ t1 t2 t3 t4 nloc
  1.00 1.00 1.00 1.00
$

```

```

$
*SECTION_SOLID
  76 1
$

```

\$\$\$\$ Define Nodes and Elements

```

$
$. . . > . . . 1 . . . > . . . 2 . . . > . . . 3 . . . > . . . 4 . . . > . . . 5 . . . > . . . 6 . . . > . . . 7 . . . > . . . 8
$

```

```

$NODE
$ nid x y z tc rc
  8719 -1.16673000E+02 -6.24000000E+02 -1.16673000E+02
  8720 -1.52440000E+02 -6.24000000E+02 -6.31430000E+01

```



**\*DAMPING\_GLOBAL**  
**Tire Bounces on the Ground and Damps Out**

---

```

      .
      ... in total, 1522 nodes defined
      .
      52040 2.444749625E+02 -7.51864725E+02 -2.79200000E+02
      52049 2.698749875E+02 -7.51864725E+02 -2.79200000E+02
$
$$$$$$$$$$$$ Shell Elements
$
*ELEMENT_SHELL
$   eid      pid      n1      n2      n3      n4
      8710      35      8719      8722      8723      8720
      .
      ... in total, 96 shells defined
      .
      8949      36      8929      8932      8926      8924
$
$$$$$$$$$$$$ Solid Elements
$
*ELEMENT_SOLID
$   eid      pid      n1      n2      n3      n4      n5      n6      n7      n8
      50880      76      50315      52520      52902      52521      52362      52686      52950      52687
      .
      ... in total, 534 solids defined
      .
      51588      76      53833      53962      53834      53423      53424      53835      53425      53689
$
$$$$$$$ Nodal Mass Elements
$
*ELEMENT_MASS
$   eid      nid      mass
      8730      8730      10.0
      8746      8746      10.0
$
*END

```

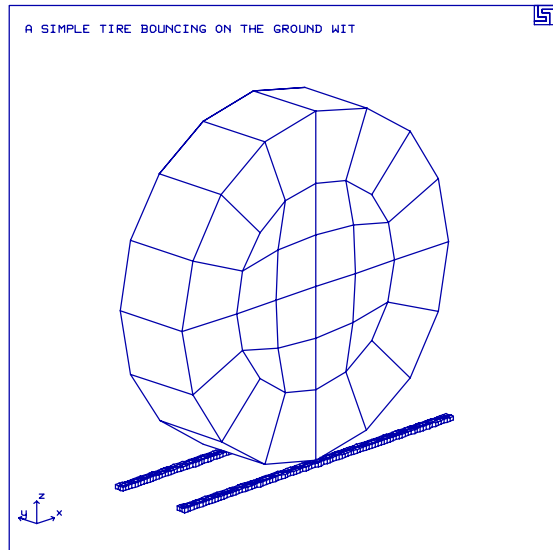
# \*DAMPING\_GLOBAL

## Tire Bounces on the Ground and Damps Out

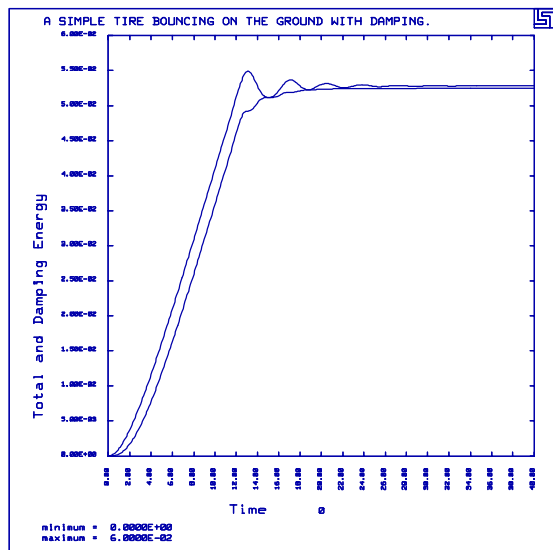
---

### Results:

taurus g=d3plot  
angle 1 rx -90  
ry 45 rx 20 view



phs3 glstat  
otxt Total and Damping Energy  
oset 0 0.06 total over damping



**LS-DYNA Manual Section:** \*DEFORMABLE\_TO\_RIGID

**Additional Sections:**

\*BOUNDARY\_SPC\_NODE  
\*LOAD\_BODY\_Y  
\*RIGID\_DEFORMABLE\_R2D

**Example:** Interaction of Pendulums

**Filenames:** deformable\_to\_rigid.pendulum.k  
deformable\_to\_rigid.pendulum.res

**Execution lines:**

ls940 i= deformable\_to\_rigid.pendulum.k  
ls940 i= deformable\_to\_rigid.pendulum.res r=d3dump01

**Description:**

Two spheres are connected to wires to form two pendulums. One sphere is in a horizontal position with gravitational acceleration, base acceleration and is given an initial velocity in the vertical direction. The other sphere is in the vertical direction. The spheres are treated as rigid bodies while no contact or deformation occurs (i.e., when the horizontal pendulum swings down towards the vertical pendulum). The spheres are switched to deformable through a restart file so that they become flexible during contact.

**Model:**

Both spheres are modeled using shell elements. The pendulum wires are modeled using elastic beams. Automatic single surface contact is used during the impact phase.

**Reference:**

Reid, J.D.

# **\*DEFORMABLE\_TO\_RIGID**

## Interaction of Pendulums

---

### List of LS-DYNA input deck:

```

*KEYWORD
*TITLE
Pendulum with 2 spheres colliding
$
$   LSTC Example
$
$   - uses *DEFORMABLE_TO_RIGID option to decrease execution time before impact
$
$   - one sphere is given an initial velocity (gravity alone just takes
$     too long for the pendulum to swing)
$
$
$   Last Modified: September 16, 1997
$
$   Units: mm, kg, ms, kN, GPa, kN-mm
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*CONTROL_TERMINATION
$   endtim   endcyc   dtmin   endeng   endmas
$         11.0         0         0.0         0.0         0.0
$
*CONTROL_CONTACT
$   slsfac   rwpnal   islchk   shlchk   penopt   thkchg   orien
$                                   2
$   usrstr   usrfrc   nsbcs   interm   xpene
$
$
*CONTROL_ENERGY
$   hgen     rwen     slnten   rylene
$         2         2
$
*CONTROL_OUTPUT
$   npopt    neecho    nrefup   iaccop   opifs    ipnint   ikedit
$         1         3
$
*CONTROL_SHELL
$   wrpang   itrlist   irnxx    istupd   theory    bwc     miter
$                                   1         2
$
$
$
*DATABASE_BINARY_D3PLOT
$   dt       lcdt
$       1.00
$
*DATABASE_EXTENT_BINARY
$   neiph    neips    maxint   strflg   sigflg   epsflg   rltflg   engflg
$
$   cmpflg   ieverp   beamip
$                                   1
$
*DATABASE_BINARY_D3THDT
$   dt       lcdt
$       999999

```

**\*DEFORMABLE\_TO\_RIGID**  
Interaction of Pendulums

---

```

$
$
*DATABASE_GLSTAT
$      dt
       0.10
$
*DATABASE_MATSUM
$      dt
       0.10
$
*DATABASE_NODOUT
$      dt
       0.10
$
*DATABASE_HISTORY_NODE
$      id1      id2      id3
       350      374      678      713
$
*DATABASE_RBDOUT
$      dt
       0.10
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Contacts - Sliding Interfaces
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTACT_AUTOMATIC_SINGLE_SURFACE
$      ssid      msid      sstyp      mstyp
          0
$      Equating ssid to zero means that all segments are included
$
$      fs      fd
          0.08      0.08
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Gravity
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
*LOAD_BODY_Y
$      lcid      sf      lciddr      xc      yc      zc
          1      0.00981
$
*DEFINE_CURVE
$      lcid      sidr      scla      sclo      offa      offo
          1
$          abscissa          ordinate
$
          0.00          1.000
          10000.00          1.000
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$

```

**\*DEFORMABLE\_TO\_RIGID**

**Interaction of Pendulums**

```

$
$$$$ Boundary and Initial Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$ Constrain translation of end points of beams
$
*BOUNDARY_SPC_NODE
$      nid      cid      dofz      dofry      dofzr
$      45004      0        1          1          1          0          0          0
$      45005      0        1          1          1          0          0          0
$      45010      0        1          1          1          0          0          0
$      45011      0        1          1          1          0          0          0
$
$
$$$$ The nodes within box 5 are given an initial velocity.
$
*INITIAL_VELOCITY
$      nsid      nsidex     boxid
$              5
$
$      vx      vy      vz      wx      wy      wz
$      0.0     -12.0     0.0
$
*DEFINE_BOX
$      boxid      xmm      xmx      ymn      ymx      zmn      zmx
$          5     -120.0     -80.0     80.0     120.0     -30.0     30.0
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$ SPHERES
$
*PART
$      pid      sid      mid      eosid      hgid      adpopt
sphere1
$          1          1          1
sphere2
$          2          2          1
$
$
$$$$ Materials
$
$ Aluminum
$
*MAT_PLASTIC_KINEMATIC
$      mid      ro      e      pr      sigy      etan      beta
$          1     2.70e-6     68.9     0.330     0.286     0.00689
$      src      srp      fs
$
$
$$$$ Sections
$
$
$
*SECTION_SHELL

```

**\*DEFORMABLE\_TO\_RIGID**  
Interaction of Pendulums

```

$
$      sid      elform      shrf      nip      propt      qr/irid      icomp
$      1         2         1.0      1.0      1.0      1.0      1.0
$      t1        t2        t3        t4        nloc
$      1.0      1.0      1.0      1.0
$
$ *SECTION_SHELL
$
$      sid      elform      shrf      nip      propt      qr/irid      icomp
$      2         2         1.0      1.0      1.0      1.0      1.0
$      t1        t2        t3        t4        nloc
$      1.0      1.0      1.0      1.0
$
$
$
$
$$$$$  PENDULUM WIRES - ELASTIC BEAMS
$
$ *PART
$      pid      sid      mid      eosid      hgid      adpopt
Pendulum Wires - Elastic Beams
$      45      45      45
$
$
$ *MAT_ELASTIC
$      mid      ro      e      pr      da      db      k
$      45      7.86e-6      210.0      0.30
$
$
$
$ *SECTION_BEAM
$      sid      elform      shrf      qr/irid      cst
$      45      3      1.00000      1.0
$ res:  a      iss      itt      irr      sa
$      10.0
$
$
$$$$$ Deformable Switching
$
$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$ *DEFORMABLE_TO_RIGID
$      pid      mrb
$      1
$
$ *DEFORMABLE_TO_RIGID
$      pid      mrb
$      2
$
$
$$$$$ Define Nodes
$
$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$ *NODE
$      node      x      y      z      tc      rc
$      1      -1.08660250E+02      9.133975000E+01      -3.66025000E+00

```





**\*DEFORMABLE\_TO\_RIGID**  
Interaction of Pendulums

---

```

*KEYWORD
*TITLE
Pendulum with 2 spheres colliding
$
$
$$$$$ Restart
$
$ Last Modified: September 16, 1997
$
$ Units: mm, kg, ms, kN, GPa, kN-mm
$
$$$$$
$
$$$$$ Switch spheres to deformables
$
$$$$$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*RIGID_DEFORMABLE_R2D
$ pid
$ 1
$
*RIGID_DEFORMABLE_R2D
$ pid
$ 2
$
$
$$$$$
$
$$$$$ Control Ouput
$
$$$$$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTROL_TERMINATION
$ ENDTIM ENDCYC DTMIN ENDENG ENDMAS
$ 13.0 0 0.0 0.0 0.0
$
$$$$$ Increase d3plot output frequency to capture deformation of impact better.
$
*DATABASE_BINARY_D3PLOT
$ dt lcdt
$ 0.10
$
*END

```

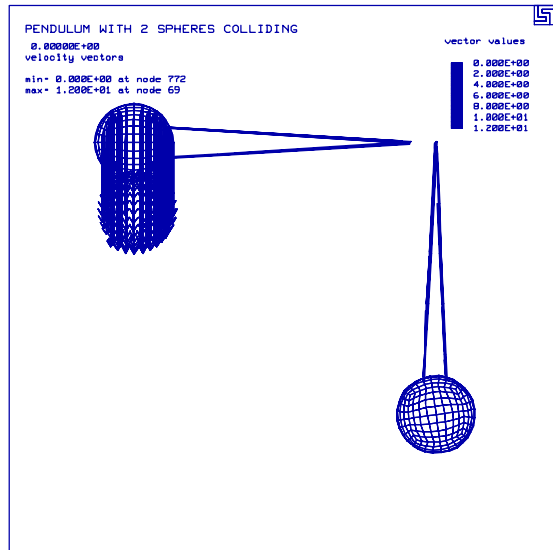
# \*DEFORMABLE\_TO\_RIGID

## Interaction of Pendulums

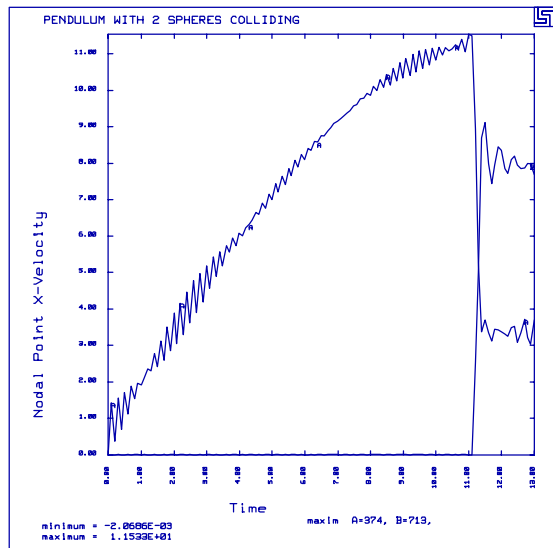
---

### Results:

taurus g=d3plot  
19  
state 1 angle 1 vect v



phs3  
nodout  
x-vel 374 713



**LS-DYNA Manual Section:** \*INTEGRATION\_SHELL

**Additional Sections:**

\*DAMPING\_GLOBAL  
\*LOAD\_NODE\_POINT

**Example:** Cantilever Beam with Lobotto Integration

**Filename:** integration\_shell.lobotto.beam.k

**Description:**

A cantilever beam has a concentrated load, and then the beam vibration critically damps. Lobotto integration rules place the quadrature points on the true surfaces of the shell. [See Hughes].

**Model:**

The plate measures  $1.00 \times 0.10 \times 0.01 \text{ in}^3$  and is modeled with 60 Belytschko-Tsay shell elements. The displacement of the nodes is fixed at one end and a concentrated load is applied to the other end. Symmetry conditions for the plane strain case exist on the beam sides.

**Input:**

The concentrated loads and load curve definition 1 defines the load on the end of the beam (\*LOAD\_NODE\_POINT, \*DEFINE\_CURVE). The beam is critically damped (\*DAMPING\_GLOBAL) The number of integration points is 5 (\*SECTION\_SHELL). The shell integration rule is the Lobotto integration rule (\*SECTION\_SHELL)

**Results:**

The displacement of the beam damps out critically. The x-stress values at the integration points exhibit tension on one side, compression on the opposite side, and balance at the neutral axis.

# **\*INTEGRATION\_SHELL**

## **Cantilever Beam with Lobotto Integration**

---

### **List of LS-DYNA input deck:**

```
*KEYWORD
*TITLE
Lobotto Integration
$
$  LSTC Example
$
$  Last Modified: September 17, 1997
$
$  Units: lbf-s2/in, in, s, lbf, psi, lbf-in
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$  Control Output
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
*CONTROL_TERMINATION
$  endtim  endcyc  dtmin  endneg  endmas
    0.015
$
*CONTROL_ENERGY
$   hgen   rwen   slnten   rylen
    2
$
*CONTROL_OUTPUT
$   npopt   neecho   nrefup   iaccop   opifs   ipnint   ikedit
    0         0         0         0         2         1000
$
$
*DATABASE_BINARY_D3PLOT
$   dt   lcdt
    0.0003
$
*DATABASE_BINARY_D3THDT
$   dt   lcdt
    10.
$
*DATABASE_EXTENT_BINARY
$   neiph   neips   maxint   strflg   sigflg   epsflg   rtflg   engflg
                    5
$   cmpflg   ieverp   beamip
$
$
*DATABASE_GLSTAT
$   dt
    0.0001
$
*DATABASE_ELOUT
$   dt
    0.0001
$
*DATABASE_HISTORY_SHELL
$   id1   id2   id3   id4   id5   id6   id7   id8
    1
$
*DATABASE_NODOUT
$   dt
    0.0001
```

**\*INTEGRATION\_SHELL**  
**Cantilever Beam with Lobotto Integration**

---

```

$
*DATABASE_HISTORY_NODE
$      id1      id2      id3      id4      id5      id6      id7      id8
      31
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Loading
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Load nodes 31, 62, 93 in the negative z-direction.
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*LOAD_NODE_POINT
$      nid      dof      lcid      sf      cid      m1      m2      m3
      31         3        1 -1.00E+00
      62         3        1 -1.00E+00
      93         3        1 -1.00E+00
$
*DEFINE_CURVE
$      lcid      sidr      scla      sclo      offa      offo
      1
$
$          a          o
      0.000E+00      0.000E+00
      8.000E-03      1.667E-03
      1.534E-02      1.667E-03
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Damping
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*DAMPING_GLOBAL
$      lcid      valdmp
      2          0.0
$
*DEFINE_CURVE
$      lcid      sidr      scla      sclo      offa      offo
      2
$
$          a          o
      0.000E+00      0.000E+00
      8.000E-03      0.000E+00
      1.000E-02      2.353E+03
      1.534E-02      2.353E+03
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$      pid      sid      mid      eosid      hgid      adpopt
Cantilever Beam - Aluminum
      1          1          1

```

# \*INTEGRATION\_SHELL

## Cantilever Beam with Lobotto Integration

---

```
$  
$  
*MAT_PLASTIC_KINEMATIC  
$ mid ro e pr sigy etan beta  
1 7.85e-4 10.00e+6 0.300 20000.0 100000 1.0  
$ src srp fs  
0.0 0.0 0.0  
$  
$$$$ irid = -1 ==> integration rule 1 used (see below)  
$  
*SECTION_SHELL  
$ sid elform shrf nip propt qr/irid icip  
1 0 shrf 5 nloc  
$ t1 t2 t3 t4  
0.010 0.010 0.010 0.010  
$  
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$  
$  
$$$$ Integration Rule  
$  
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$  
$  
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8  
$  
*INTEGRATION_SHELL  
$ irid nip esop  
1 5  
$ s wf pid  
-1.000E+00 1.000E-01  
-6.546E-01 5.444E-01  
0.000E+00 7.111E-01  
6.546E-01 5.444E-01  
1.000E+00 1.000E-01  
$  
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$  
$  
$$$$ Define Nodes and Elements  
$  
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$  
$  
*NODE  
$ node x y z tc rc  
1 0.000000E+00 0.000000E+00 0.000000E+00 7 7  
2 3.333334E-02 0.000000E+00 0.000000E+00 2 6  
3 6.666667E-02 0.000000E+00 0.000000E+00 2 6  
. . . .  
... in total, 93 nodes defined  
. . . .  
91 9.333333E-01 1.000000E-01 0.000000E+00 2 6  
92 9.666666E-01 1.000000E-01 0.000000E+00 2 6  
93 1.000000E+00 1.000000E-01 0.000000E+00 2 6  
$  
$$$$$ Shell Elements  
$  
*ELEMENT_SHELL  
$ eid pid n1 n2 n3 n4  
1 1 1 32 33 2  
2 1 2 33 34 3  
3 1 3 34 35 4  
. . . .  
... in total, 60 shells defined  
. . . .  
58 1 59 90 91 60
```

---

**\*INTEGRATION\_SHELL**

**Cantilever Beam with Lobotto Integration**

---

59	1	60	91	92	61
60	1	61	92	93	62

\$  
\*END

# \*INTEGRATION\_SHELL

## Cantilever Beam with Lobotto Integration

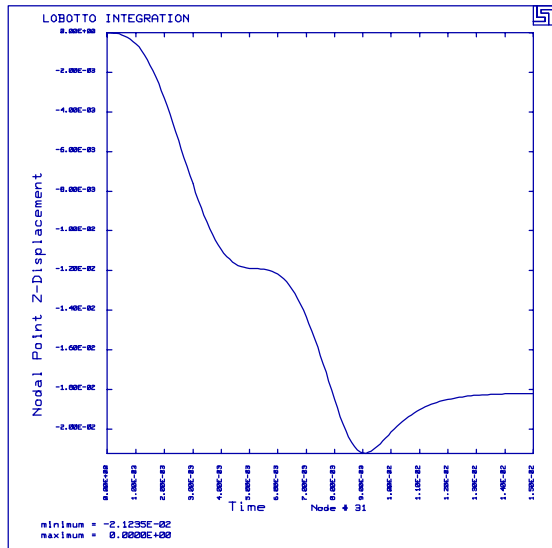
---

**Results:**

taurus g=d3plot  
19  
rx -90 s 50 udg 1 g



phs3  
nodout  
z-disp





## **\*INTERFACE\_COMPONENT**

### An Interface File Controls the Response of a Cube

---

**LS-DYNA Manual Section:** \*INTERFACE\_COMPONENT

**Additional Sections:**

\*INITIAL\_VELOCITY  
\*INTERFACE\_LINKING\_SEGMENT

**Example:** An Interface File Controls the Response of a Cube

**Filenames:** interface\_component.cube.k  
interface\_component.cube.rk

**Execution Line:**

```
LS940 i=interface_component.cube.k z=d3iff
```

After completion, copy d3iff to a separate directory containing interface\_component.cube.rk, then from that directory run:

```
LS940 i=interface_component.cube.rk l=d3iff
```

**Description:**

A cube, one solid element, strikes and rebounds from an elastic plate. In the first run, an interface file (d3iff) is created that contains the position of the bottom segment of the cube. In the second run, the cube mesh refinement increases from 1 element to 8 elements. The interface file is then used to control the position of the bottom of the new cube as if it underwent the same impact as the cube in run one..

**Model:**

The material of the cube and the plate are elastic. The plate, that measures  $40 \times 40 \times 2$  mm<sup>3</sup>, is modeled with 16 Belytschko-Tsay shell elements. The cube has a side length of 10 mm and is initially positioned 10 mm above the plate. The cube is given an initial velocity towards the plate.

**Reference:**

Schweizerhof, K. and Weimer, K.

# \*INTERFACE\_COMPONENT

## An Interface File Controls the Response of a Cube

---

### List of LS-DYNA input deck:

```

*KEYWORD
*TITLE
INTERFACE SEGMENTS (FIRST ANALYSIS)
$
$ LSTC Example
$
$ Last Modified: September 18, 1997
$
$ Units: ton, mm, s, N, MPa, N-mm
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*CONTROL_TERMINATION
$   endtim   endcyc   dtmin   endneg   endmas
$         0.0003
$
*CONTROL_ENERGY
$   hgen     rwen     slnten   rylen
$         2
$
*CONTROL_HOURLASS
$   ihq      qh
$         4
$
$$$$ opifs - output interval for interface file
$
*CONTROL_OUTPUT
$   npopt   neecho   nrefup   iaccop   opifs   ipnint   ikedit
$                                     2.000E-6
$
*CONTROL_TIMESTEP
$   dtinit   scft     isdo     tslimt   dtms     lctm     erode     mslst
$                 0.10
$
$
*DATABASE_BINARY_D3PLOT
$   dt      lcdt
$     0.00002
$
*DATABASE_BINARY_D3THDT
$   dt      lcdt
$     0.00001
$
*DATABASE_EXTENT_BINARY
$   neiph   neips   maxint   strflg   sigflg   epsflg   rtlflg   engflg
$                                     1
$   cmpflg   ieverp   beamip
$
$
*DATABASE_GLSTAT
$   dt
$     0.00001
$
*DATABASE_NODOUT

```

**\*INTERFACE\_COMPONENT**  
An Interface File Controls the Response of a Cube

---

```
$      dt
0.00001
$
*DATABASE_HISTORY_NODE
$      id1      id2      id3      id4      id5      id6      id7      id8
101
$
*DATABASE_RCFORC
$
dt
0.00001
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Interface
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$ Save the behavior on the following segment in the interface file.
$$$$ This file will then be used in the second analysis.
$
*INTERFACE_COMPONENT_SEGMENT
$      sid
3
$
*SET_SEGMENT
$      sid      da1      da2      da3      da4
3
$      n1      n2      n3      n4      a1      a2      a3      a4
101      102      104      103
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Initial Velocity
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ All nodes in box 1 are given an initial velocity (nodes of the cube).
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*INITIAL_VELOCITY
$      nsid      nsidex      boxid
1
$      vx      vy      vz
0.0      0.0 -100000.0
$
*DEFINE_BOX
$      boxid      xmm      xmx      ymn      ymx      zmn      zmx
1      15.0      25.0      15.0      25.0      10.0      20.0
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Contact - Sliding Interfaces
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$ Contact between the bottom of the cube (segment set 1) and the plate.
```

## \*INTERFACE\_COMPONENT

An Interface File Controls the Response of a Cube

---

```
$
*CONTACT_SURFACE_TO_SURFACE
$      ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
      1          2
$      fs        fd          dc          vc          vdc        penchk      bt        dt
$      sfs      sfm        sst        mst        sfst        sfmt        fsf        vsf

$
*SET_SEGMENT
$      sid      da1      da2      da3      da4
      1
$      n1      n2      n3      n4      a1      a2      a3      a4
      101     103     104     102
$
*SET_SEGMENT
$      sid      da1      da2      da3      da4
      2
$      n1      n2      n3      n4      a1      a2      a3      a4
      7       8       13      12
      8       9       14      13
      12      13      18      17
      13      14      19      18

$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$      pid      sid      mid      eosid      hgid      adpopt
Plate
      1          1          1
Cube
      2          2          2

$
$
*MAT_ELASTIC
$      mid      ro      e      pr      da      db
      1      2.00e-8 100000.0 0.300
$
*MAT_ELASTIC
$      mid      ro      e      pr      da      db
      2      1.00e-8 100000.0 0.300

$
$
*SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icomp
      1                0.83333      2.0      3.0
$      t1      t2      t3      t4      nloc
      2.0      2.0      2.0      2.0

$
*SECTION_SOLID
$      sid      elform
      2

$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Define Nodes and Elements
```

---



# \*INTERFACE\_COMPONENT

## An Interface File Controls the Response of a Cube

---

```

$      hgen      rwen      slnten      rylen
$          2
$
$
*CONTROL_HOURLASS
$      ihq      qh
$          4
$
$$$$ opifs - output interval for interface file
$
*CONTROL_OUTPUT
$      npopt      neecho      nrefup      iaccop      opifs      ipnint      ikedit
$                                0.002E-3
$
*CONTROL_TIMESTEP
$      dtinit      scft      isdo      tslimt      dtms      lctm      erode      mslst
$                                0.10
$
*DATABASE_BINARY_D3PLOT
$      dt      lcdt
$      0.00002
$
*DATABASE_BINARY_D3THDT
$      dt      lcdt
$      0.00001
$
*DATABASE_EXTENT_BINARY
$      neiph      neips      maxint      strflg      sigflg      epsflg      rtlflg      engflg
$                                1
$      cmpflg      ieverp      beamip
$
$
*DATABASE_GLSTAT
$
$      dt
$      0.00001
$
*DATABASE_NODOUT
$      dt
$      0.00001
$
*DATABASE_HISTORY_NODE
$      id1      id2      id3      id4      id5      id6      id7      id8
$      101      201      205
$
*DATABASE_RCFORC
$      dt
$      0.00001
$
$$$$
$$$$ Interface
$$$$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$ Link the interface file to the following segments.
$
*INTERFACE_LINKING_SEGMENT
$      ssid      ifid
$          3          1
$
*SET_SEGMENT

```



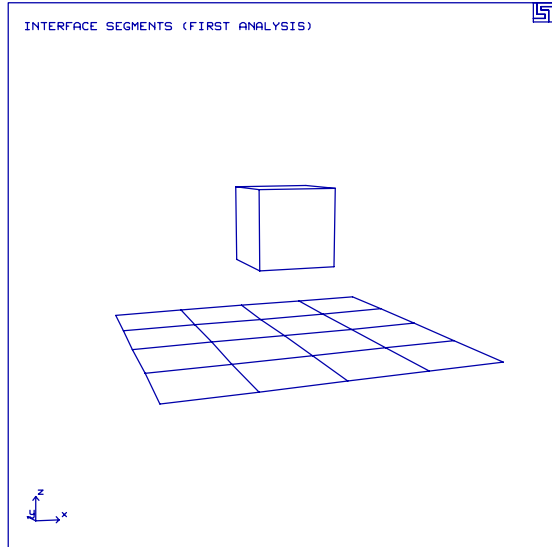
# \*INTERFACE\_COMPONENT

## An Interface File Controls the Response of a Cube

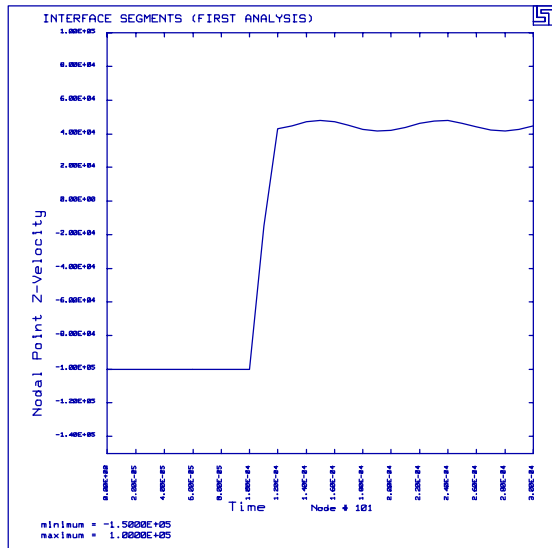
---

**Results:**

taurus g=d3plot  
 19  
 rz 20 rx -80 center v



phs3  
 nodout  
 oset -1.5e5 1.0e5 z-vel 101



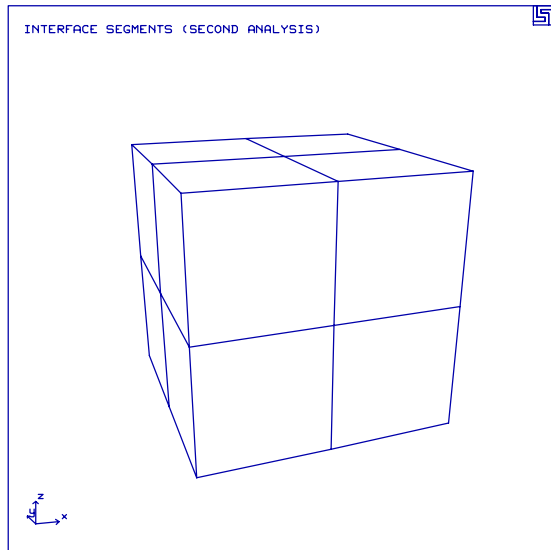


# \*INTERFACE\_COMPONENT

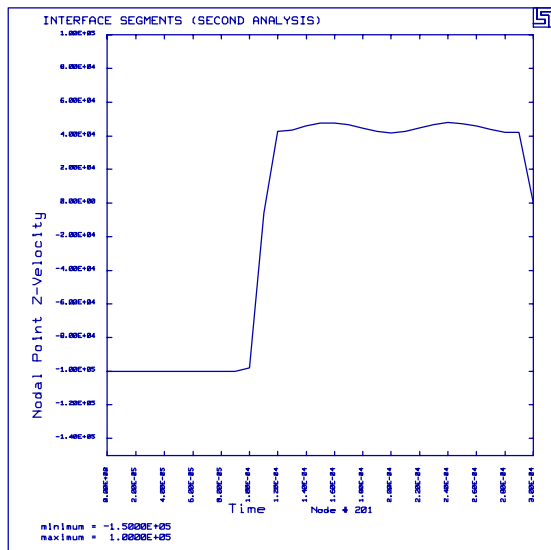
## An Interface File Controls the Response of a Cube

### Results:

taurus g=d3plot  
19  
rz 20 rx -70 center v



phs3  
nodout  
oset -1.5e5 1.0e5 z-vel 201



## **\*INTERFACE\_COMPONENT**

An Interface File Controls the Response of a Cube

---

**LS-DYNA Manual Section:** \*LOAD\_BODY\_GENERALIZED

**Additional Sections:**

\*BOUNDARY\_PRESCRIBED\_MOTION\_NODE  
\*DATABASE\_CROSS\_SECTION\_SET  
\*INITIAL\_VELOCITY\_NODE

**Example:** Rotating Elements

**Filename:** load\_body.shell.k

**Description:**

A body has constant angular velocity. The radial vibration introduced due to the rapid deployment of the rotation is damped out in the initialization phase using dynamic relaxation.

**Model:**

The body measures  $200 \times 100 \times 10 \text{ mm}^3$ . The body consists of 2 Belytschko-Tsay elastic shell elements. The body rotates about the y-axis at 62.83 radians per second. The analysis ends at 0.1 seconds.

**Input:**

All nodes have an initial translational velocity based on the angular velocity  $v = \omega \times r$ . (\*INITIAL\_VELOCITY\_NODE). Dynamic relaxation damps oscillations in the radial direction during the initialization (\*LOAD\_BODY\_GENERALIZED, \*DEFINE\_CURVE). This essentially pre-stresses the structure and the load continues into the analysis portion. Because of the condition of constant angular velocity of the two nodes on the axis of rotation, the motion remains uniform throughout the calculation (\*BOUNDARY\_PRESCRIBED\_MOTION\_NODE). The section forces are available in the ASCII database file secforc (\*DATABASE\_SECFORC).

**Reference:**

Schweizerhof, K. and Weimer, K.

# \*LOAD\_BODY\_GENERALIZED

## Rotating Elements

---

### List of LS-DYNA input deck:

```
*KEYWORD
*TITLE
Mass with Angular Rotation - 2 Shell Elements
$
$ LSTC Example
$
$ Last Modified: September 18, 1997
$
$ Units: ton, mm, s, N, MPa, N-mm
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*CONTROL_TERMINATION
$  endtim  endcyc  dtmin  endneg  endmas
    0.1
$
*CONTROL_HOURLASS
$  ihq  qh
    4
$
$
*DATABASE_BINARY_D3PLOT
$  dt/cycl  lcdt
  10.00E-03
$
*DATABASE_BINARY_D3THDT
$  dt/cycl  lcdt
    0.50E-03
$
*DATABASE_ELOUT
$  dt
    0.001
$
*DATABASE_HISTORY_SHELL
$  id1  id2  id3  id4  id5  id6  id7  id8
    1  2    3    4    5    6    7    8
$
*DATABASE_GLSTAT
$  dt
    0.001
$
*DATABASE_NODOUT
$  dt
    0.001
$
*DATABASE_HISTORY_NODE
$  id1  id2  id3  id4  id5  id6  id7  id8
    1  2    3    4    5    6    7    8
$
*DATABASE_SECFORC
$  dt/cycl  lcdt
    0.001
$
*DATABASE_CROSS_SECTION_SET
```

## \*LOAD\_BODY\_GENERALIZED Rotating Elements

```

$      nsid      hsid      bsid      ssid      tsid      dsid
         1              1
$
*SET_NODE_LIST
$      sid      da1      da2      da3      da4
         1
$      nid1     nid2     nid3     nid4     nid5     nid6     nid7     nid8
         1         2
$
*SET_SHELL_LIST
$      sid      da1      da2      da3      da4
         1
$      eid1     eid2     eid3     eid4     eid5     eid6     eid7     eid8
         1
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Initial Velocity
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*INITIAL_VELOCITY_NODE
$      nid      vx      vy      vz      vx     vye     vze
         1      0.0     0.0     0.0     0.00    62.83    0.00
         2      0.0     0.0     0.0     0.00    62.83    0.00
         3      0.0     0.0    -6283.0    0.00    62.83    0.00
         4      0.0     0.0    -6283.0    0.00    62.83    0.00
         5      0.0     0.0  -12566.0    0.00    62.83    0.00
         6      0.0     0.0  -12566.0    0.00    62.83    0.00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Boundary Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*BOUNDARY_PRESCRIBED_MOTION_NODE
$      nid      dof      vad      lcid      sf      vid
         1         6         0         1         1.0
         2         6         0         1         1.0
$
*DEFINE_CURVE
$      lcid      sidr      scla      sclo      offa      offo
         1
$
           abscissa      ordinate
           0.000           62.83
           1.000           62.83
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Loading
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*LOAD_BODY_GENERALIZED

```

**\*LOAD\_BODY\_GENERALIZED**

**Rotating Elements**

---

```

$   n1      n2      lcid  drlcid     xc       yc       zc
$   1        6        0       2       0.0       0.0       0.0
$   ax      ay      az      omx      omy      omz
$   0.0     0.0     0.0     0.0     1.0     0.0
$
*DEFINE_CURVE
$   lcid      sidr      scla      sclo      offa      offo
$   2         1
$      abscissa      ordinate
$           0.000          62.83
$           1.000          62.83
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
*PART
$   pid      sid      mid      eosid      hgid      adpopt
shells
$   1        1        1
$
$
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
$   1 1.00e-08 210000. 0.300
$
$
*SECTION_SHELL
$   sid      elform      shrf      nip      propt      qr/irid      icomp
$   1                 3
$   t1      t2      t3      t4      nloc
$   10.0    10.0    10.0    10.0
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
*NODE
$   node      x      y      z      tc      rc
$   1 0.000000E+00 0.000000E+00 0.000000E+00 7 0
$   2 0.000000E+00 1.000000E+02 0.000000E+00 6 0
$   3 1.000000E+02 0.000000E+00 0.000000E+00 0 0
$   4 1.000000E+02 1.000000E+02 0.000000E+00 0 0
$   5 2.000000E+02 0.000000E+00 0.000000E+02 0 0
$   6 2.000000E+02 1.000000E+02 0.000000E+00 0 0
$
$
*ELEMENT_SHELL
$   eid      pid      n1      n2      n3      n4
$   1        1        1        3        4        2
$   2        1        3        5        6        4
$
*END

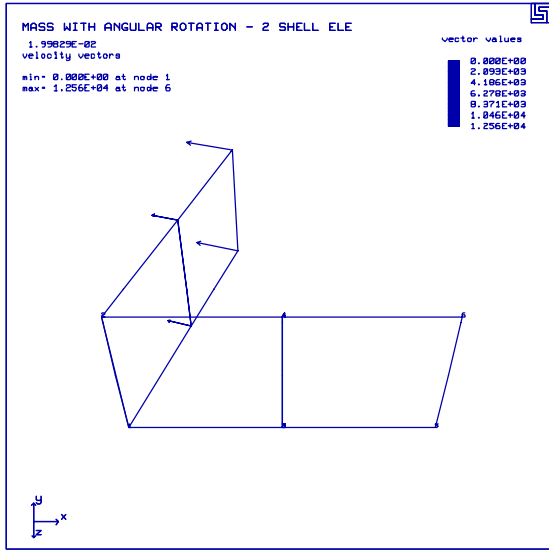
```

---

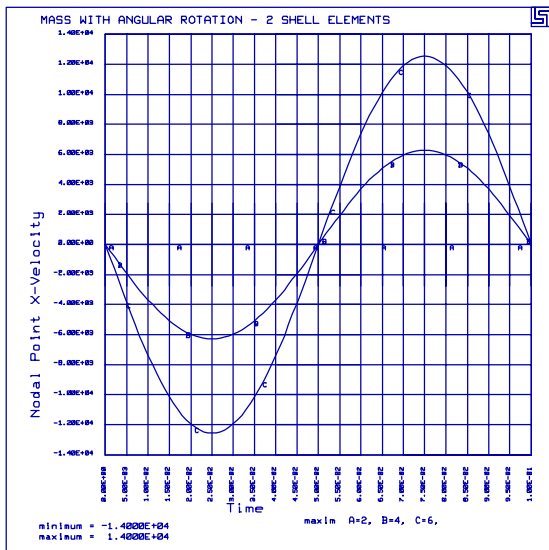
**\*LOAD\_BODY\_GENERALIZED**  
Rotating Elements

**Results:**

taurus g=d3plot  
19  
ytran -80 rx 40 ndplt s 3 over vect velo



phs3  
nodout  
grid oset -1.4e4 1.4e4 x-vel 2 4 6



**\*LOAD\_BODY\_GENERALIZED**

Rotating Elements

---



**LS-DYNA Manual Section:** \*LOAD\_BODY\_Z

**Additional Sections:**

\*RIGIDWALL\_PLANAR

**Example:** Tire Under Gravity Loading Bounces on a Rigid Wall

**Filename:** load\_body.gravity.k

**Description:**

A simple model of a tire is placed under gravity loaded and bounces on a rigid wall.

**Model:**

A positive gravity constant of  $0.00981 \text{ mm/ms}^2$  is used to make the tire drop in the negative z-direction. A \*RIGIDWALL\_PLANAR keyword is used to define the ground. Nodes on the bottom of the tire are prevented from penetrating the rigid wall by specifying them within the \*RIGIDWALL\_PLANAR command (using a \*SET\_NODE\_COLUMN keyword).

**Results:**

The rigid wall forces oscillate about the steady state, which is the weight of the tire ( $W = 0.26 \text{ kN}$ ). Curiously, the tire damps out even though no damping is specified within the model. See the example in \*DAMPING\_GLOBAL for an explanation and fix.





# \*LOAD\_BODY\_Z

## Tire Under Gravity Loading Bounces on a Rigid Wall

```
8913
8914
8919
8920
8921
8922
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$ pid sid mid eosid hgid grav adpopt

wheel
35 1 1
tire
36 1 1
$
$
$$$ Materials
$
*MAT_PIECEWISE_LINEAR_PLASTICITY
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$ mid ro e pr sigy etan eppf tdel
1 0.783E-05 200.0 0.3 0.207 0.750
$ Cowper/Symonds Strain Rate Parameters
$ C p lcss lcsr
40 5
$ Plastic stress/strain curves
0.000 0.080 0.160 0.400 1.000
0.207 0.250 0.275 0.290 0.300
$
$
$
$$$ Sections
$
*SECTION_SHELL
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$ sid elform shrf nip propt qr/irid icomp
1 2 3.0000
$ t1 t2 t3 t4 nloc
1.00 1.00 1.00 1.00
$
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*NODE
$ nid x y z tc rc
8719 -1.16673000E+02 -6.24000000E+02 -1.16673000E+02 0 0
8720 -1.52444000E+02 -6.24000000E+02 -6.31430000E+01 0 0
.
... in total, 82 nodes defined
```

**\*LOAD\_BODY\_Z**

**Tire Under Gravity Loading Bounces on a Rigid Wall**

---

```
.
8931 2.790000000E+02 -7.54000000E+02 0.000000000E+00 0 0
8932 2.577620000E+02 -7.54000000E+02 1.067690000E+02 0 0
$
$$$$$$$ Shell Elements
$
*ELEMENT_SHELL
$  eid      pid      n1      n2      n3      n4
   8710      35      8719      8722      8723      8720
   8711      35      8720      8723      8724      8721
.
... in total, 96 shells defined
.
8948      36      8928      8931      8932      8929
8949      36      8929      8932      8926      8924
$
$$$$$$$ Nodal Mass Elements
$
*ELEMENT_MASS
$  eid      nid      mass
   8730      8730      10.0
   8746      8746      10.0
$
*END
```

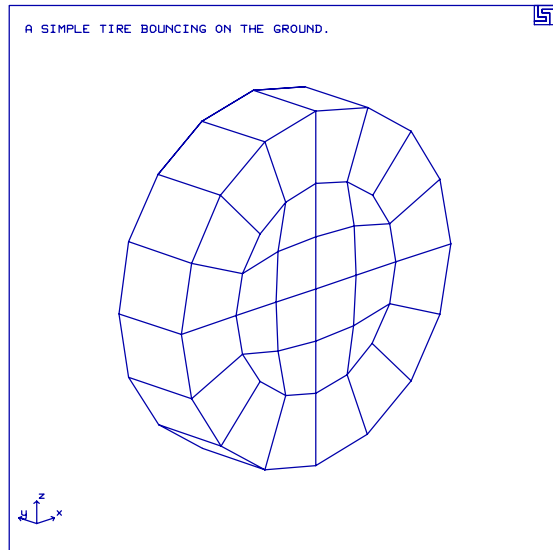
# \*LOAD\_BODY\_Z

## Tire Under Gravity Loading Bounces on a Rigid Wall

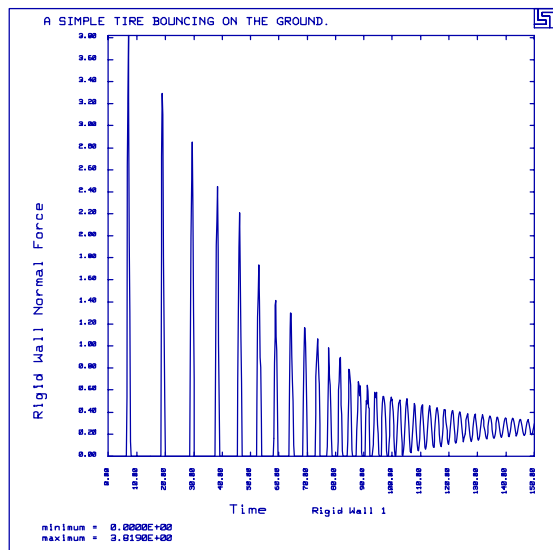
---

### Results:

taurus g=d3plot  
angle 1 rx -90  
ry 45 rx 20 view



phs3  
rwforc  
normal



## \*MAT\_FRAZER\_NASH\_RUBBER\_MODEL

### Frazer-Nash Single Element

---

**LS-DYNA Manual Section:** \*MAT\_FRAZER\_NASH\_RUBBER\_MODEL

**Example:** Frazer-Nash Single Element

**Filename:** mat\_fn\_rubber.element.k

#### **Description:**

This model illustrates the behavior of the Frazer Nash rubber model using a single element.

#### **Model:**

The example contains a single element which measures  $7.5 \times 7.5 \times 100$ . The element is constrained in the z-direction on the bottom and has prescribed velocity on the top surface.

#### **Input:**

Unitary input for any constant indicates least squares curve fitting. (\*MAT\_FRAZER\_NASH\_RUBBER). The least squares curve fit requires specimen dimensions and a stress-strain load curve. The model provides the option to stop the calculation based on maximum and minimum strain values.

#### **Results:**

The compressibility of the element and the pressure versus average strain are shown in the plots..

#### **References:**

Kenchington, D. C.





\*MAT\_FRAZER\_NASH\_RUBBER\_MODEL  
Frazer-Nash Single Element

---

```

$     dt
     0.1
$
*DATABASE_HISTORY_NODE
$     id1      id2      id3      id4      id5      id6      id7      id8
     1
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Boundary Conditions - Prescribed Motion
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*BOUNDARY_PRESCRIBED_MOTION_NODES
$     nid      dof      vad      lcid      sf      vid
     1         4         2         1 4.000E-02     1
     2         4         2         1 4.000E-02     1
     3         4         2         1 4.000E-02     1
     4         4         2         1 4.000E-02     1
$
*DEFINE_VECTOR
$     vid      xt      yt      zt      xh      yh      zh
     1 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00-1.000E+00
$
*DEFINE_CURVE
$     lcid      sidr      scla      sclo      offa      offo
     1
$
     abscissa      ordinate
0.00000000E+00     0.00000000E+00
2.00000000E+00     7.13000011E+00
4.00000000E+00     1.35200005E+01
6.00000000E+00     1.86100006E+01
8.00000000E+00     2.18700008E+01
1.00000000E+01     2.30000000E+01
1.20000000E+01     2.18700008E+01
1.40000000E+01     1.86100006E+01
1.60000000E+01     1.35200005E+01
1.80000000E+01     7.13000011E+00
2.00000000E+01     0.00000000E+00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$     pid      sid      mid      eosid      hgid      adpopt
Rubber
     1         1         1
$
$
$
*MAT_FRAZER_NASH_RUBBER_MODEL
$     mid      ro      pr      c100      c200      c300      c400
     1 1.254E-06     0.495 1.000E+00 0.000E+00
$
$
$     c110      c210      c010      c020      exit      emax      emin
     1.000E+00 0.000E+00 1.000E+00 1.000E+00 1.000E+00 9.000E-01-9.000E-01

```

---

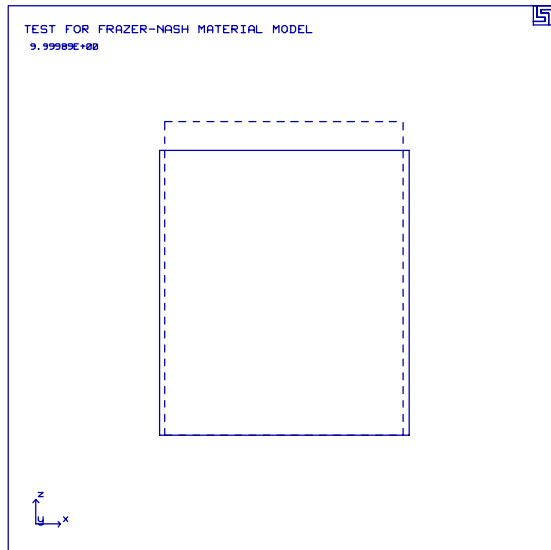


# \*MAT\_FRAZER\_NASH\_RUBBER\_MODEL

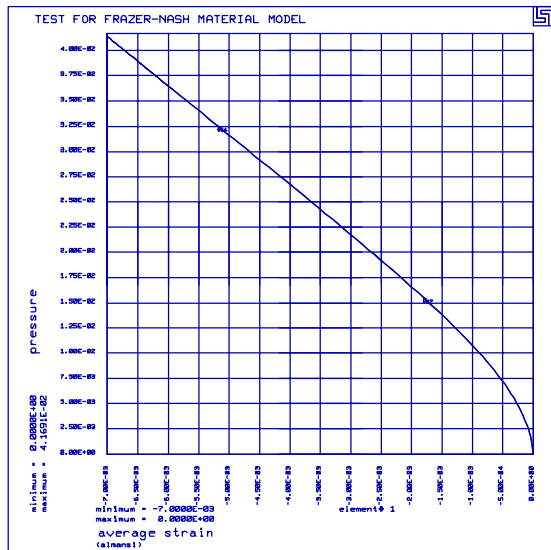
## Frazer-Nash Single Element

### Results:

taurus g=d3plot  
19  
rx -90 angle 1 dist 1000 udg 1 state 101 view



phs2  
element 1 1 gather  
grid aset -7e-3 0 e2hist 8 308 1 1



**\*MAT\_FRAZER\_NASH\_RUBBER\_MODEL**  
Frazer-Nash Single Element

---

## **\*MAT\_PIECEWISE\_LINEAR\_PLASTICITY** Piecewise Linear Plasticity Fragmenting Plate

---

### **LS-DYNA Manual Section:** \*MAT\_PIECEWISE\_LINEAR\_PLASTICITY

**Example:** Piecewise Linear Plasticity Fragmenting Plate

**Filename:** mat\_piecewise\_linear.plate-shatter.k

#### **Description:**

A plate of 1,200 Belytschko-Tsay shell elements strikes a wall at an angle of 45 degrees from the wall normal. The impact velocity is 20,775 in/sec. and the termination time is 0.00025 seconds.

#### **Model:**

The material description contains Young's Modulus, Poisson's ratio, yield stress, hardening modulus, ultimate plastic strain, and time step size for element deletion.

#### **Input:**

One material definition for a Belytschko-Tsay shell with viscous hourglass control (\*CONTROL\_HOURLASS). Young's Modulus, Poisson's ratio, yield stress and the hardening modulus are 16 Msi, 0.35, 155,000 psi, and 192,000 psi respectively. (\*MAT\_LINEAR\_PIECEWISE\_PLASTICITY). The plastic strain at failure is 32% and the failure minimum time step size is 0.3  $\mu$ seconds.

#### **Results:**

The plate deforms away from the stonewall and the plate fragments.

# \*MAT\_PIECEWISE\_LINEAR\_PLASTICITY

## Piecewise Linear Plasticity Fragmenting Plate

---

### List of LS-DYNA input deck:

```
*KEYWORD
*TITLE
Test for Material 24 with Failure
$
$ LSTC Example
$
$ Last Modified: September 18, 1997
$
$ Units: lbf-s2/in, in, s, lbf, psi, lbf-in
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1.>....2.>....3.>....4.>....5.>....6.>....7.>....8
$
*CONTROL_TERMINATION
$  endtim    endcyc    dtmin    endneg    endmas
   2.500E-04          5.000E-02
$
*CONTROL_CONTACT
$  slsfac    rwpnal    islchk    shlthk    penopt    thkchg    orien
   0.01
$  usrstr    usrfac    nsbcs    interm    xpenen
$
$
*CONTROL_HOURLGLASS
$   ihq        qh
      4
$
*DATABASE_BINARY_D3PLOT
$  dt/cycl    lcdt
   1.250E-05
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Initial Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>....1.>....2.>....3.>....4.>....5.>....6.>....7.>....8
$
$$$$ All nodes except nodes in node set 1 are given an initial velocity.
$$$$ Node set 1 contains the nodes of the wall.
$
*INITIAL_VELOCITY
$  nsid    nsidex    boxid
                             1
$
$  vx      vy      vz      vxr      vyr      vzr
-1.469E+04-1.469E+04 0.000E+00 0.000E+00 0.000E+00 0.000E+00
$
$  vx     vye     vze     vxre     vyre     vzre
$
$
*SET_NODE_LIST
$  sid
   1
$  nid1    nid2    nid3    nid4    nid5    nid6    nid7    nid8
   1282    1283    1284    1285
```



# **\*MAT\_PIECEWISE\_LINEAR\_PLASTICITY**

## **Piecewise Linear Plasticity Fragmenting Plate**

---

```
*NODE
$  node          x          y          z          tc          rc
   1  0.000000E+00  0.000000E+00  0.000000E+00    0          0
   .
   ... in total, 1285 nodes defined
   .
  1285 -5.000000E-02 -1.000000E+01  5.000000E+00    7          7
$
$$$$$ Shell Elements
$
*ELEMENT_SHELL
$  eid          pid          n1          n2          n3          n4
   1           2           22           1           2           23
   .
   ... in total, 1201 shells defined
   .
  1201          3          1282          1283          1284          1285
$
*END
```



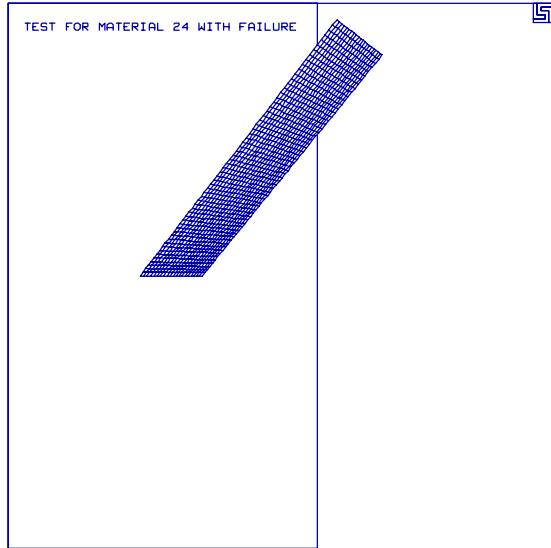
# \*MAT\_PIECEWISE\_LINEAR\_PLASTICITY

## Piecewise Linear Plasticity Fragmenting Plate

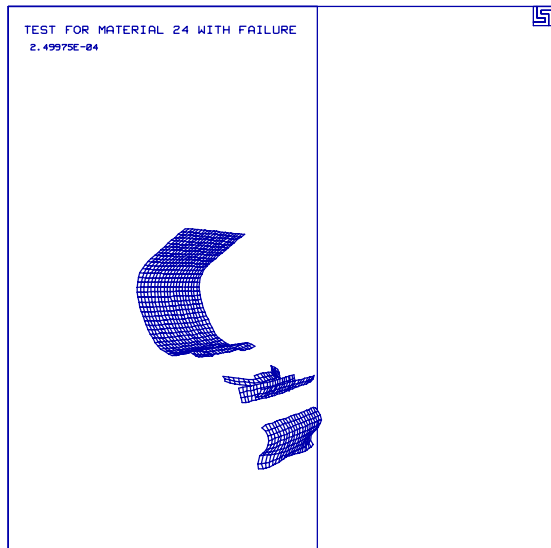
---

**Results:**

taurus g=d3plot  
19  
ry -30 dist 12 view



state 21  
view



**\*MAT\_PIECEWISE\_LINEAR\_PLASTICITY**  
Piecewise Linear Plasticity Fragmenting Plate

---

**LS-DYNA Manual Section:** \*MAT\_RIGID**Additional Sections:**

\*DEFINE\_COORDINATE\_VECTOR  
\*LOAD\_SEGMENT

**Example:** Rigid Sliding Block in Local Coordinate System

**Filename:** mat\_rigid.block-slide.k

**Description:**

A center of mass is constrained to slide along a local coordinate system. The termination time is 0.010 seconds.

**Model:**

The material description references a local coordinate system to constrain the rigid block. The rigid block is free to translate along the local z axis.

**Input:**

The material definition is a rigid material (\*MAT\_RIGID). The material specifies the use of a local coordinate system, the local coordinate constraint value of 100111 (tx ty tz rx ry rz), and the local coordinate system for output. The local coordinate system specifies that the local origin is the global origin, the local x-axis point is (1.0,0.0,1.0) and the local y-axis point is (0.0,0.0,1.0) (\*DEFINE\_COORDINATE\_VECTOR).

A shell element is defined in order to control the timestep.

**Results:**

The block slides along the local coordinate system.





## \*MAT\_RIGID

### Rigid Sliding Block in Local Coordinate System

---

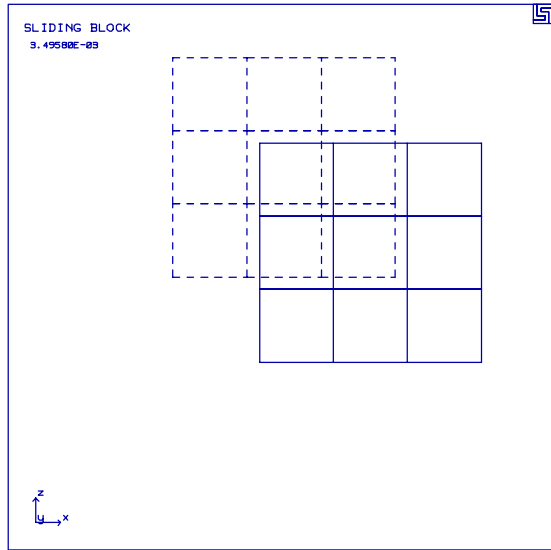
```

      1      1      1      2      6      5      17      18      22      21
      2      1      2      3      7      6      18      19      23      22
      3      1      3      4      8      7      19      20      24      23
      .
      ... in total, 27 solids defined
      .
      25      1      41      42      46      45      57      58      62      61
      26      1      42      43      47      46      58      59      63      62
      27      1      43      44      48      47      59      60      64      63
$
$$$$$ Shell Element - used to control the timestep
$
*ELEMENT_SHELL
$   eid      pid      n1      n2      n3      n4
   1         2         65         67         68         66
*END
```

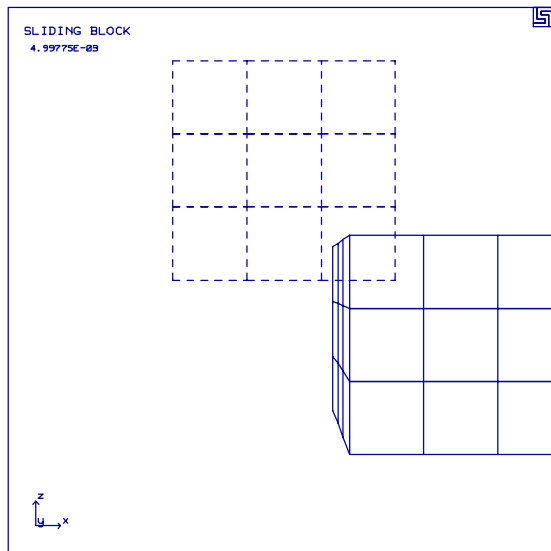
# Rigid Sliding Block in Local Coordinate System

**Results:**

taurus g=d3plot  
19  
m 1 udg 1 rx -90 state 8 view



state 11  
view



**\*MAT\_RIGID**

Rigid Sliding Block in Local Coordinate System

---



**LS-DYNA Manual Section:** \*MAT\_SOIL\_AND\_FOAM

**Example:** Soil and Foam Single Element

**Filename:** mat\_soil\_foam.element.k

**Description:**

This problem contains a single element with one degree of freedom on a side. The element compresses and expands.

**Model:**

The element measures 100 cubic inches. One side follows a velocity curve which results in a range of relative volume ( $V/V_0$ ) 1.000 to 0.0091 to 1.441.

**Input:**

The foam follows a pressure volumetric strain relationship (\*MAT\_SOIL\_AND\_FOAM). The unloading behavior may follow either the unloading bulk modulus or the loading curve. The unloading in the first case follows the bulk modulus, while the unloading in the second case follows the loading curve. The material has a cutoff pressure of 0.5.

**Results:**

The plots show the element pressure versus time.







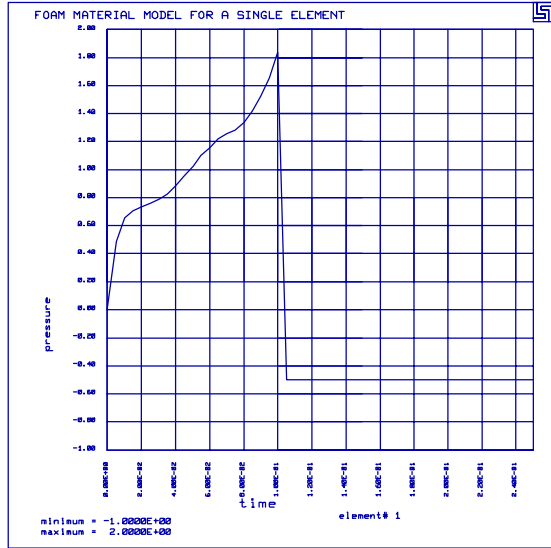
Results:

**Volumetric Crushing**

taurus g=d3plot

19

phs2 elem 1 1 gather grid oset -1 2 etime 8 1 1

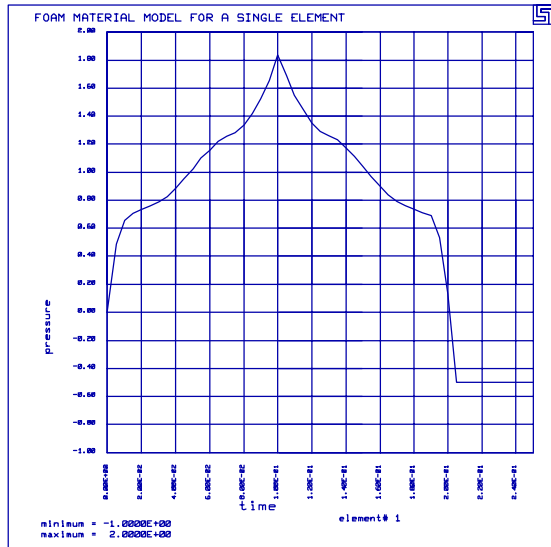


**Unloading Follows Loading Curve**

taurus g=d3plot

phs2

elem 1 1 gather grid oset -1 2 etime 8 1 1



**\*MAT\_SOIL\_AND\_FOAM**  
Soil and Foam Single Element

---

**LS-DYNA Manual Section:** \*MAT\_SPRING

**Additional Sections:**

- \*CONSTRAINED\_EXTRA\_NODES\_SET
- \*CONSTRAINED\_JOINT\_SPHERICAL
- \*CONTACT\_SURFACE\_TO\_SURFACE
- \*DEFINE\_SD\_ORIENTATION
- \*ELEMENT\_DISCRETE
- \*LOAD\_BODY\_Z
- \*MAT\_DAMPER\_VISCOUS
- \*PART\_INERTIA

**Example:** Belted Dummy with Springs

**Filename:** mat\_spring.belted-dummy.k

**Description:**

This is a simulation of the interaction between a dummy and seating system. The dummy has an initial velocity, base vehicle acceleration, and decelerated base.

**Model:**

The dummy consists of 15 ellipsoidal rigid bodies connected through cylindrical joints, springs and dampers. The base of the seat belts and the seat decelerates backwards relative to the dummy.

**Input:**

The dummy consists of rigid bodies 1 through 15. Materials 16 through 20 define the seat and material 21 and 22 define the seat belt. The rigid bodies are constrained with respect to each other with spherical joints (\*CONSTRAINED\_JOINT\_SPHERICAL). Discrete springs and dampers between the rigid body provide the relative stiffness and viscosity. The initial velocity of all nodes is 14.8 units, while the acceleration of the seat and belt ends follow an acceleration curve in the opposite direction.

**Results:**

LS-DYNA predicts that the dummy slides under the seat belts.

**Reference:**

Stillman, D. W.

# \*MAT\_SPRING

## Belted Dummy with Springs

---

### List of LS-DYNA input deck:

```

*KEYWORD
*TITLE
Belted Dummy
$
$ LSTC Example
$
$ Last Modified: September 19, 1997
$
$ Units: kg, m, s, N, Pa, Joule
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTROL_TERMINATION
$ endtim endcyc dtmin endneg endmas
1.200E-01
$
*CONTROL_CONTACT
$ slsfac rwpnal islchk shlthk penopt thkchg orien
2
$ usrstr usrfac nsbcs interm xpenen
$
$
*CONTROL_TIMESTEP
$ dtinit scft isdo tslimt dtms lctm erode mslst
0.000E+00 8.000E-01 0 0.000E+00 0.000E+00 0 0
$
$
*DATABASE_BINARY_D3PLOT
$ dt/cycl lcdt
2.500E-03
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Initial Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
$$$$ All nodes are given an initial velocity.
$
*INITIAL_VELOCITY
$ nsid nsidex boxid
0
$
$ vx vy vz vxr vyr vzr
1.480E+01 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Boundary Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$

```





**\*MAT\_SPRING**  
**Belted Dummy with Springs**

---

```

$      lcid      sf      lciddr
      51      1.00      0
$
*DEFINE_CURVE
$      lcid      sidr      scla      sclo      offa      offo
      51
$      abscissa      ordinate
      0.00000000E+00      9.81
      1.51999995E-01      9.81
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$ Contacts - Sliding Interfaces
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
$$$$$ The segment sets associated with these contacts are located at the end
$$$$$ of this file.
$
*CONTACT_SURFACE_TO_SURFACE
$      ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
      1      2      0      0
$      fs      fd      dc      vc      vdc      penchk      bt      dt
      6.200E-01
$      sfs      sfm      sst      mst      sfst      sfmt      fsf      vsf
$
*CONTACT_SURFACE_TO_SURFACE
$      ssid      msid      sstyp      mstyp      sboxid      mboxid      spr      mpr
      3      4      0      0
$      fs      fd      dc      vc      vdc      penchk      bt      dt
      6.200E-01
$      sfs      sfm      sst      mst      sfst      sfmt      fsf      vsf
$
*CONTACT_SURFACE_TO_SURFACE
      5      6      0      0
      6.200E-01
$
*CONTACT_SURFACE_TO_SURFACE
      7      8      0      0
      8.000E-01
$
*CONTACT_SURFACE_TO_SURFACE
      9      10      0      0
      1.000E+00
$
*CONTACT_SURFACE_TO_SURFACE
      11      12      0      0
      8.000E-01
$
*CONTACT_SURFACE_TO_SURFACE
      13      14      0      0
      8.800E-01
$

```

**\*MAT\_SPRING**  
**Belted Dummy with Springs**

---

```
*CONTACT_SURFACE_TO_SURFACE
    15      16      0      0
  8.800E-01

$
*CONTACT_SURFACE_TO_SURFACE
    17      18      0      0
  1.600E-01

$
*CONTACT_SURFACE_TO_SURFACE
    19      20      0      0
  8.800E-01

$
*CONTACT_SURFACE_TO_SURFACE
    21      22      0      0
  0.000E+00

$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Constraints
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
*CONSTRAINED_JOINT_SPHERICAL
$   n1      n2      n3      n4      n5      rps      damp
    99      227      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
    228      405      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
    406      865      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
    866      971      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
    407      537      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
    538      685      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
    408      603      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
    604      763      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
    972     1097      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
    1098     1497      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
    1498     1645      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
    973     1317      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
    1318     1579      0      0      0      0 0.000E+00
*CONSTRAINED_JOINT_SPHERICAL
    1580     1733      0      0      0      0 0.000E+00

$
$
*CONSTRAINED_EXTRA_NODES_SET
$   pid      nsid
    1        2
```

---

**\*MAT\_SPRING**  
**Belted Dummy with Springs**

---

```

$
*SET_NODE_LIST
$   sid
    2
$   nid1      nid2      nid3      nid4      nid5
    99       100       101       102
$
.
... in total, 15 extra_nodes_set & set_node_list pairs defined
.
$
*CONSTRAINED_EXTRA_NODES_SET
$   pid      nsid
    2        3
$
*SET_NODE_LIST
$   sid
    3
$   nid1      nid2      nid3      nid4      nid5      nid6      nid7      nid8
    227       228       229       230       231       232       233       234
$
$
$$$$ Define Spring Orientation Vectors and Curves
$
$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*DEFINE_SD_ORIENTATION
$   vid      iop      xt      yt      zt      nid1      nid2
    1        2 0.000E+00 0.000E+00 0.000E+00      100       229
    2        2 0.000E+00 0.000E+00 0.000E+00      101       230
    3        2 0.000E+00 0.000E+00 0.000E+00      102       231
.
... in total, 42 sd_orientation vectors defined
.
    40       2 0.000E+00 0.000E+00 0.000E+00      1584      1734
    41       2 0.000E+00 0.000E+00 0.000E+00      1585      1735
    42       2 0.000E+00 0.000E+00 0.000E+00      1586      1736
$
$$$$ Define Curves
$
*DEFINE_CURVE
$   lcid      sidr      scla      sclo      offa      offo
    1
$   abscissa      ordinate
-1.71000004E+00    -5.38000000E+02
-7.09999979E-01    -8.47500000E+01
-6.80000007E-01    -7.76600037E+01
-6.60000026E-01    -7.10599976E+01
-5.89999974E-01    -5.36800003E+01
-5.00000000E-01    -4.05800018E+01
-3.89999986E-01    -2.99799995E+01
-2.09999997E-02    -4.65000010E+00
0.00000000E+00     0.00000000E+00
2.09999997E-02     4.65000010E+00
3.89999986E-01     2.99799995E+01
5.00000000E-01     4.05800018E+01
5.89999974E-01     5.36800003E+01

```



# \*MAT\_SPRING

## Belted Dummy with Springs

---

```

part-22
  22      22      22      0
spring 101
  101     101     101
$
.
... spring pid's 102-207 also defined here
.
$
spring 208
  208     208     208
$
$$$$$$$$ Materials
$
$
$$$$ Rigid Materials
$
*MAT_RIGID
$   mid      ro      e      pr      n      couple      m      alias
    1 4.064E+03 4.000E+08 3.000E-01 0.000E+00 0.000E+00 0.000E+00
    0.000E+00 0.000E+00 0.000E+00
    0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
$
.
... mat_rigid mid's 2-14 also defined here
.
$
*MAT_RIGID
$   mid      ro      e      pr      n      couple      m      alias
    15 2.000E+03 4.000E+08 3.000E-01 0.000E+00 0.000E+00 0.000E+00
    0.000E+00 0.000E+00 0.000E+00
    0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00 0.000E+00
$
$
$$$$ Elastic Materials
$
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    16 4.646E+03 4.000E+08 3.000E-01
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    17 4.646E+03 4.000E+08 3.000E-01
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    18 4.646E+03 4.000E+09 3.000E-01
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    19 4.646E+03 4.000E+08 3.000E-01

*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    20 2.000E+03 4.100E+08 3.000E-01
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    21 2.000E+03 4.100E+08 3.000E-01
*MAT_ELASTIC
$   mid      ro      e      pr      da      db      k
    22 4.000E+03 2.000E+08 3.000E-01
$
$
$$$$ Nonlinear Elastic Spring Materials
$
*MAT_SPRING_NONLINEAR_ELASTIC

```

**\*MAT\_SPRING**  
**Belted Dummy with Springs**

---

```

101      1
$
.
... mat_spring_nonlinear_elastic mid's 101-142 also defined here
.
$
*MAT_SPRING_NONLINEAR_ELASTIC
142      42
$
$
$$$$ Viscous Damper Materials
$
*MAT_DAMPER_VISCOUS
143 2.300E+00
$
.
... mat_damper_viscous mid's 143-184 also defined here
.
$
*MAT_DAMPER_VISCOUS
184 1.000E+00
$
$
$$$$ Nonlinear Viscous Damper Materials
$
*MAT_DAMPER_NONLINEAR_VISCOUS
185      43
$
.
... mat_damper_nonlinear_viscous mid's 185-208 also defined here
.
$
*MAT_DAMPER_NONLINEAR_VISCOUS
208      49
$
$
$$$$$$$$ Sections
$
$$$$ Shell Sections
$
*SECTION_SHELL
$   sid   elform      shrf      nip      propt   qr/irid   icomp
$     1     0 0.000E+00 0.000E+00 0.000E+00
$    t1     t2     t3     t4     nloc
1.000E-02 1.000E-02 1.000E-02 1.000E-02 0.000E+00
$
.
... shell sid's 2-21 also defined here
.
$
*SECTION_SHELL
$   sid   elform      shrf      nip      propt   qr/irid   icomp
$    22     0 0.000E+00 0.000E+00 0.000E+00
1.000E-02 1.000E-02 1.000E-02 1.000E-02 0.000E+00
$
$
$$$$ Spring-Damper Sections
$
*SECTION_SPRING-DAMPER
101      1 0.000E+00 0.000E+00 0.000E+00 0.000E+00

```

---

**\*MAT\_SPRING**  
**Belted Dummy with Springs**

---

```
0.000E+00 0.000E+00
$
.
... spring-damper sid's 102-207 also defined here
.
$
*SECTION_SPRING-DAMPER
    208      1 0.000E+00 0.000E+00 0.000E+00 0.000E+00
0.000E+00 0.000E+00
$
$$$$$ Define Nodes and Elements
$
$$$$$
$
...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*NODE
$ node           x           y           z           tc           rc
    1-2.416931689E-01-3.286990896E-02 5.876007080E-01    0    0
    2-2.475307435E-01-1.784761623E-02 5.820254087E-01    0    0
    3-2.498186529E-01-1.089885016E-03 5.798402429E-01    0    0
.
... in total, 2043 nodes defined
.
    2041-5.439429283E-01 2.696031034E-01 6.014695168E-01    0    0
    2042-5.649484396E-01 2.777405977E-01 6.089934111E-01    0    0
    2043-5.859540105E-01 2.858780622E-01 6.165173650E-01    5    0
$
$$$$$ Shell Elements
$
*ELEMENT_SHELL
$ eid    pid    n1     n2     n3     n4
    1     1     1      4      5      2
    2     1     2      5      6      3
    3     1     4      7      8      5
.
... in total, 1950 shells defined
.
    1948     22     394     357     365     403
    1949     22     403     365     367     404
    1950     22     404     367     369     379
$
$$$$$ Discrete Elements
$
*ELEMENT_DISCRETE
$ eid    pid    n1     n2     vid    s         pf    offset
    1     101     1     129     1 0.00000000E+00    1
    2     102     1     129     2 0.00000000E+00    1
    3     103     1     129     3 0.00000000E+00    1
.
... in total, 108 discrete elements defined
.
    106     206     1505     1675     41 0.00000000E+00    1
    107     207     1505     1675     42 0.00000000E+00    1
    108     208     1505     1675     40 0.00000000E+00    1
$
$$$$$
$
$$$$$ Segment sets for the contacts defined previously.
$
$$$$$
```

---



**\*MAT\_SPRING**  
**Belted Dummy with Springs**

---

```
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*SET_SEGMENT
$   sid      da1
    1         4
$   n1      n2      n3      n4
    1780    1783    1784    1781
    1783    1786    1787    1784
    1781    1784    1785    1782
    1784    1787    1788    1785
.
... in total, 22 segment sets defined for the contacts
.
$
*END
```

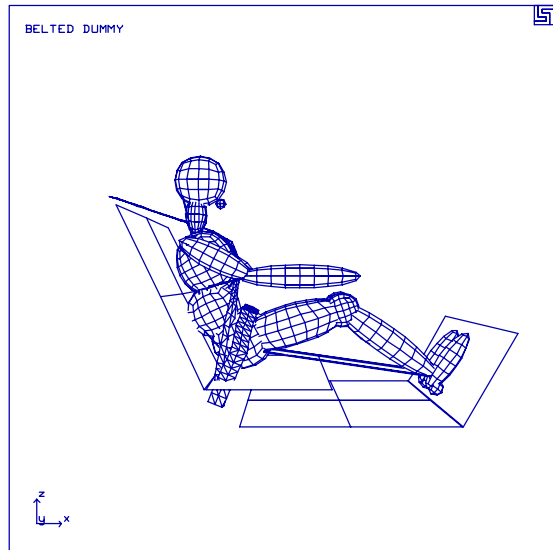
# \*MAT\_SPRING

## Belted Dummy with Springs

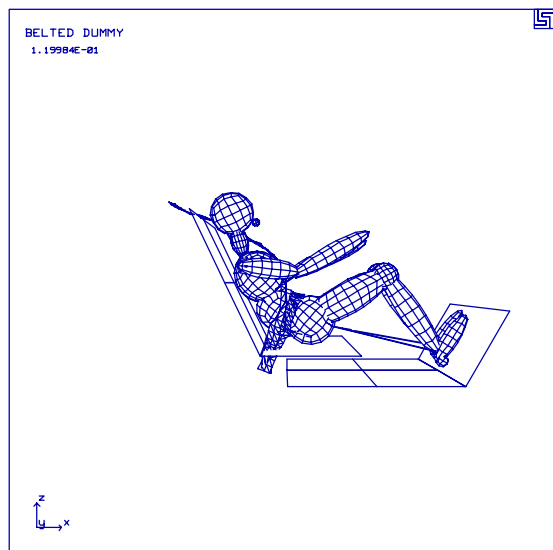
---

**Results:**

taurus g=d3plot  
19  
rx -90 center view



state 49  
center  
view



## \*MAT\_TRANSVERSELY\_ANISOTROPIC Rectangular Cup Drawing

---

**LS-DYNA Manual Section:** \*MAT\_TRANSVERSELY\_ANISOTROPIC

**Additional Sections:**

\*CONTACT\_ONE\_WAY\_SURFACE\_TO\_SURFACE  
\*LOAD\_SHELL\_ELEMENT

**Example:** Rectangular Cup Drawing

**Filename:** mat\_transversely\_anisotropic.cup-draw.k

**Description:**

This problem includes three tools a punch, a holder and a die, and a blank. The blank is drawn by moving the punch downwards to form around the die. The blank uses the \*MAT\_TRANSVERSELY\_ANISOTROPIC\_ELASTIC\_PLASTIC material model.

**Model:**

The \*BOUNDARY\_PRESCRIBED\_MOTION\_RIGID keyword is used to give the punch a prescribed velocity in the z-direction. All shells on the holder are given a pressure load to clamp down on the blank (\*LOAD\_SHELL\_ELEMENT). One way surface to surface contact is defined between the major parts in the model. Because of symmetry, only 1/4 of the system is modeled.

**Results:**

A contour plot of the effective stress on the blank after drawing is shown.



**\*MAT\_TRANSVERSELY\_ANISOTROPIC**  
**Rectangular Cup Drawing**

---

```
      0      0      3      1      1      1      1      1
$   cmpflg   ieverp   beamip
      0      1      0
$
*DATABASE_GLSTAT
  0.0001
$
*DATABASE_RCFORC
  0.0001
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Curves
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*DEFINE_CURVE
$   lcid      sidr      scla      sclo      offa      offo
      1         0        1.0       1.0     2.0E-03     0.0
$
$   abscissa      ordinate
  0.000000E+00,   0.000000E+00
  3.000000E-04,   1.644664E+00
  6.000000E-04,   3.287704E+00
      .
      ... in total, 102 points defined for this curve
      .
  2.970000E-02,   1.644661E+00
  3.000000E-02,   0.000000E+00
  100.0000E-03,   0.000000E+00
$
$
*DEFINE_CURVE
$   lcid      sidr      scla      sclo      offa      offo
      2
$   absc      ordin
  0.0000, 127.55
  0.00598, 129.69
  0.0119, 156.99
  0.0178, 171.96
  0.0180, 182.50
  0.0296, 205.95
  0.0583, 252.14
  0.0860, 283.72
  0.1345, 319.43
  0.1660, 336.81
  0.2150, 358.25
  0.2620, 376.45
  0.3070, 389.14
  0.3290, 394.86
  0.6000, 394.86
$
$
*DEFINE_CURVE
$   lcid      sidr      scla      sclo      offa      offo
      3
$   absc      ordin
  0.0, 0.0
  1.0, 0.413E05
```

---

## \*MAT\_TRANSVERSELY\_ANISOTROPIC

### Rectangular Cup Drawing

---

```

$
$
*DEFINE_CURVE
$      lcid      sidr      scla      sclo      offa      offo
$          4
$ absc      ordin
$      0.0,      0.0
$      1.0,      1.0
$
$
*DEFINE_CURVE
$      lcid      sidr      scla      sclo      offa      offo
$          5
$      absc      ordin
$          0.0,      0.0
$       1.0E-03,      5.0
$     150.0E-03,      5.0
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Boundary Motion Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$    The punch (part 4) is given a prescribed velocity in the z-direction.
$$$    Velocity follows curve 1 (scaled by -20).
$
*BOUNDARY_PRESCRIBED_MOTION_RIGID
$      nid      dof      vad      lcid      sf      vid
$          4          3          0          1       -20.0
$
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
$$$$$  PARTS
$
*PART
$      pid      sid      mid      eosid      hgid      grav      adpopt
blank      1          1          1
die         2          2          2
holder      3          2          3
punch       4          2          3
$
$
$$$$$  Materials
$
*MAT_TRANSVERSELY_ANISOTROPIC_ELASTIC_PLASTIC
$
$ mat #37
$      mid      ro      e      pr      sigy      etan      r      hlcid
$          1 0.787E-08 0.207E+06 0.280 127.6 0.0 1.0 2.0
$

```

---









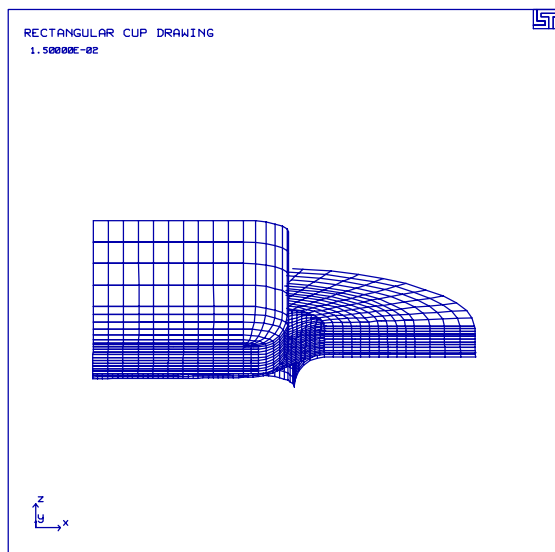
# \*MAT\_TRANSVERSELY\_ANISOTROPIC

## Rectangular Cup Drawing

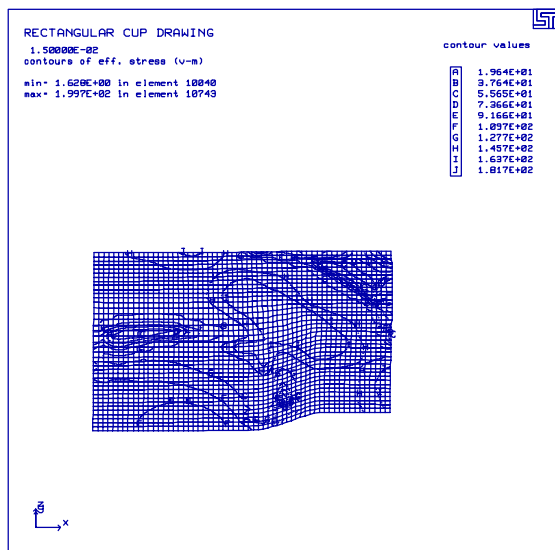
---

### Results:

taurus g=d3plot  
angle 1 rx -90  
state 20 view



m 1  
numc 10 mono  
rx 25 contour 9



## **\*RIGIDWALL\_GEOMETRIC\_SPHERE\_MOTION**

### Rigid Wall Sphere Impacts a Plate

---

#### **LS-DYNA Manual Section:** \*RIGIDWALL\_GEOMETRIC\_SPHERE\_MOTION

**Example:** Rigid Wall Sphere Impacts a Plate

**Filename:** rigidwall\_geometric\_sphere.plate.k

#### **Description:**

A “Stonewall” - sphere impacts an elastic plate. (The sphere will not be shown in LS-TAURUS.)

#### **Model:**

The plate has an elastic material model with Belytschko-Tsay shell formulation. The plate is  $40 \times 40 \times 2 \text{ mm}^3$ . The sphere has a radius of 8 mm and its center is 9 mm above the plate. The sphere moves towards the plate with a prescribed displacement resulting in a velocity of velocity of 3 mm/second.

#### **Input:**

A spherical stonewall surface represents the true geometry of the ball. (\*RIGIDWALL\_GEOMETRIC\_SPHERE\_MOTION). The stonewall cards contain direction and load curve number defining the motion. All nodes of the plate are prevented from penetrating the sphere

#### **Reference:**

Schweizerhof, K. and Weimer, K.



## \*RIGIDWALL\_GEOMETRIC\_SPHERE\_MOTION Rigid Wall Sphere Impacts a Plate

```

1         1         0.0       0.0       -1.0
$
$
*DEFINE_CURVE
$      lcid       sidr       scla       sclo       offa       offo
$          1
$      abscissa          ordinate
$              0.0             0.0
$              0.0005          15.0
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*PART
$      pid       sid       mid       eosid       hgid       adpopt
plate
$          1         1         1
$
$
*MAT_ELASTIC
$      mid       ro        e        pr        da        db        k
$          1    2.00e-08    100000.    0.300
$
$
*SECTION_SHELL
$      sid       elform      shrf      nip      propt      qr/irid      icomp
$          1             0.83333      2.0       3.0
$      t1       t2       t3       t4       nloc
$      2.0       2.0       2.0       2.0
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Nodes on the outside edges of the plate are constrained in z-translation.
$
*NODE
$      node      x              y              z              tc       rc
$      1     0.000000E+00    0.000000E+00    0.000000E+00     3        0
$      2     5.000000E+00    0.000000E+00    0.000000E+00     3        0
$      3     1.000000E+01    0.000000E+00    0.000000E+00     3        0
$
$      ... in total, 81 nodes defined
$
$      79     3.000000E+01    4.000000E+01    0.000000E+00     3        0
$      80     3.500000E+01    4.000000E+01    0.000000E+00     3        0
$      81     4.000000E+01    4.000000E+01    0.000000E+00     3        0
$
$$$$ Shell Elements
$
*ELEMENT_SHELL
$      eid       pid       n1       n2       n3       n4
$      1         1         1         2         11        10
$      2         1         2         3         12        11
$      3         1         3         4         13        12

```

# **\*RIGIDWALL\_GEOMETRIC\_SPHERE\_MOTION**

## **Rigid Wall Sphere Impacts a Plate**

---

.  
... in total, 64 shells defined

62	1	69	70	79	78
63	1	70	71	80	79
64	1	71	72	81	80

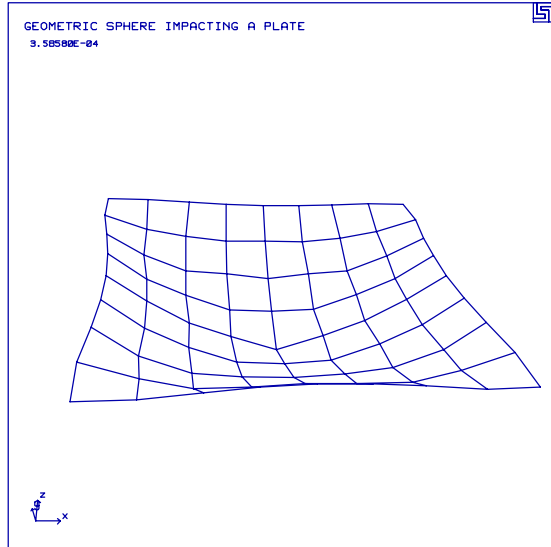
.\$  
\*END

# \*RIGIDWALL\_GEOMETRIC\_SPHERE\_MOTION

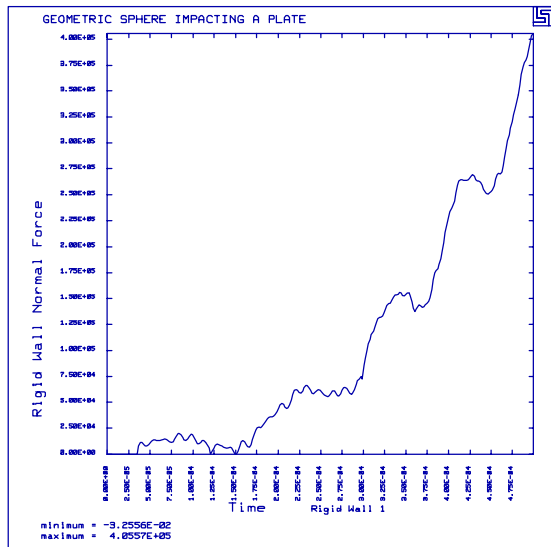
## Rigid Wall Sphere Impacts a Plate

### Results:

taurus g=d3plot  
19  
rx -60 ry 10 state 19 view



phs3  
rwforc  
normal



**\*RIGIDWALL\_GEOMETRIC\_SPHERE\_MOTION**

Rigid Wall Sphere Impacts a Plate

---



**LS-DYNA Manual Section:** \*RIGIDWALL\_PLANAR

**Additional Sections:**

\*INITIAL\_VELOCITY\_NODE

**Example:** Rotating Shell Strikes Rigid Wall

**Filename:** rigidwall\_planar.shell.k

**Description:**

A rotating shell element strikes and rebounds from a rigid wall surface. The plate is modeled with shell elements for viewing in LS-TAURUS. This does not affect the calculation.

**Model:**

The shell element has an elastic material model with Belytschko-Tsay shell formulation. The plate measures  $10 \times 10 \times 2 \text{ mm}^3$ . The plate has an initial velocity of 100,000 mm/second in negative z-direction and an initial angular velocity of 100,000 radians/second about the y-axis. The rigid surface is modeled by an infinite smooth stonewall surface.

**Input:**

Nodes requiring initial velocity are specified with \*INITIAL\_VELOCITY\_NODE. The location of the “Stonewall” is in the x-y plane with  $z=0$  (\*RIGIDWALL\_PLANAR). The 4 nodes belonging to the shell element are slave nodes in the stonewall definition. The velocity components of the slave nodes in the normal direction to the stonewall are reset to zero at the moment of impact.

**Reference:**

Schweizerhof, K. and Weimer, K.

# **\*RIGIDWALL\_PLANAR**

## Rotating Shell Strikes Rigid Wall

### List of LS-DYNA input deck:

```
*KEYWORD
*TITLE
STONEWALL SURFACE
$
$  LSTC Example
$
$  Last Modified: September 23, 1997
$
$  Units: ton, mm, s, N, MPa, N-mm
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Control Ouput
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*CONTROL_TERMINATION
$  endtim  endcyc  dtmin  endneg  endmas
  2.000E-04
$
*CONTROL_ENERGY
$   hgen  rwen  slnten  rylen
     2     2
$
$
$
*DATABASE_BINARY_D3PLOT
$   dt  lcdt
  1.000E-05
$
*DATABASE_BINARY_D3THDT
$   dt  lcdt
  2.000E-03
$
$
*DATABASE_GLSTAT
$   dt
  4.0e-06
$
*DATABASE_NODOUT
$   dt
  4.0e-06
$
$
*DATABASE_HISTORY_NODE
$   i      i      i      i      i      i      i      i      i
$  id1    id2    id3    id4    id5    id6    id7    id8
     12     13     101
$
$
*DATABASE_RWFORC
$   dt
  4.0e-06
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$$  Rigidwalls
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
```



**\*RIGIDWALL\_PLANAR**  
**Rotating Shell Strikes Rigid Wall**

```

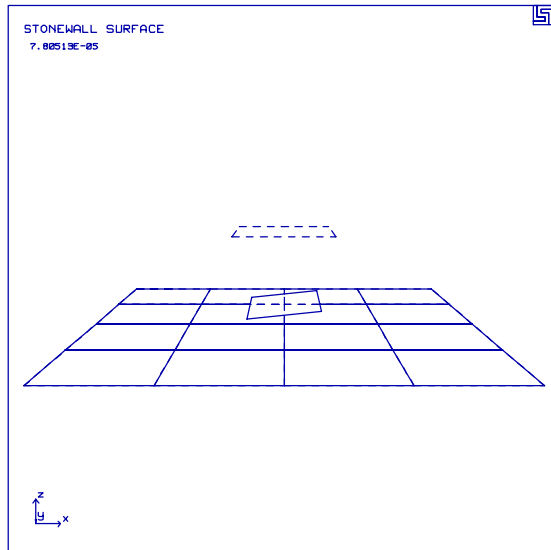
1 2 0.83333 2.000E+00 3.000E+00 0.000E+00
$ t1 t2 t3 t4 nloc
1.000E+00 1.000E+00 1.000E+00 1.000E+00 0.000E+00
$
*SECTION_SHELL
$ sid elform shrf nip propt qr/irid icom
2 2 0.83333 2.000E+00 3.000E+00 0.000E+00
$ t1 t2 t3 t4 nloc
2.000E+00 2.000E+00 2.000E+00 2.000E+00 0.000E+00
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Nodes and Elements
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$.>...1.>...2.>...3.>...4.>...5.>...6.>...7.>...8
$
*NODE
$ node x y z tc rc
1 0.000000000E+00 0.000000000E+00 0.000000000E+00 7 0
2 1.000000000E+01 0.000000000E+00 0.000000000E+00 7 0
3 2.000000000E+01 0.000000000E+00 0.000000000E+00 7 0
.
... in total, 29 nodes defined
.
102 2.500000000E+01 1.500000000E+01 1.000000000E+01 0 0
103 1.500000000E+01 2.500000000E+01 1.000000000E+01 0 0
104 2.500000000E+01 2.500000000E+01 1.000000000E+01 0 0
$
$$$$ Shell Elements - All shells except 101 are for display of the Rigidwall
$
*ELEMENT_SHELL
$ eid pid n1 n2 n3 n4
1 1 1 2 7 6
2 1 2 3 8 7
3 1 3 4 9 8
4 1 4 5 10 9
5 1 6 7 12 11
6 1 7 8 13 12
7 1 8 9 14 13
8 1 9 10 15 14
9 1 11 12 17 16
10 1 12 13 18 17
11 1 13 14 19 18
12 1 14 15 20 19
13 1 16 17 22 21
14 1 17 18 23 22
15 1 18 19 24 23
16 1 19 20 25 24
101 2 101 102 104 103
$
*END

```

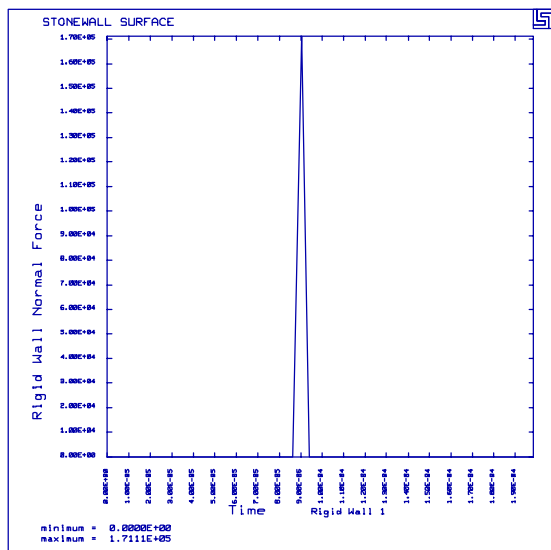
# \*RIGIDWALL\_PLANAR Rotating Shell Strikes Rigid Wall

## Results:

taurus g=d3plot  
19  
udg 1 state 9 rx -80 view



phs3  
rwforc  
normal



**\*RIGIDWALL\_PLANAR**

Rotating Shell Strikes Rigid Wall

---

**LS-DYNA Manual Section:** \*RIGIDWALL\_PLANAR\_FORCES

**Example:** Cube Rebounding

**Filename:** rigidwall\_planar.cube.k

**Description:**

A cube impacts and rebounds from a rigid plate (“Stonewall”). The plate is modeled with shell elements for viewing in LS-TAURUS.

**Model:**

The cube measures  $10 \times 10 \times 10 \text{ mm}^3$  and is 10 mm above the rigid plate. It has 8 brick elements with elastic material properties. The initial velocity of the cube is 100,000 mm/second. The plate is an infinite “Stonewall” - surface

**Input:**

The box option defines the nodes with the initial velocity (\*DEFINE\_BOX, \*INITIAL\_VELOCITY). The location of the “Stonewall” is at  $z=0$  (\*RIGIDWALL\_PLANAR\_FORCES). The nine nodes on the lower side of the cube are slave nodes to the “Stonewall” definition. The soft option of the rigidwall is used, which means that the slave nodes will come to stop within 10 time steps of initial contact with the rigidwall.

**Reference:**

Schweizerhof, K. and Weimer, K.





# \*RIGIDWALL\_PLANAR\_FORCES

## Cube Rebounding

```
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*RIGIDWALL_PLANAR_FORCES
$    nsid    nsidex    boxid
$         1         0         0
$
$    xt      yt      zt      xh      yh      zh      fric
$    20.0    20.0    0.0    20.0    20.0    100.0    0.000
$
$    soft    ssid    nid1    nid2    nid3    nid4
$    10      0      1      4      13     16
$
$
$
*SET_NODE_LIST
$    sid
$         1
$    nid1    nid2    nid3    nid4    nid5    nid6    nid7    nid8
$    201     202     203     204     205     206     207     208
$    209
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Initial Conditions
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
$$$$ All nodes located within box 1 are given an initial velocity.
$
*INITIAL_VELOCITY
$    nsid    nsidex    boxid
$                             1
$    vx      vy      vz
$    0.0     0.0 -100000.0
$
*DEFINE_BOX
$    boxid    xmm      xmx      ymn      ymx      zmn      zmx
$         1     14.9     25.1     14.9     25.1     9.0     21.0
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$$$$ Define Parts and Materials
$
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
$
$...>....1....>....2....>....3....>....4....>....5....>....6....>....7....>....8
$
*PART
$    pid      sid      mid      eosid      hgid      adpopt
wall-display
$         1         1         1
cube
$         2         2         2         0         0         0
$
$
$
*MAT_ELASTIC
$    mid      ro      e      pr      da      db
$         1    2.00e-8 100000.0 0.300
$
$
*MAT_ELASTIC
```

# \*RIGIDWALL\_PLANAR\_FORCES

## Cube Rebounding

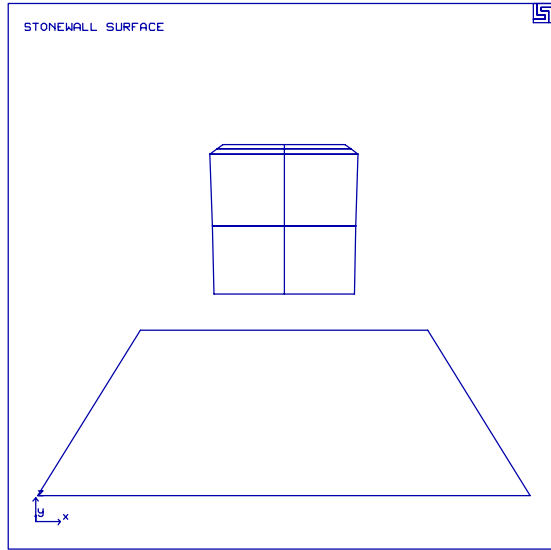
```
$      mid      ro      e      pr      da      db
      2      1.00e-8 100000.0 0.300
$
$
*SECTION_SHELL
$      sid      elform      shrf      nip      propt      qr/irid      icomp
      1
      0.83333      2.0      3.0
$      t1      t2      t3      t4      nloc
      2.0      2.0      2.0      2.0
$
*SECTION_SOLID
$      sid      elform
      2
$
$$$$$ Define Nodes and Elements
$
$$$$$
$
$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8
$
*NODE
$      node      x      y      z      tc      rc
      1      5.000000E+00      5.000000E+00      0.000000E+00      7      0
      4      3.500000E+01      5.000000E+00      0.000000E+00      7      0
      13      3.500000E+01      3.500000E+01      0.000000E+00      0      0
      .
      ... in total, 31 nodes defined
      .
      201      1.500000E+01      1.500000E+01      1.000000E+01      0      0
      225      1.500000E+01      2.500000E+01      2.000000E+01      0      0
      226      2.000000E+01      2.500000E+01      2.000000E+01      0      0
      227      2.500000E+01      2.500000E+01      2.000000E+01      0      0
$
$$$$$ Shell Elements - For Display of the Rigidwall
$
*ELEMENT_SHELL
$      eid      pid      n1      n2      n3      n4
      1      1      1      4      13      16
$
$$$$$ Solid Elements
$
*ELEMENT_SOLID
$      eid      pid      n1      n2      n3      n4      n5      n6      n7      n8
      101      2      201      202      205      204      210      211      214      213
      102      2      202      203      206      205      211      212      215      214
      103      2      204      205      208      207      213      214      217      216
      104      2      205      206      209      208      214      215      218      217
      105      2      210      211      214      213      219      220      223      222
      106      2      211      212      215      214      220      221      224      223
      107      2      213      214      217      216      222      223      226      225
      108      2      214      215      218      217      223      224      227      226
$
*END
```

# \*RIGIDWALL\_PLANAR\_FORCES

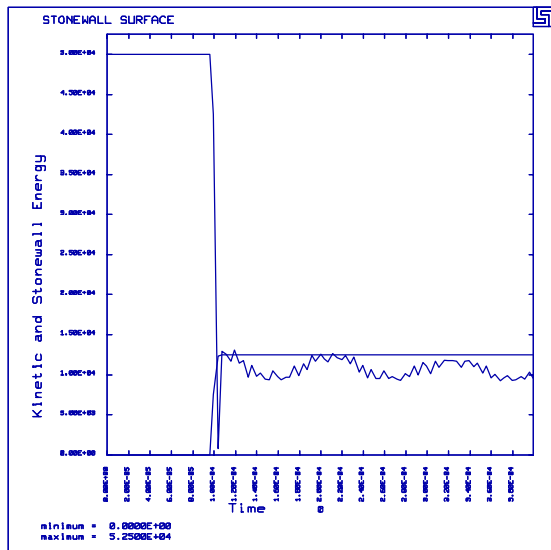
## Cube Rebounding

### Results:

taurus g=d3plot  
19  
rx -80 view



phs3 glstat  
otxt Kinetic and Stonewall Energy  
oset 0 5.25e4 kinetic over stonewall



## **\*RIGIDWALL\_PLANAR\_FORCES**

Cube Rebounding

---

**LS-DYNA Manual Section:** \*RIGIDWALL\_PLANAR\_MOVING

**Additional Sections:**

\*CONTACT\_AUTOMATIC\_SINGLE\_SURFACE

**Example:** Symmetric Crush Tube

**Filename:** rigidwall\_planar.symtube.k

**Description:**

A tube is crushed using a planar, moving rigid wall.

**Model:**

Because of symmetry , only 1/4 of the system is modeled. Automatic single surface contact is defined to prevent penetrations as the tube folds on itself. The bottom nodes of the tube are fixed using SPC's. The top of the tube is hit by a rigid wall that is defined with a mass of 800 kg and an initial velocity of 8.94 mm/ms in the negative z-direction. The friction coefficient on the wall is 1.0, this means that the nodes are prevented from sliding along the plane of the wall. An extra node is defined and associated with the rigid wall so that the walls velocity and displacement can be tracked in the ascii output file nodout (node id 99999).

**Results:**

The tubes crush and the wall forces from the ascii output file rwforc are shown. The force-deflection of the crush tube can be obtained by using the force data from rwforc and the displacement data from nodout.









**\*RIGIDWALL\_PLANAR\_MOVING**  
**Symmetric Crush Tube**

---

```
715 -5.80000000E+01 -2.40000000E+01 2.724830000E+02 0 0
716 -5.80000000E+01 -3.20000000E+01 2.724830000E+02 0 0
$
$$$$$$$$ Shell Elements
$
*ELEMENT_SHELL
$  eid      pid      n1      n2      n3      n4
   752      1      547      552      553      553
   753      1      553      548      547      547
     1      1      1      2      9      8
     2      1      2      3      10     9
     .
     ... in total, 467 shells defined
     .
   640      1      710      711      716      715
   641      1      711      485      487      716
$
*END
```

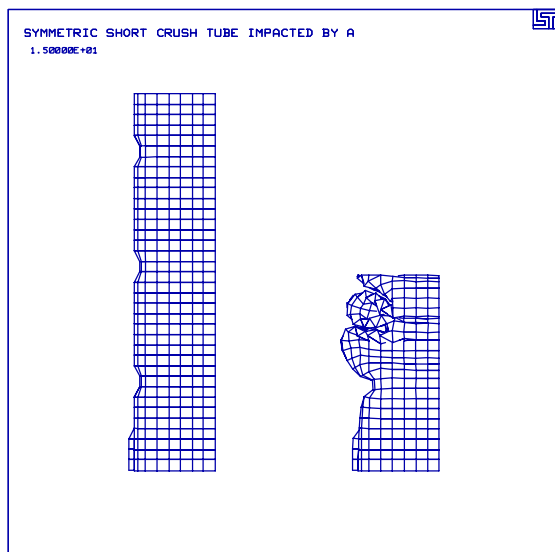
# \*RIGIDWALL\_PLANAR\_MOVING

## Symmetric Crush Tube

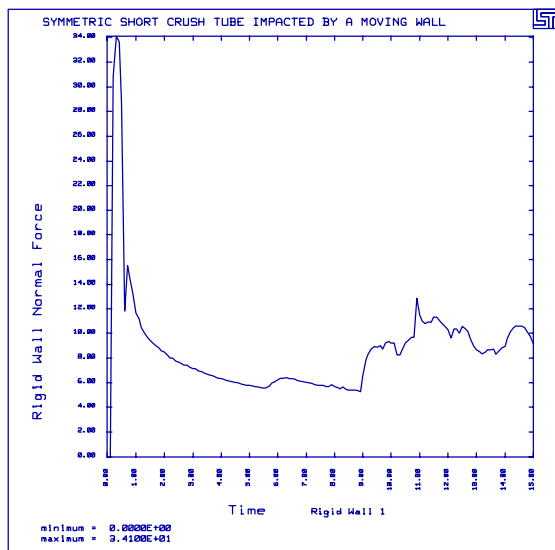
---

### Results:

taurus g=d3plot  
angle 1 rx -90 xtrans -80 view  
xtrans 160 state 16 over view



phs3  
rwforc  
oscl -1 normal



**LS-DYNA Manual Section:** \*SECTION\_SHELL

**Additional Sections:**

\*CONSTRAINED\_SPOTWELD  
\*LOAD\_NODE\_POINT

**Example:** Fuse Plate in Tension Exhibits Hourglassing

**Filename:** section\_shell.hourglassing.k

**Description:**

A fuse plate is used to connect a cut in a wide flange beam. The beam is loaded at an end, putting the fuse plate in tension. In this loading condition, the fuse plate exhibits a great deal of hourglassing.

**Model:**

The fuse plate and beam are constructed with shell elements and a piecewise linear plasticity material model with failure. The fuse plate is connected to the beam using spot welds (\*CONSTRAINED\_SPOTWELD). One end of the beam is fixed with SPC's, while the other end has several nodal point loads (\*BOUNDARY\_SPC\_NODE, \*LOAD\_NODE\_POINT). Multiple point loads are used to better distribute the input loads.

**Results:**

One look at the figures explains why it's called "hourglassing". To fix the hourglassing problem the fuse plate could be re-meshed or a fully integrated shell element formulation could be used.







**\*SECTION\_SHELL**  
**Fuse Plate in Tension Exhibits Hourglassing**

---

```
$$$$$$$ Shell Elements
$
*ELEMENT_SHELL
$   eid      pid      n1      n2      n3      n4
   487        1      647      123      501      501
   488        1      647      501      653      653
   .
   ... in total, 436 shells defined
   .
   387        3      499      496      289      497
   388        3      422      499      497      287
$
*END
```

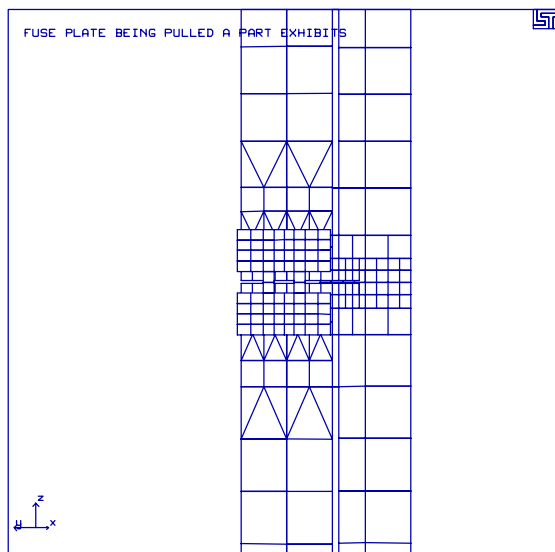
# \*SECTION\_SHELL

## Fuse Plate in Tension Exhibits Hourglassing

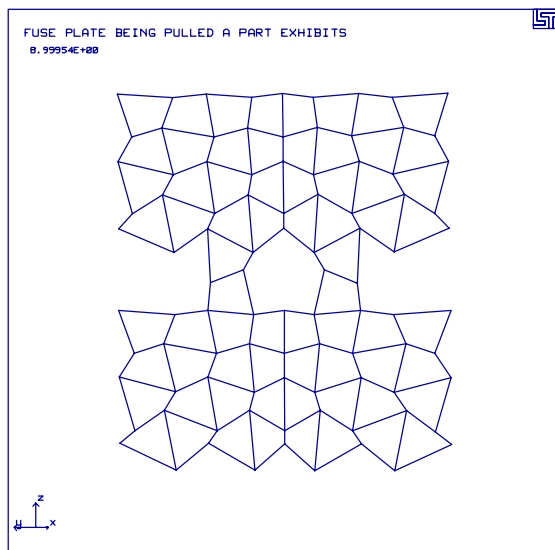
---

### Results:

taurus g=d3plot  
angle 1 rx -90 ry 60 m 3 center  
zmax 50000 dist 30000 dam view



s 10  
m 3  
center view





**LS-DYNA Manual Section:** \*SECTION\_SOLID

**Additional Sections:**

\*CONTACT\_ERODING\_SINGLE\_SURFACE  
\*INITIAL\_VELOCITY\_GENERATION

**Example:** Breaking Post Exhibits Hourglassing

**Filename:** section\_solid.hourglassing.k

**Description:**

A rigid beam strikes a post near the top of the post. There is hole cut out of the lower portion of the post to reduce its' section modulus and thus, allow it to snap-off easier. In the first model, the post begins to break, but hourglassing starts to dominate the solution and the post does not completely snap.

In the second model, a fully integrated solid formulation is used for the post, causing the post to snap-off as desired.

**Model:**

The beam is constructed with rigid shell elements. An initial velocity is given to the beam using the \*INITIAL\_VELOCITY\_GENERATION keyword. The post is constructed with solid elements using a piecewise linear plasticity material model with failure. Single point constraints (SPC's) are placed on the bottom of the post. Eroding single surface contact is required in order for the contact to behave properly while the post snaps in two (\*CONTACT\_ERODING\_SINGLE\_SURFACE).

**Results:**

The first model results are significantly different than the second model due to hourglassing.





# \*SECTION\_SOLID

## Breaking Post Exhibits Hourglassing

---

\$...>...1...>...2...>...3...>...4...>...5...>...6...>...7...>...8

\$

\$\$\$ Part 3 shell: beam

\$

\$\$\$ Part 4 solid: lower\_post

\$

\$\$\$ Part 5 solid: upper\_post

\$

\$

\*PART

\$ pid sid mid eosid hgid grav adpopt

bumper

3 1 1

lower\_post

4 2 2

upper\_post

5 2 3

\$

\$

\$\$\$\$ Materials

\$

\$\$ Bumper - Rigid, constrained to translate only in the x-direction

\$

\*MAT\_RIGID

\$ mid ro e pr n couple m alias

1 0.143E-02 200.0 0.33

\$

\$ cmo con1 con2

1.0 5 7

\$

\$ lco/a1 a2 a3 v1 v2 v3

\$

\$

\$

\$\$ Post - the lower portion is softer and fails sooner than the upper portion

\$

\*MAT\_PIECEWISE\_LINEAR\_PLASTICITY

\$ mid ro e pr sigy etan eppf tdel

2 0.499E-06 11.37 0.32 0.0468 0.11

\$

\$ c p lcss lcsr

\$

\$ Plastic stress/strain curve

0.0000 0.2500

0.0468 0.0470

\$

\$

\*MAT\_PIECEWISE\_LINEAR\_PLASTICITY

\$ mid ro e pr sigy etan eppf tdel

3 0.499E-06 110.37 0.32 0.0468 0.25

\$

\$ c p lcss lcsr

\$

\$ Plastic stress/strain curve

0.0000 0.2500

0.0468 0.0470

\$

\$

\$\$\$\$ Sections

\$

\*SECTION\_SHELL

\$ sid elform shrf nip propt qr/irid icomp

---



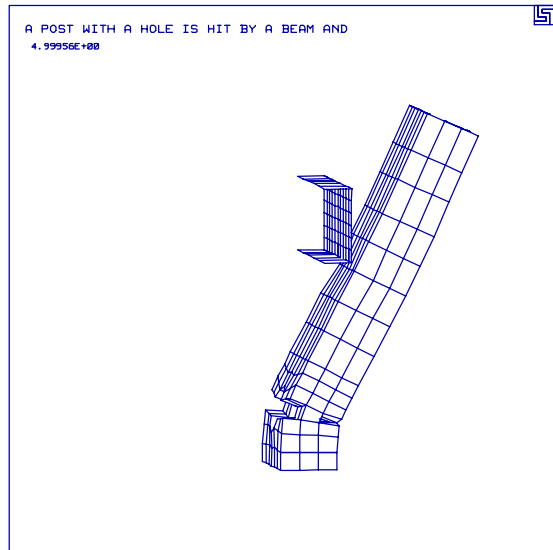
# \*SECTION\_SOLID

## Breaking Post Exhibits Hourglassing

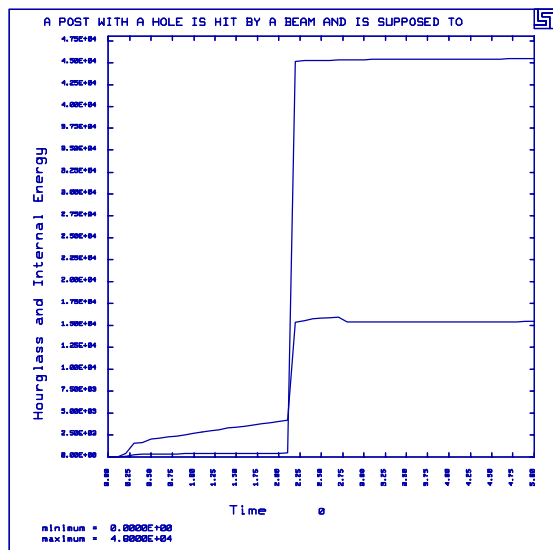
---

### Results:

taurus g=d3plot  
angle 1 rx -90 state 11  
ry 10 rx 5 view



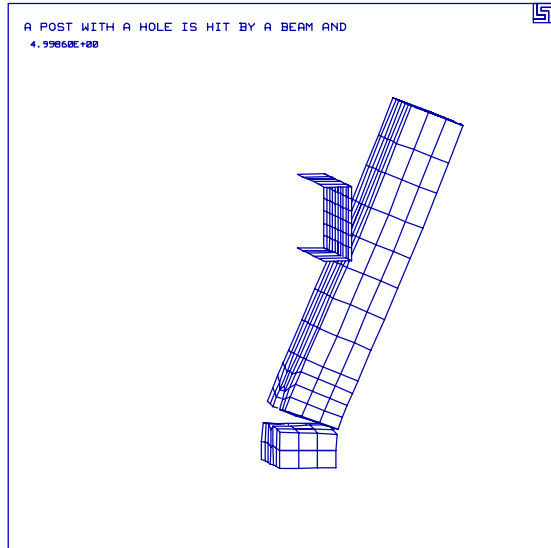
phs3 glstat  
otxt Hourglass and Internal Energy  
oset 0 4.8e4 hour over internal



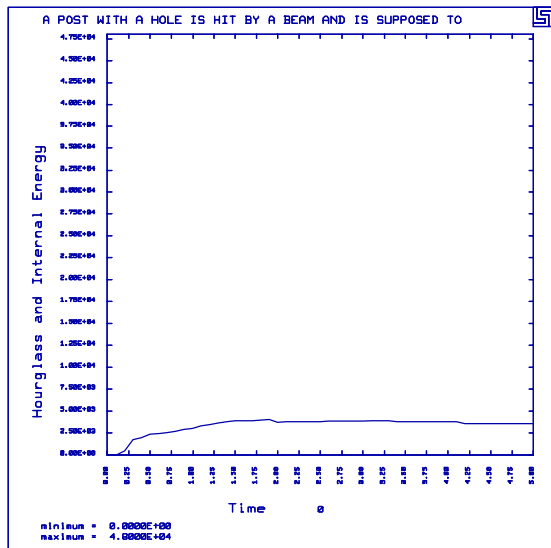
**\*SECTION\_SOLID**  
Breaking Post Exhibits Hourglassing

**Results - No Hourglassing:**

taurus g=d3plot  
angle 1 rx -90 state 11  
ry 10 rx 5 view



phs3 glstat  
otxt Hourglass and Internal Energy  
oset 0 4.8e4 hour over internal



**\*SECTION\_SOLID**

Breaking Post Exhibits Hourglassing

---



### **Acknowledgments**

N. Brannberg, L. Fredriksson and A. Gokstorp translated the description of many CADFEM examples from German to English.

Several of the new examples in the 1997 edition of this examples manual were constructed by starting with models obtained from Gene Paulsen (former Graduate student at U. Nebraska), John Gee (Cray Research), and Brad Maker (LSTC).

## **ACKNOWLEDGMENTS**

---

**References**

- Avitzur, B., Handbook of Metal Forming Procedures, John Wiley & Sons, pp. 952-954, 1983
- Belytschko, T., Wong, B. L. and Chiang, H. Y. (Northwestern University) "Improvements in Low-Order Shell Elements for Explicit Transient Analysis", Analytical and Computation Models of Shells, Edited by Belytschko, T. and Simo, J., American Society of Mechanical Engineers, 1989.
- Kenchington, C. J., "A Non-Linear Elastic Material Model for DYNA3D", DYNA3D User Group Conference, Frazer-Nash Consultancy Ltd., 1988.
- Hallquist, J. O. and Wynn, D. J. "LS-TAURUS: An Interactive Post-Processor for the Analysis Codes LS-NIKE3D, LS-DYNA3D, and TOPAZ3D", Livermore Software Technology Corporation, 1992.
- Honecker, A and Mattiasson, K, Finite Element Procedures for 3D Sheet Forming Simulation, NUMIFORM 89, pp. 457-464, Balkema, 1989.
- Hughes, T. J. R., The Finite Element Method: Linear Static and Dynamic Finite Element Analysis, Stanford University, 1987.
- Lee, C.H., and Altan, T., "Influence of Flow Stress and Friction upon Metal Flow in Upset Forging of Rings and Cylinders," Journal of Engineering for Industry," pp. 775-782, August, 1972.
- Littlewood, T., Correspondence
- Schweizerhof, K. and Weimer, K. CADFEM GmbH, Anzinger Str. 11 D-8017 Ebersberg/Munich, Tel 08092 -24012. Correspondence.
- Stillman, D. W., Correspondence.
- Wei, Lixin, Correspondence, KBS2 Inc.

## **REFERENCES**

---

## Index

### Content

Airbag Deploys into Cylinder, 3  
An Interface File Controls the Response of a Cube, 181  
Bar Impact, 117  
Belted Dummy, 227  
Billet Upset, 135  
Blow Molding, 11  
Breaking Post Exhibits Hourglassing, 277  
Cantilever Beam, 109  
Cantilever Beam with Lobotto Integration, 175  
Cube Rebounding, 259  
Cylinder Undergoing Deformation with Adaptivity, 155  
Deep Drawing with Adaptivity, 141  
Discrete Nodes Tied to a Surface, 89  
Fragmenting Plate, 209  
Frazer Nash Single Element, 203  
Fuse Plate in Tension Exhibits Hourglassing, 271  
Hemispherical Load, 123  
Hemispherical Punch, 101  
Hinged Shell with Stop Angle (Revolute Joint), 35  
Impulsively Loaded Cap with Shells and Solids, 47  
Interaction of Pendulums, 167  
Linearly Constrained Plate, 41  
Projectile Penetrates Plate, 69  
Rectangular Cup Drawing, 239  
Rigid Sphere Impacts a Plate at High Speed, 75  
Rigid Sphere Impacts Plate, 95  
Rigidwall Sphere Impacts a Plate, 247  
Rotating Elements, 191  
Rotating Shell Strikes Stonewall, 253  
Shell Rebounds from Plate Using Five Contact Types, 61  
Sliding Block in Local Coordinate System, 215  
Sliding Blocks with Planar Joint, 27  
Soil and Foam Single Element, 221  
Spotweld Secures Two Plates, 55  
Square Crush Tube with Adaptivity, 149  
Symmetric Crush Tube, 265  
Tire Bounces on a Ground and Damps Out, 161  
Tire Under Gravity Loading Bounces on a Rigidwall, 197  
Twisted Cantilever Beam, 129  
Two Plates Connected with Butt Welds, 19

## INDEX

---

### Filename

airbag.deploy.k, 3  
boundary\_prescribed\_motion.blow-mold.k, 11  
constrained.butt-weld.k, 19  
constrained.joint\_planar.k, 27  
constrained.joint\_revolute.k, 35  
constrained.linear.plate.k, 41  
constrained.shell\_solid.dome.k, 47  
constrained.spotweld.plates.k, 55  
contact.edge.k, 83  
contact.n2s-sphere.k, 75  
contact.plates.k, 61  
contact.projectile.k, 69  
contact.tied\_nodes.box.k, 89  
contact\_entity.sphere.k, 95  
control\_adaptive.cup-draw.k, 141  
control\_adaptive.cylinder.k, 155  
control\_adaptive.square-beam.k, 149  
control\_contact.hemi-draw.k, 101  
control\_damping.beam.k, 109  
control\_energy.bar-impact.k, 117  
control\_shell.beam-twist.k, 129  
control\_shell.hemi-load.k, 123  
control\_timestep.billet-forge.k, 135  
damping.tire.k, 161  
deformable\_to\_rigid.pendulum.k, 167  
deformable\_to\_rigid.pendulum.res, 167  
integration\_shell.lobotto.beam.k, 175  
interface\_component.cube.k, 181  
interface\_component.cube.rk, 181  
load\_body.gravity.k, 197  
load\_body.shell.k, 191  
mat\_fn\_rubber.element.k, 203  
mat\_piecewise\_linear.plate-shatter.k, 209  
mat\_rigid.block-slide.k, 215  
mat\_soil\_foam.element.k, 221  
mat\_spring.belted-dummy.k, 227  
mat\_transversely\_anisotropic.cup-draw.k, 239  
rigidwall\_geometric\_sphere.plate.k, 247  
rigidwall\_planar.cube.k, 259  
rigidwall\_planar.shell.k, 253  
rigidwall\_planar.symtube.k, 265  
section\_shell.hourglassing.k, 271  
section\_solid.hourglassing.k, 277

---

**Section**

- \*AIRBAG\_SIMPLE\_AIRBAG\_MODEL, 3
- \*BOUNDARY\_PRESCRIBED\_MOTION, 11
- \*BOUNDARY\_PRESCRIBED\_MOTION\_NODE, 41, 191
- \*BOUNDARY\_PRESCRIBED\_MOTION\_RIGID, 95
- \*BOUNDARY\_PRESCRIBED\_MOTION\_SET, 55
- \*BOUNDARY\_SPC\_NODE, 167
- \*CONSTRAINED\_EXTRA\_NODES\_SET, 27, 227
- \*CONSTRAINED\_GENERALIZED\_WELD, 19
- \*CONSTRAINED\_JOINT\_PLANAR, 27
- \*CONSTRAINED\_JOINT\_REVOLUTE, 35
- \*CONSTRAINED\_JOINT\_SPHERICAL, 227
- \*CONSTRAINED\_JOINT\_STIFFNESS, 35
- \*CONSTRAINED\_LINEAR, 41
- \*CONSTRAINED\_SHELL\_TO\_SOLID, 47
- \*CONSTRAINED\_SPOTWELD, 55, 271
- \*CONSTRAINED\_TIED\_NODES\_FAILURE, 75
- \*CONTACT, 61
- \*CONTACT\_AUTOMATIC\_SINGLE\_SURFACE, 265
- \*CONTACT\_ENTITY, 95
- \*CONTACT\_ERODING\_SINGLE\_SURFACE, 277
- \*CONTACT\_ERODING\_SURFACE\_TO\_SURFACE, 69
- \*CONTACT\_FORCE\_TRANSDUCER\_PENALTY, 83
- \*CONTACT\_NODES\_TO\_SURFACE, 3, 75
- \*CONTACT\_ONE\_WAY\_SURFACE\_TO\_SURFACE, 239
- \*CONTACT\_SINGLE\_EDGE, 83
- \*CONTACT\_SURFACE\_TO\_SURFACE, 227
- \*CONTACT\_TIED\_NODES\_TO\_SURFACE, 89
- \*CONTROL\_ADAPTIVE, 141, 149, 155
- \*CONTROL\_CONTACT, 101
- \*CONTROL\_DAMPING, 109, 161
- \*CONTROL\_ENERGY, 117
- \*CONTROL\_SHELL, 123, 129
- \*CONTROL\_SUBCYCLE, 149
- \*CONTROL\_TIMESTEP, 35, 135
- \*DAMPING\_GLOBAL, 109, 141, 161, 175
- \*DATABASE\_CROSS\_SECTION\_PLANE, 19, 55
- \*DATABASE\_CROSS\_SECTION\_SET, 55, 191
- \*DATABASE\_CROSS\_SECTION\_SET, 109
- \*DEFINE\_COORDINATE\_VECTOR, 155, 215
- \*DEFINE\_CURVE, 41
- \*DEFINE\_SD\_ORIENTATION, 227
- \*DEFORMABLE\_TO\_RIGID, 167
- \*ELEMENT\_DISCRETE, 227
- \*INITIAL\_VELOCITY, 61, 181
- \*INITIAL\_VELOCITY\_GENERATION, 69, 277

## INDEX

---

- \*INITIAL\_VELOCITY\_NODE, 27, 191, 253
- \*INTEGRATION\_SHELL, 175
- \*INTERFACE\_COMPONENT, 181
- \*INTERFACE\_LINKING\_SEGMENT, 181
- \*LOAD\_BODY\_GENERALIZED, 191
- \*LOAD\_BODY\_Y, 167
- \*LOAD\_BODY\_Z, 161, 197, 227
- \*LOAD\_NODE\_POINT, 27, 175, 271
- \*LOAD\_NODE\_SET, 109
- \*LOAD\_RIGID\_BODY, 141
- \*LOAD\_SEGMENT, 47
- \*LOAD\_SEGMENT, 11, 27, 101, 215
- \*LOAD\_SHELL\_ELEMENT, 239
- \*MAT\_DAMPER\_VISCOUS, 227
- \*MAT\_PIECEWISE\_LINEAR\_PLASTICITY, 209
- \*MAT\_POWER\_LAW\_PLASTICITY, 101
- \*MAT\_RIGID, 215
- \*MAT\_SOIL\_AND\_FOAM, 221
- \*MAT\_SPRING, 227
- \*MAT\_TRANSVERSELY\_ANISOTROPIC, 239
- \*PART\_INERTIA, 227
- \*RIGID\_DEFORMABLE\_R2D, 167
- \*RIGIDWALL\_GEOMETRIC\_SPHERE\_MOTION, 247
- \*RIGIDWALL\_PLANAR, 3, 101, 197, 253
- \*RIGIDWALL\_PLANAR\_FORCES, 259
- \*RIGIDWALL\_PLANAR\_MOVING, 265
- \*SECTION\_SHELL, 271
- \*SECTION\_SOLID, 277